

MICRO-SCALE AND FULL-SCALE CFD SIMULATION OF AFTER- TREATMENT DEVICES FOR INTERNAL COMBUSTION ENGINES

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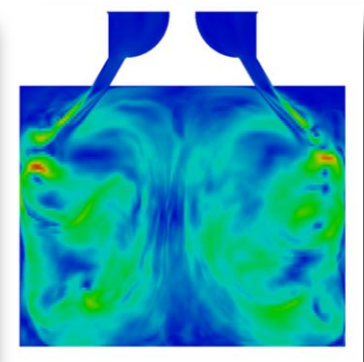
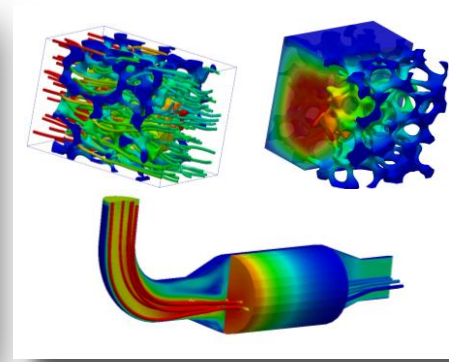
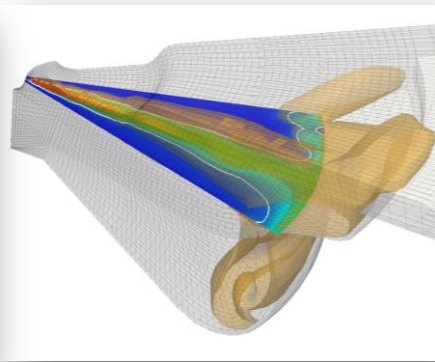
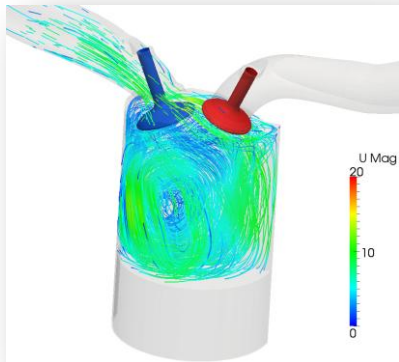
Outline

- ✧ Characterization of the flow regimes occurring inside real open cell foams
 - ✧ Micro-CT scans
 - ✧ Surface reconstruction and mesh creation
 - ✧ Equivalent artificial and repeatable structures (cubic cells, Kelvin cells ...)
 - ✧ Detailed simulation and flow analysis
- ✧ Developments of up-scaling and surface reactions with conjugate heat transfer in OpenFOAM^R
- ✧ Performances foam-type structures (Kelvin cell) vs honeycombs
 - ✧ Pressure drop
 - ✧ Mass transfer
 - ✧ Global performance
- ✧ Full scale simulation and comparison with honeycomb performance during a driving cycle

LibICE for OpenFOAM

INTERNAL COMBUSTION ENGINES

- GDI and Diesel spray modelling: atomization, cavitation, spray-wall interaction
- combustion models with complex chemistry for Diesel, SI and HCCI engines
- unsteady flows in intake and exhaust systems: plenums, silencers, 1D-3D coupling
- reacting flows in after-treatment devices: DPF, SCR, catalytic converter
- Large Eddy Simulation of engine-like geometries and injector internal nozzle flows
- 1D thermo-fluid dynamic models of the turbocharged engines

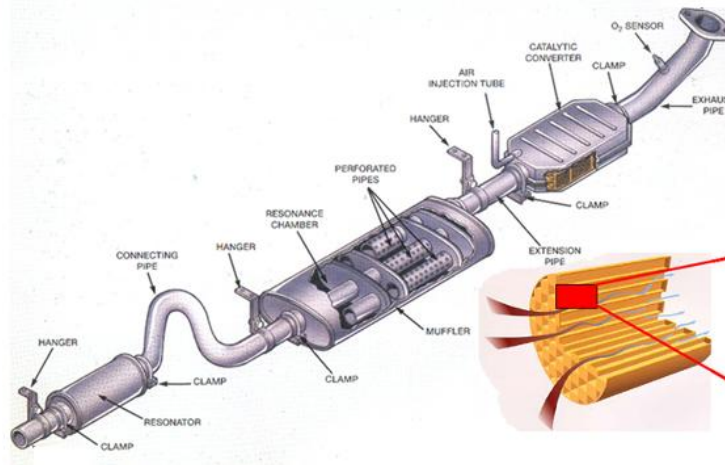


Main concept: applied to ICE

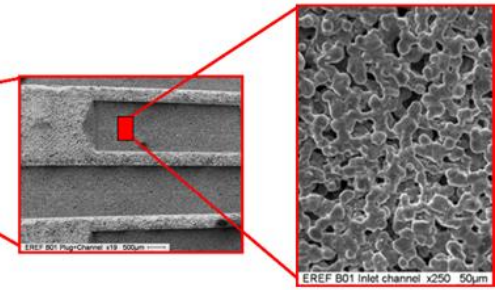
Engine scale



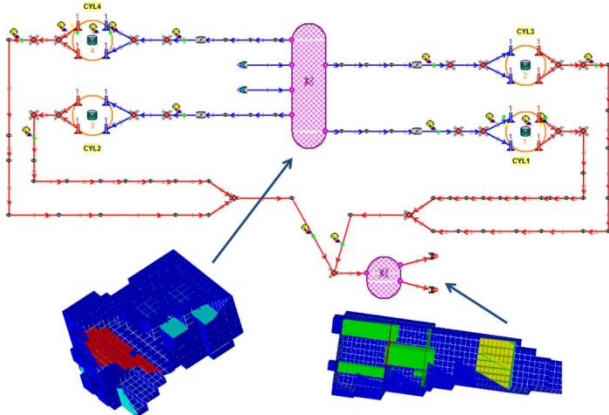
Component scale



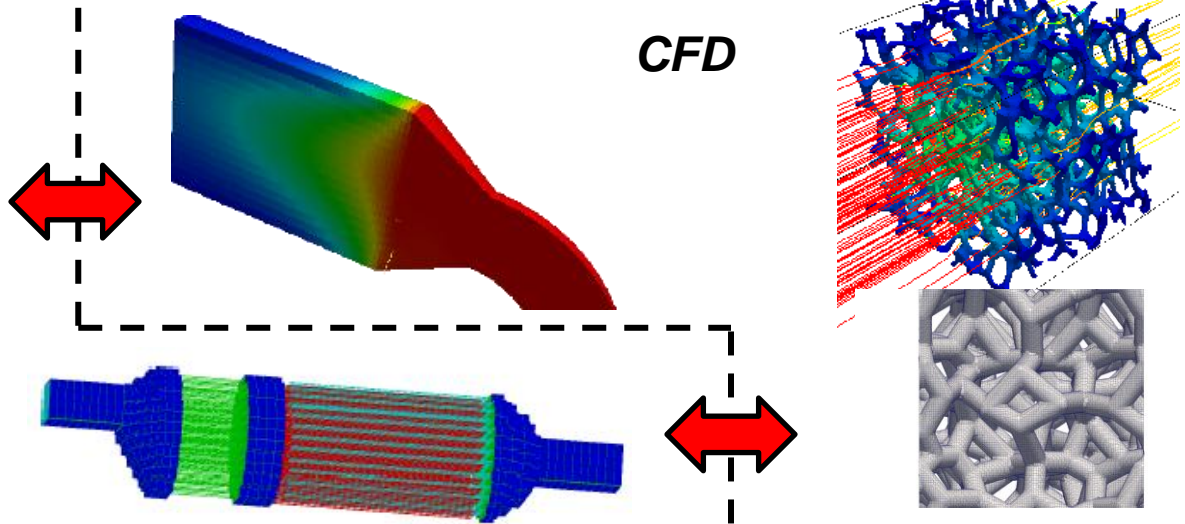
Micro-structure scale



Quasi-3D

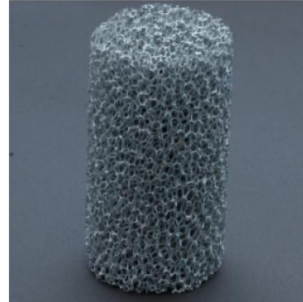
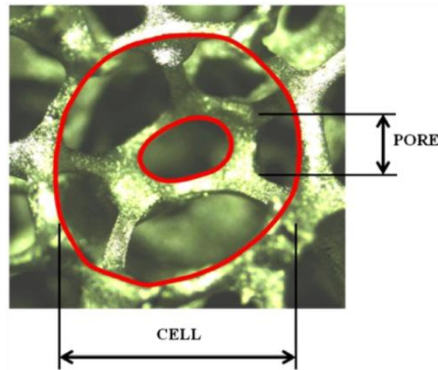


CFD



The substrates

Open-cell foam



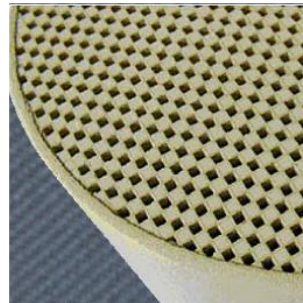
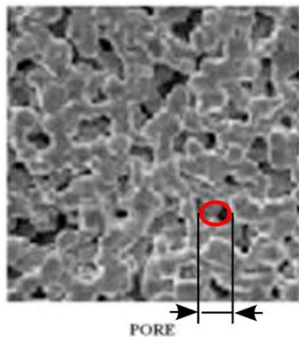
Al alloy
95% porosity
40 ppi



SiC
86% porosity
80 ppi

Applications:
Catalytic substrates for after-treatment devices (as an alternative to traditional honeycomb)

Filtering media



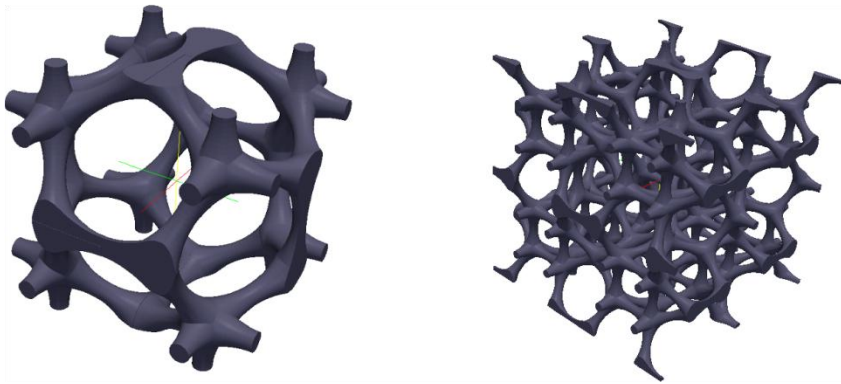
Cordierite
50% porosity
16 μm pore

Applications:
Removal of particulate matter from exhaust gas

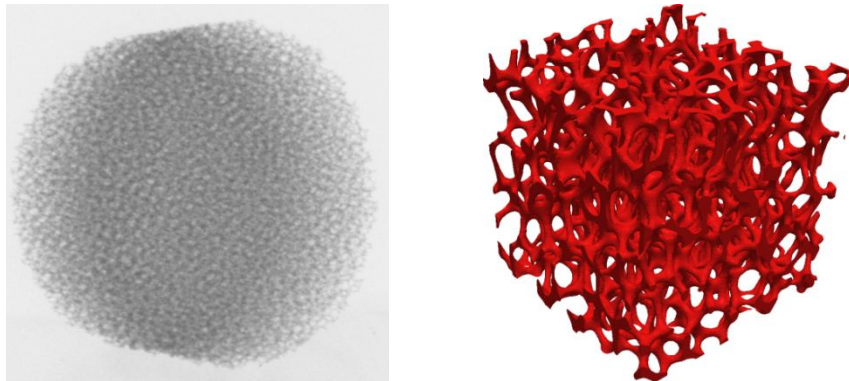
From the sample to the CFD model

Geometry reconstruction

Geometry idealization

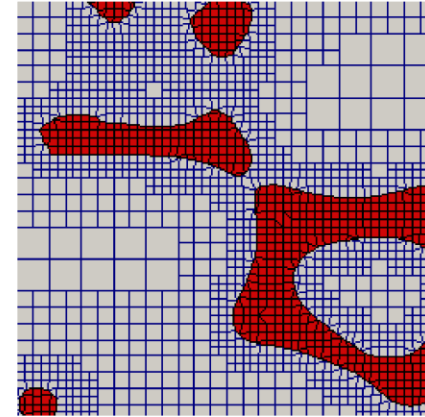


Micro-CT geometry reconstruction

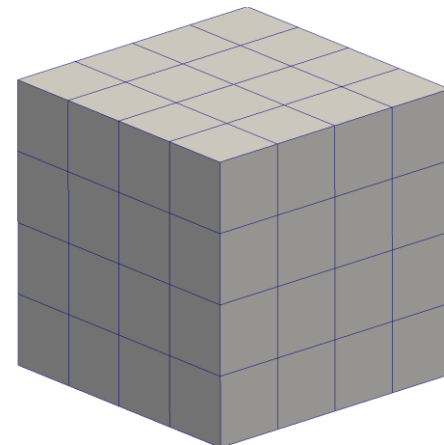


Mesh generation

snappyHexMesh



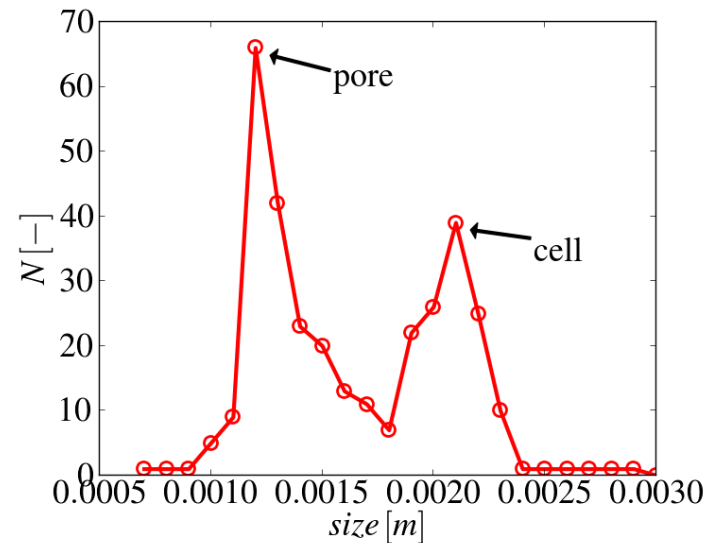
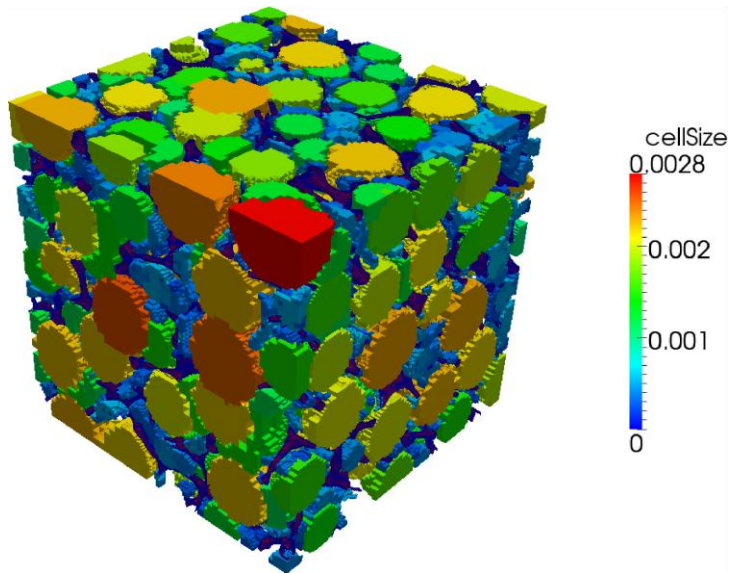
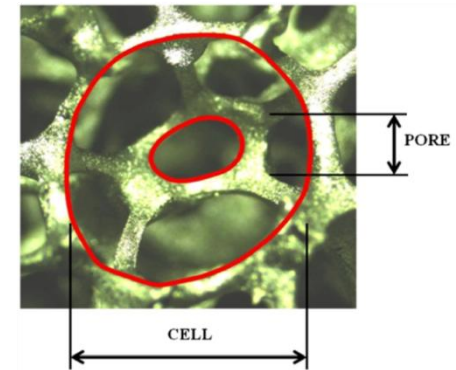
imageHexMesh



Geometry characterization

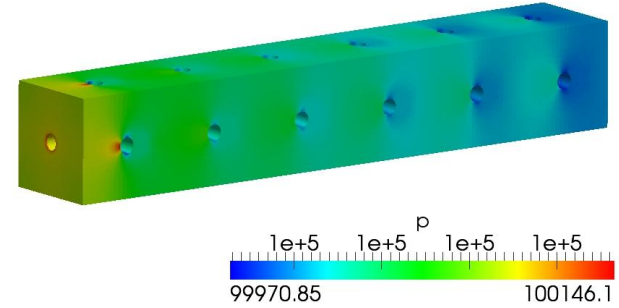
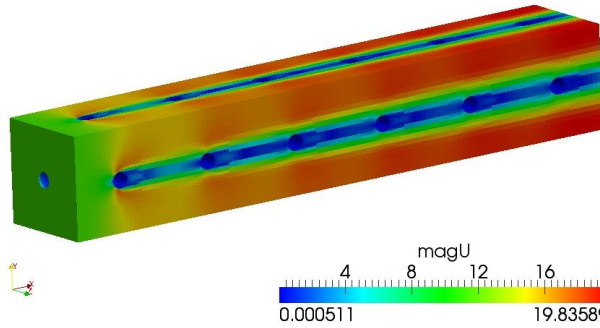
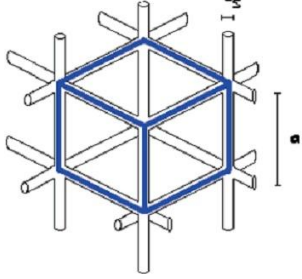
- Geometric parameters of the micro-structure computed on the CFD mesh
- Cell/pore size calculation: algorithm based on the opening size concept

	Al foam	Si-C foam	Cordierite
porosity [-]	0.96	0.87	0.50
spec. surf. [m^2/m^2]	664.6	4053.3	64833.6
cell size [m]	$2.1 \cdot 10^{-3}$	$5.0 \cdot 10^{-4}$	-
pore size [m]	$1.2 \cdot 10^{-3}$	$3.1 \cdot 10^{-4}$	$1.6 \cdot 10^{-5}$

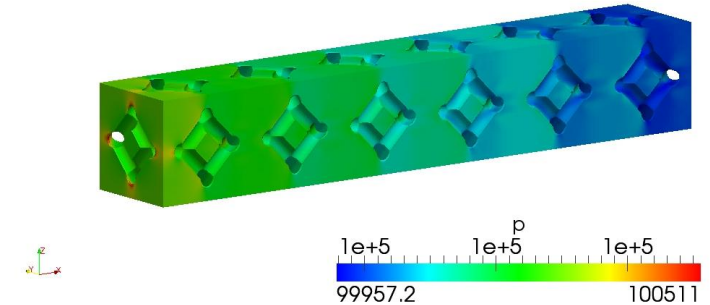
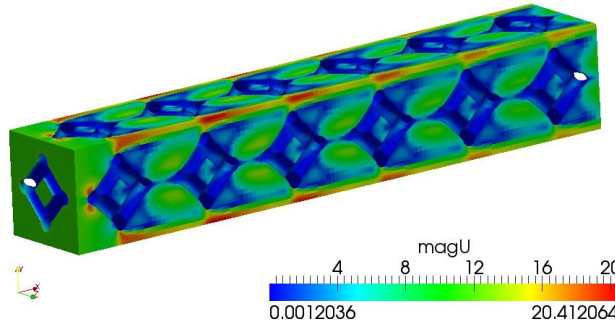
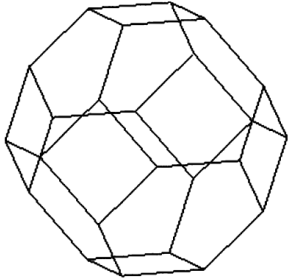


How can we approximate a real foam?

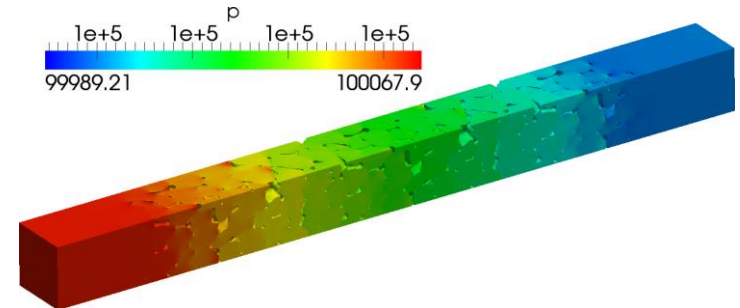
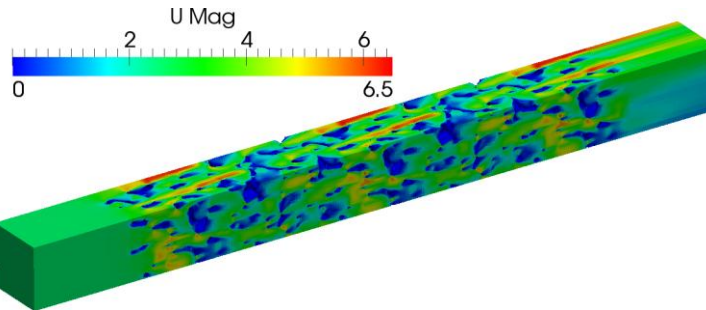
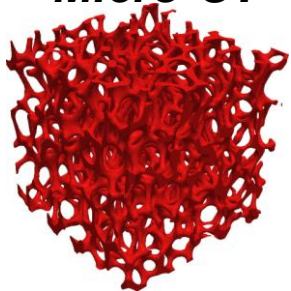
Cubic cell



Kelvin cell

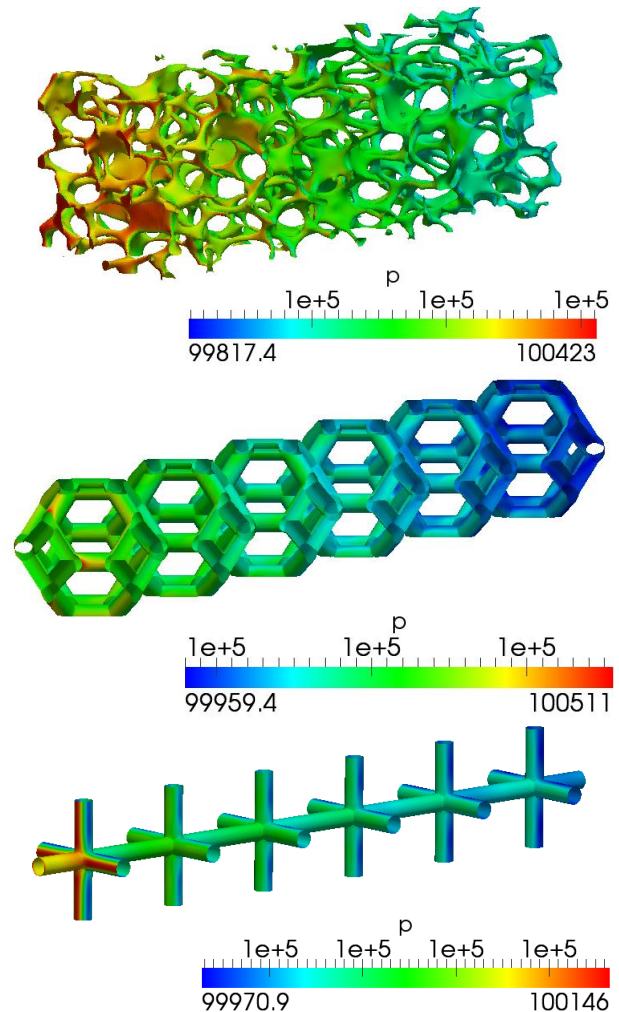
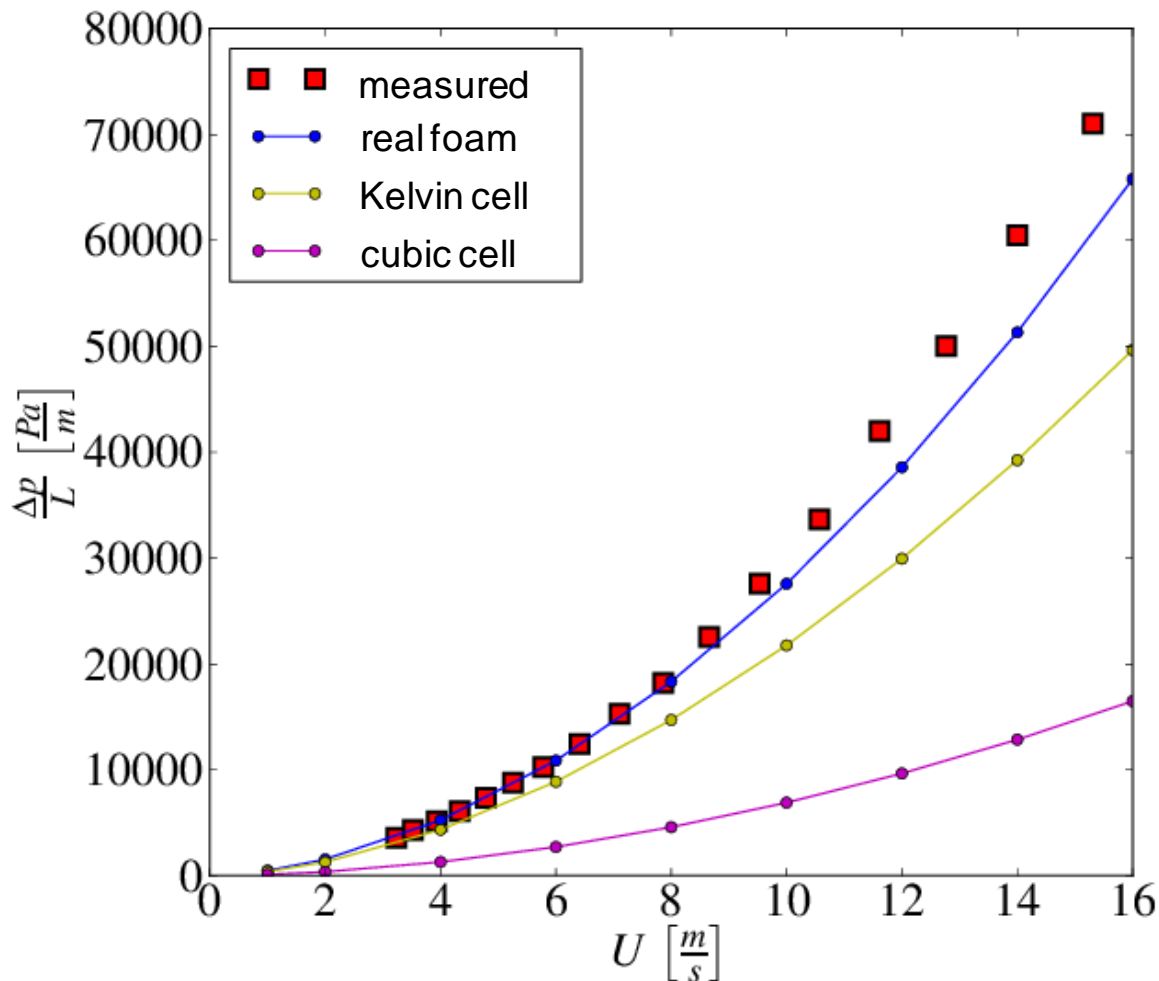


Micro-CT

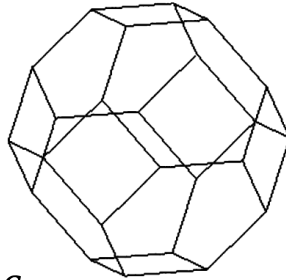
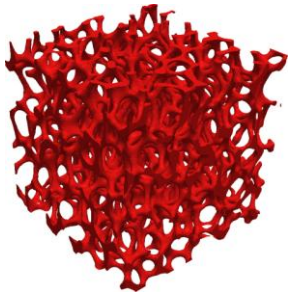


Comparison of the pressure drop

- Same porosity and cell size

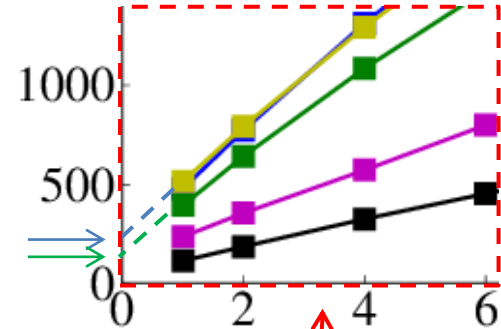
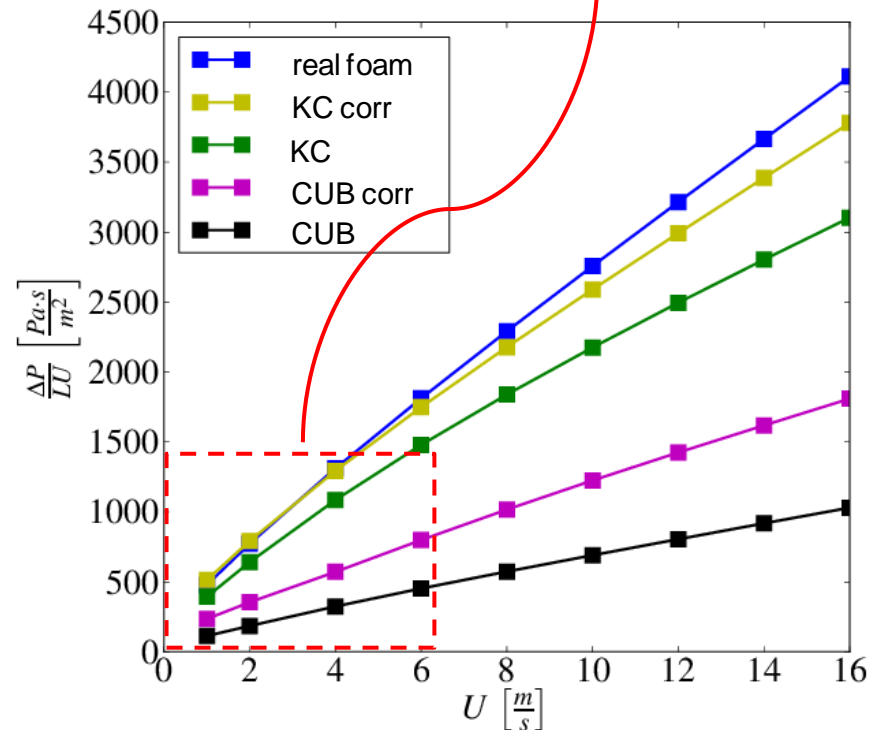
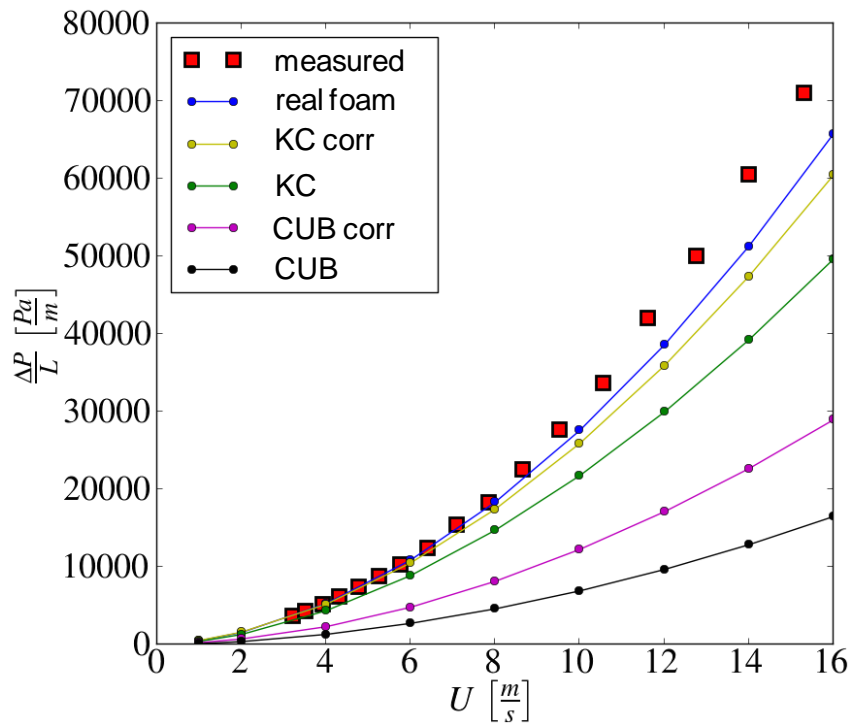


Correction of the KC model: pressure drop



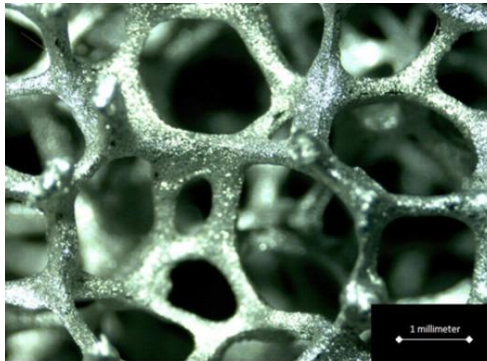
$$\varphi_{real} = \varphi_{KC}$$

$$S_{V,real} = S_{V,KC}$$

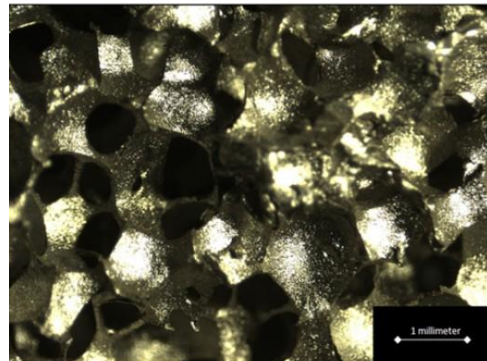


Comparison: pressure drop

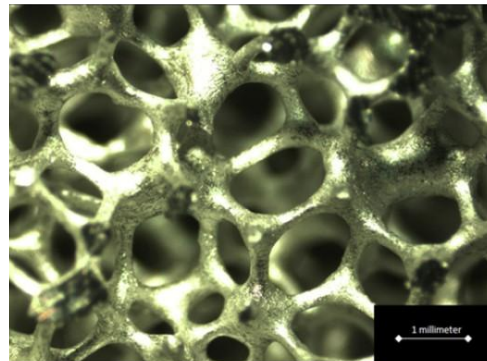
B



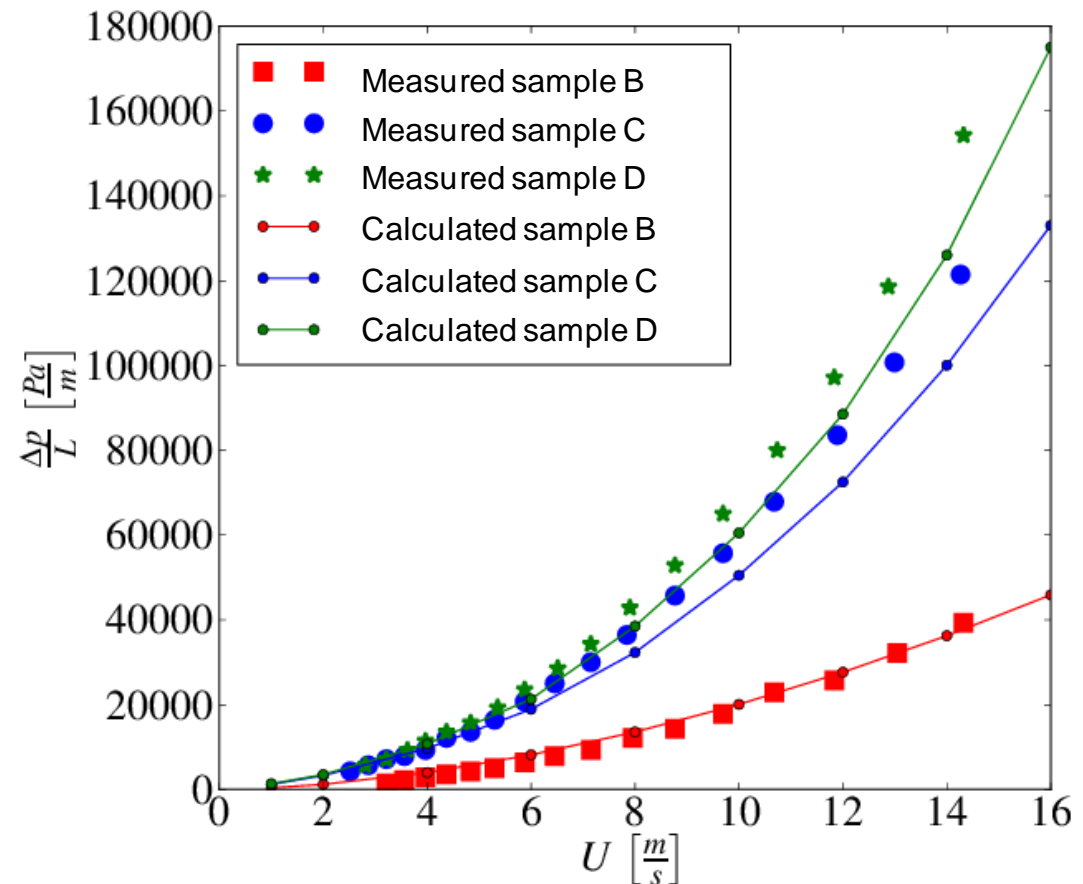
C



D

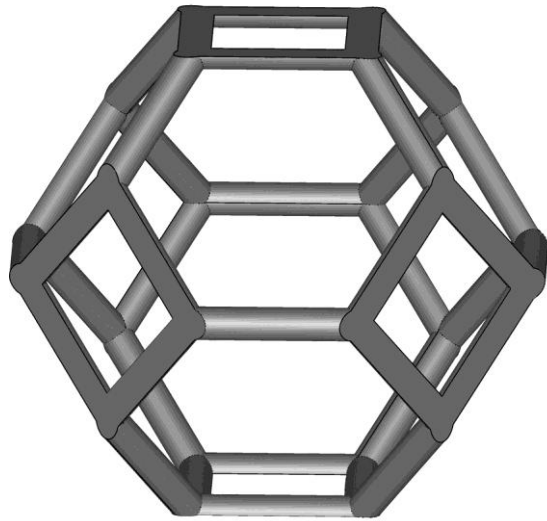


- Reconstruction of real sample by Kelvin cell type idealized foam

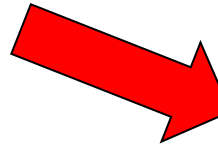
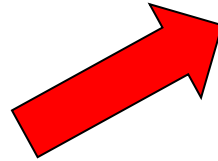


Further enhancement

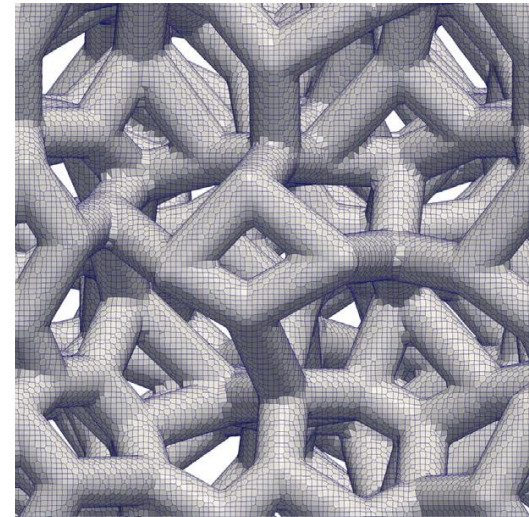
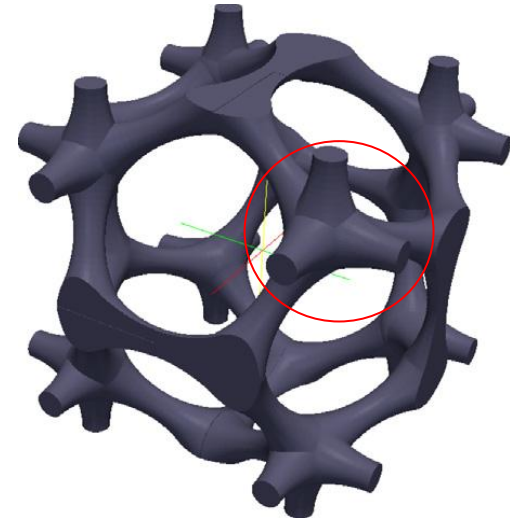
- Introduction of an additional degree of freedom



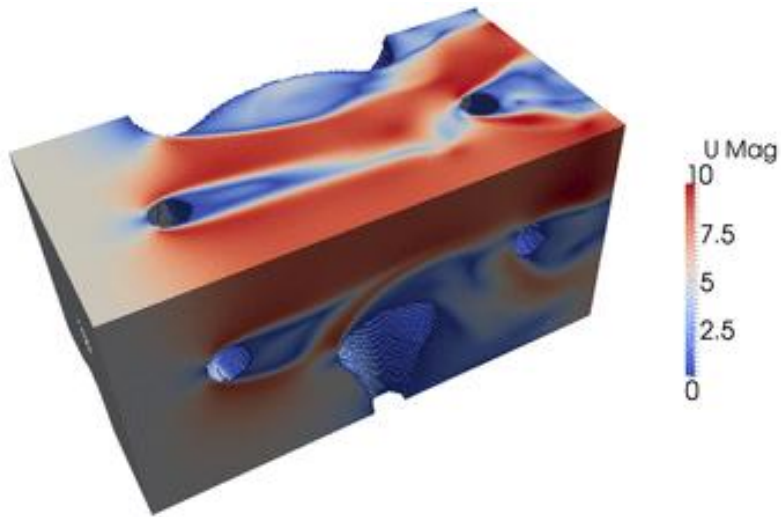
Material clustering
at cell vertexes



Randomization
(edge length)



Detailed simulation: cold flow

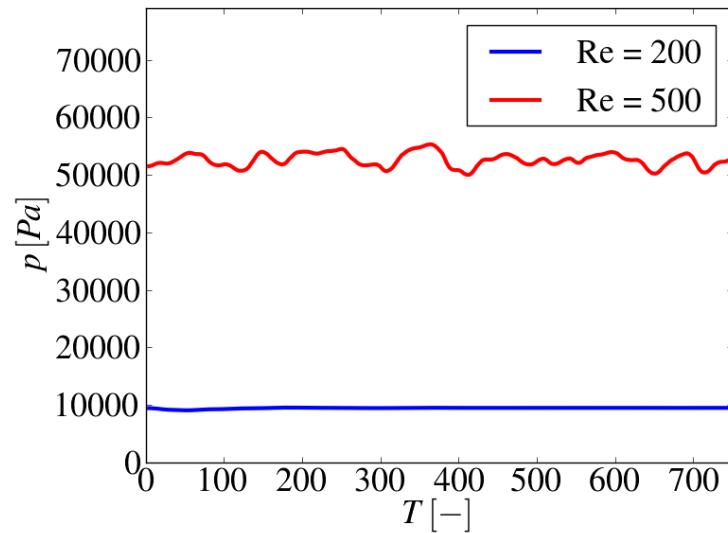


Numerical schemes accuracy:

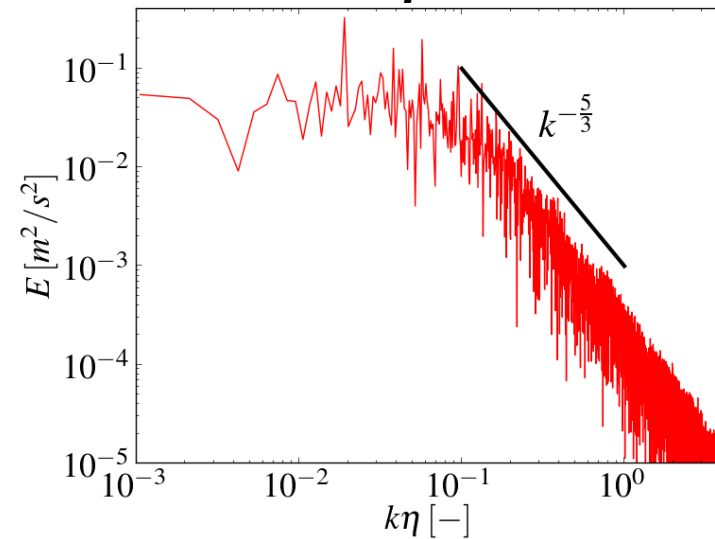
- **Time:** second order
- **Space:** third order

Re [-]	200	500
η [m]	$1.8 \cdot 10^{-5}$	$9.4 \cdot 10^{-6}$
τ_η [s]	$9.0 \cdot 10^{-6}$	$1.8 \cdot 10^{-6}$
$\Delta x / \eta$ [-]	1.1	2.1

Pressure



TKE spectrum



From Micro-scale to Macro-scale

Upscaling of the micro-scale governing equations:

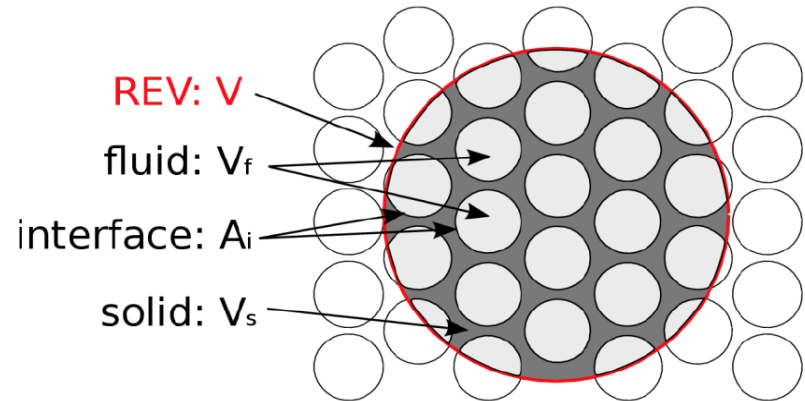
- Local volume average operator:

$$\langle \varphi \rangle^V = \frac{1}{V} \int_V \varphi dV, \quad \varphi = \langle \varphi \rangle^i + {}^i \varphi$$

- Time average operator:

$$\bar{\varphi} = \frac{1}{\Delta t} \int_{\Delta t} \varphi dt, \quad \varphi = \bar{\varphi} + \varphi'$$

- Double decomposition concept



Theorem of local volumetric average

$$\langle \nabla \varphi \rangle^V = \nabla (\Phi \langle \varphi \rangle^i) + \frac{1}{V} \int_{S_i} \mathbf{n} \varphi dS$$

$$\langle \nabla \cdot \varphi \rangle^V = \nabla \cdot (\Phi \langle \varphi \rangle^i) + \frac{1}{V} \int_{S_i} \mathbf{n} \cdot \varphi dS$$

$$\left\langle \frac{\partial \varphi}{\partial t} \right\rangle^V = \frac{\partial}{\partial t} (\Phi \langle \varphi \rangle^i) + \frac{1}{V} \int_{S_i} \mathbf{n} \cdot (\mathbf{U}_i \varphi) dS$$

Application of volumetric average operators on the micro-scale governing equations

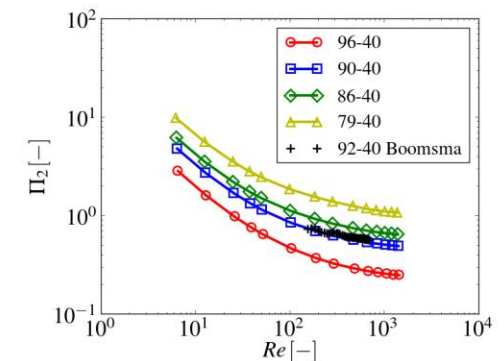
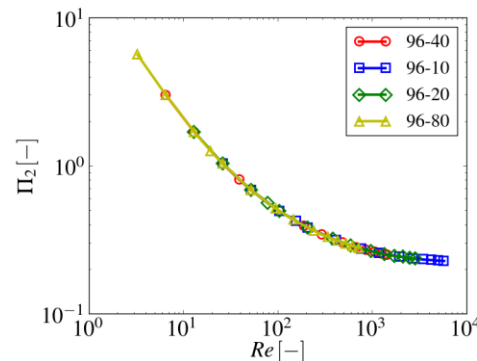
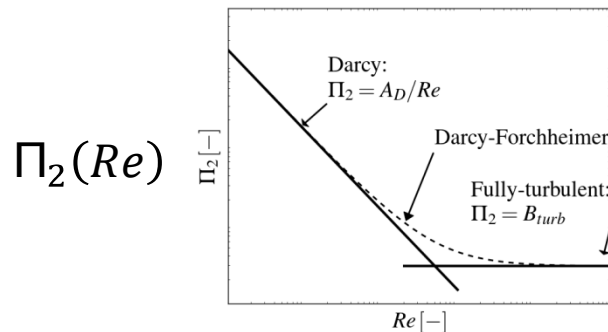
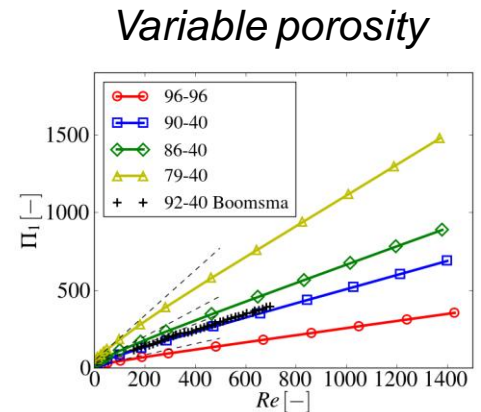
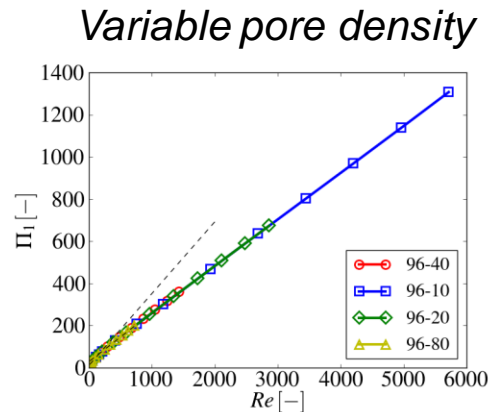
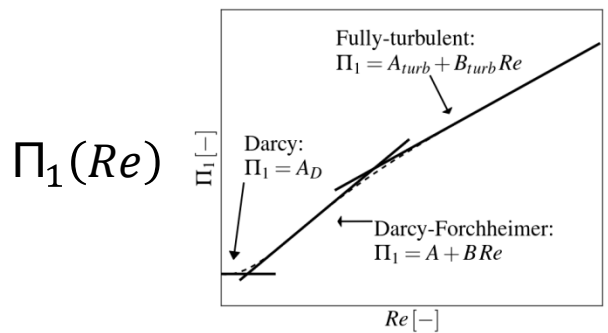


Appearance of **extra source terms**

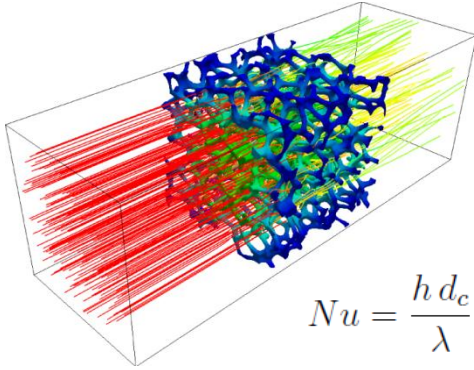
Extracting information for upscaling

Non-dimensional relationships evaluated on the basis of **micro-scale simulations**

$$\Pi_1 = \frac{\mathfrak{R} d_c^2}{\hat{U} \hat{\mu}} = \mathcal{F}_{\Pi_1} \left(\text{Re} = \frac{\rho \hat{U} d_c}{\hat{\mu}} \right) \quad \Pi_2 = \frac{\mathfrak{R} d_c}{\hat{\rho} \hat{U}^2} = \mathcal{F}_{\Pi_2} \left(\frac{1}{\text{Re}} = \frac{\hat{\mu}}{\hat{\rho} \hat{U} d_c} \right)$$



Modelling the heat transfer source term



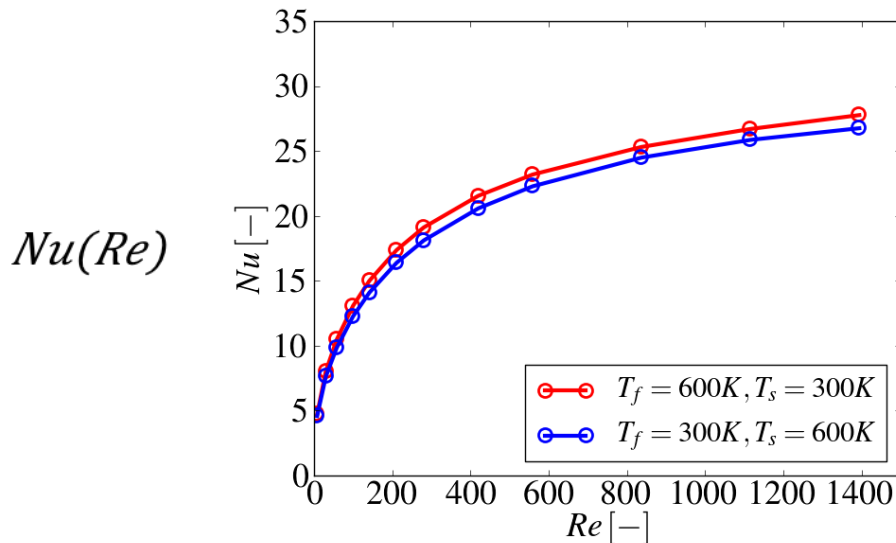
Non-dimensional relationship evaluated on the basis of **micro-scale simulations**

$$Nu = \frac{h d_c}{\lambda} = \mathcal{F}_{Nu} \left(Re = \frac{\hat{\rho} \|\hat{\mathbf{U}}\| d_c}{\hat{\mu}}, Pr = \frac{\hat{\mu} \hat{c}_{p,f}}{\hat{\lambda}_f} \right)$$

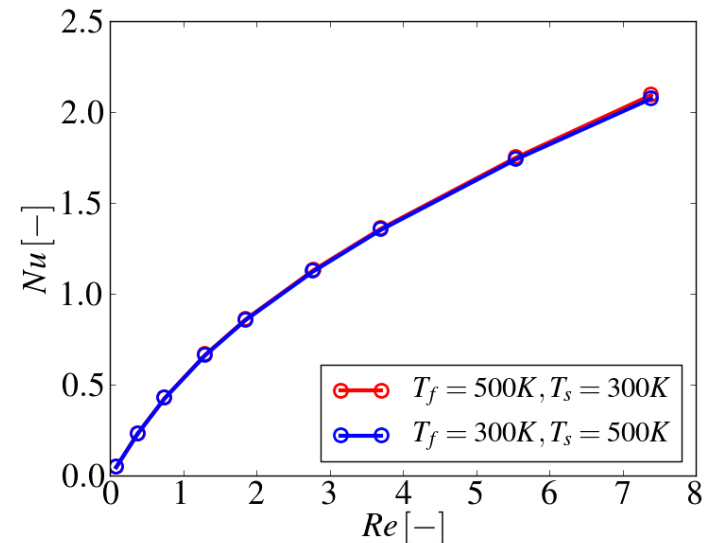
Inter-phase **heat transfer source term** in macro-scale energy equation

$$Q^{f \rightarrow s} = Nu \frac{\lambda_f}{d_c} \sigma V (\hat{T}_s - \hat{T}_f)$$

Al foam



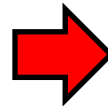
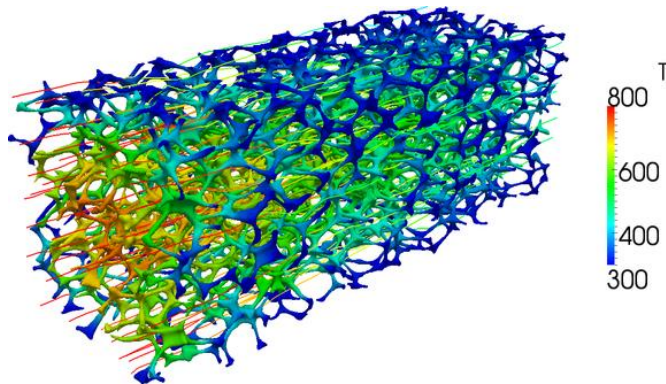
SiC foam



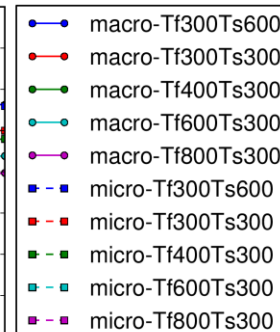
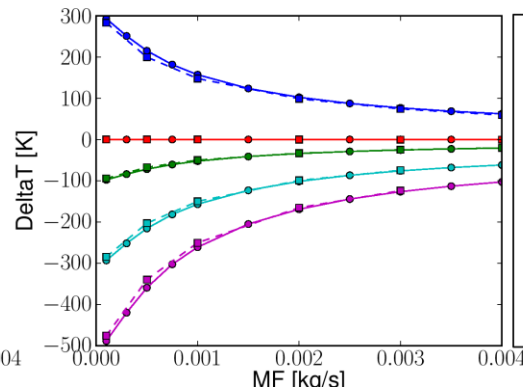
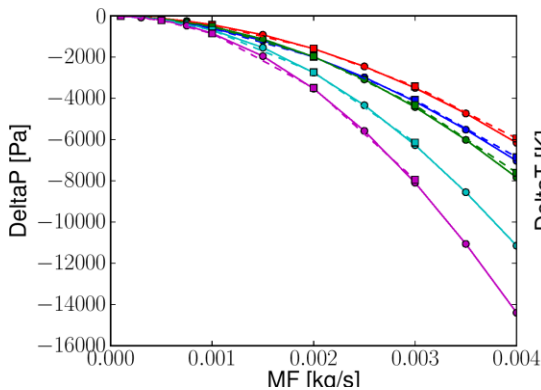
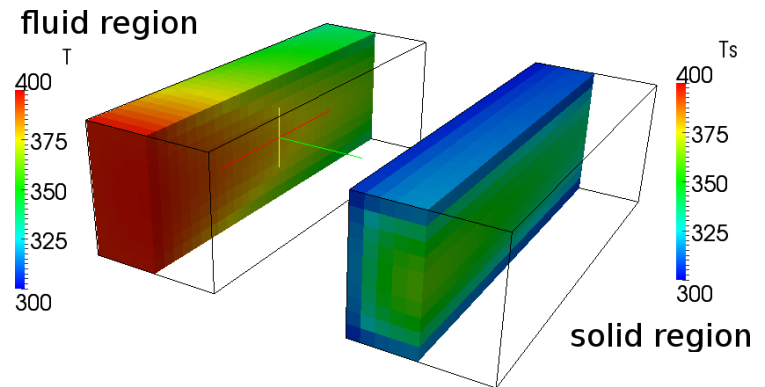
Examples of application

- Macro-scale approach is based on a multi-regions framework, in which fluid and solid phases are simulated on different (partially or totally) overlapping mesh.
- Models are introduced for the coupling between the solid and fluid phases.

Micro-scale approach



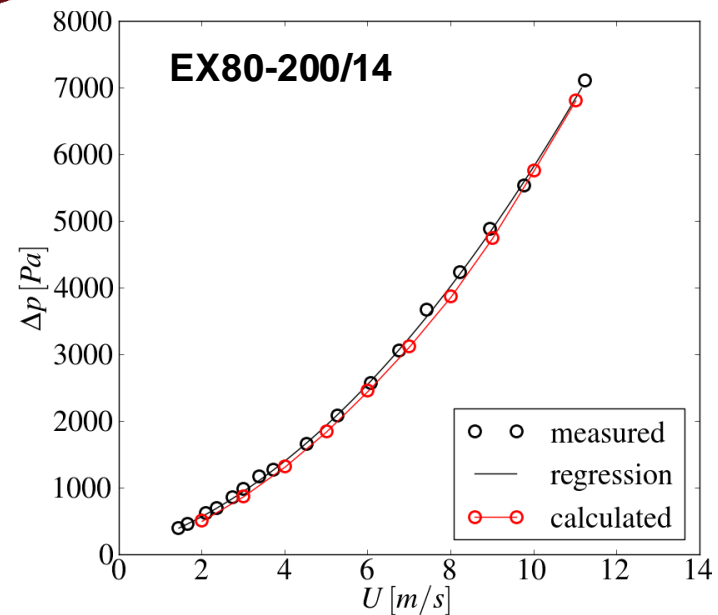
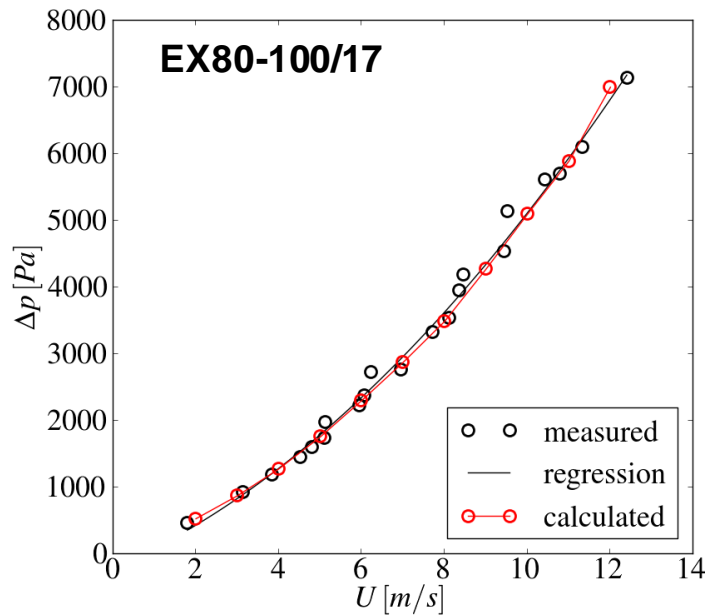
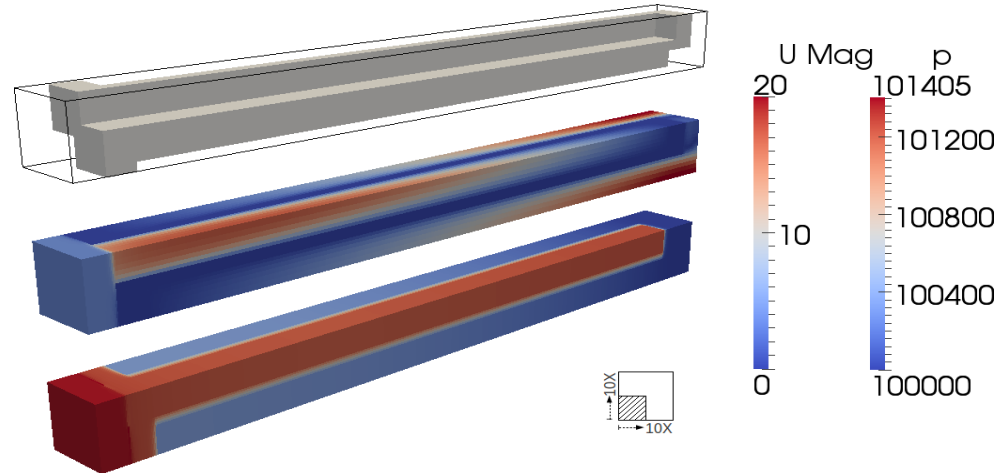
Macro-scale approach



Check on consistency between macro- and micro-scale approaches

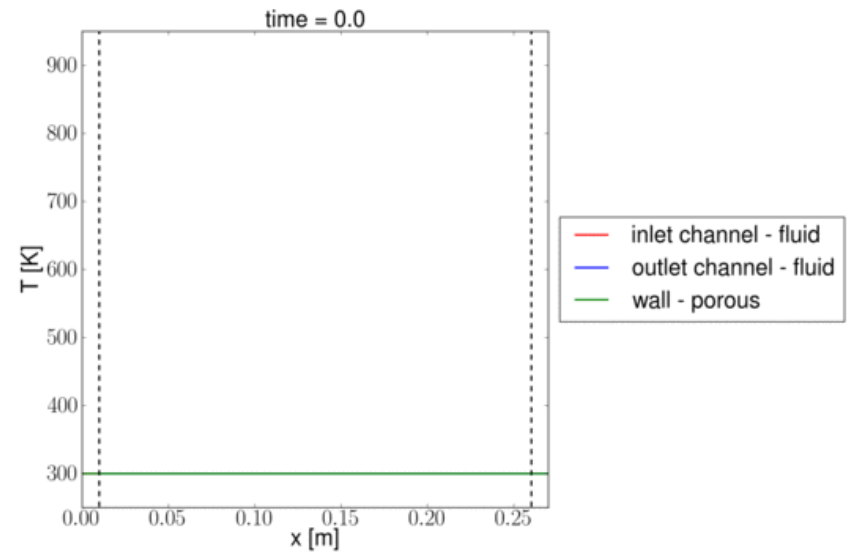
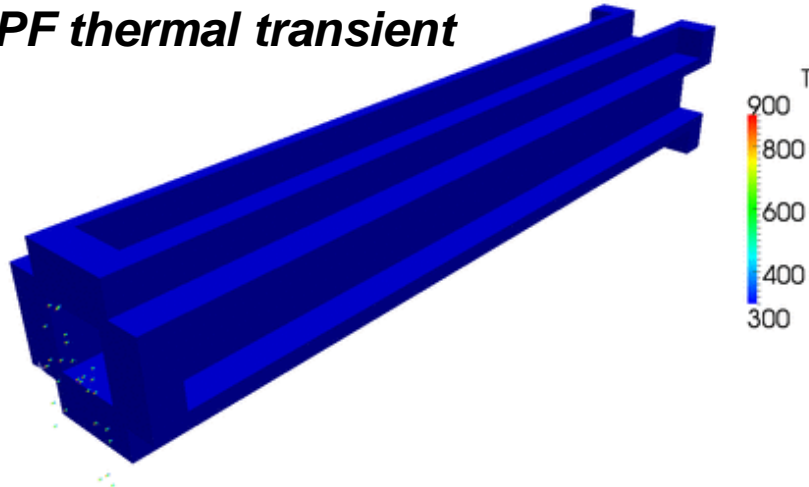
Examples of application

Simulation of flow through a couple of DPF channels

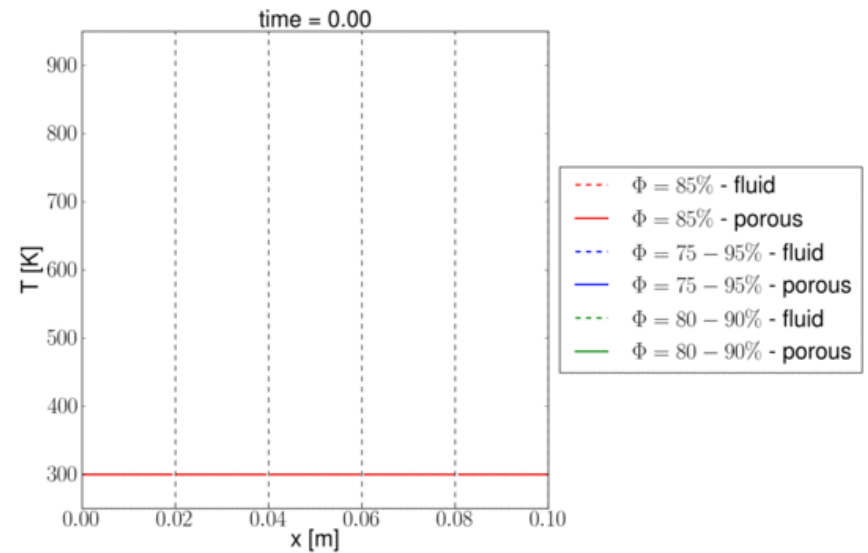
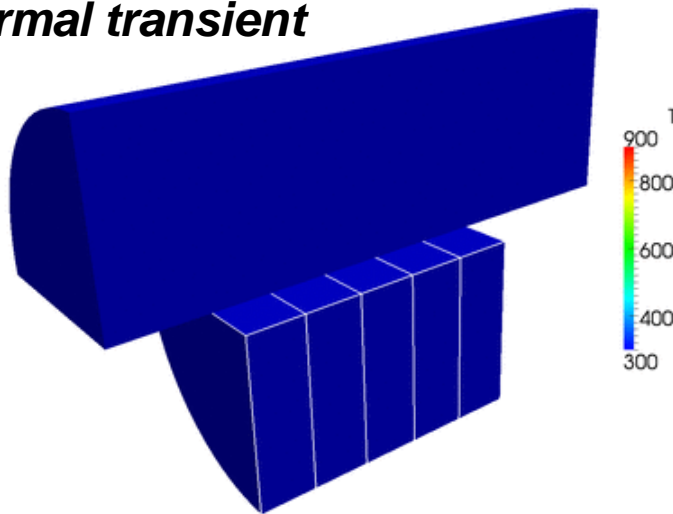


Examples of application

DPF thermal transient

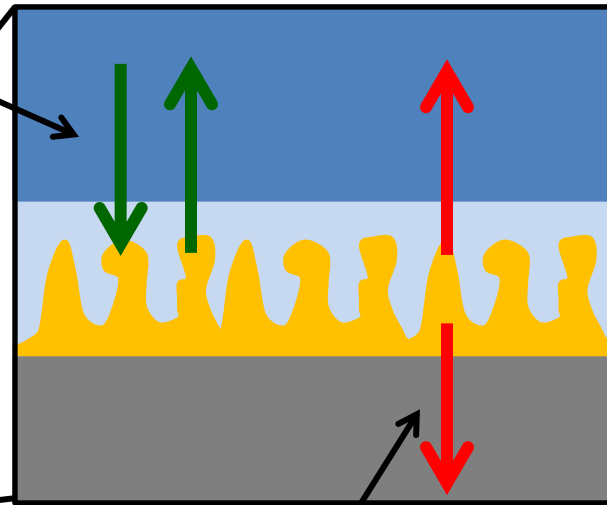
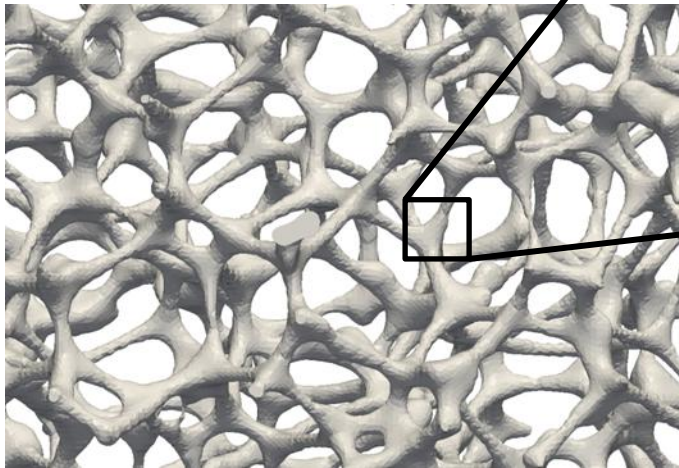


Multi-layer foam catalyst thermal transient



Modelling catalytic reactions

Mass transfer between gas phase and catalytic surface inside the washcoat



gas
near wall
gas
washcoat
solid wall

Reaction heat is released and transferred to fluid and solid phase

Definition of the washcoatZone

Definition of the **washcoatZone**, which contains the geometric information and supports CHT simulations in a multi-region framework

```
class washcoatZone
{
    // Private data
    //- Name of this zone, or a regular expression
    keyType key_;

    //- Dictionary containing the parameters
    dictionary dict_;

    //- Reference to the fluid finite volume mesh
    const fvMesh& mesh_;

    //- List of fluid faces belonging to the zone
    labelList faces_;

    //- List of fluid cells owner of the zone faces
    labelList cells_;

    //- Reference to the solid finite volume mesh (for cht)
    const fvMesh& sMesh_;

    //- Name of the solid face zone (for cht)

    ...
}
```

Reference to the
fluid mesh and
definition of the
connectivity

Reference to the
solid mesh and
definition of the
connectivity

The reactingWashcoatZone

The generic `washcoatZone` is extended to `reactingWashcoatZone` in order to model surface reactions:

```
class reactingWashcoatZone
:
    public washcoatZone
{
    // Private data

    //- Disallow default bitwise copy construct
    reactingWashcoatZone(const reactingWashcoatZone&);

    //- Disallow default bitwise assignment
    void operator=(const reactingWashcoatZone&);

    //- Washcoat solver
    autoPtr<Foam::washcoat::washcoatSolver> wsctSolver_;

    ...
}
```

Washcoat solver is
run-time selectable

Washcoat solver is based on 3 run-time selectable sub-models:

- Diffusion
- Reactions
- Heat transfer

Specialization of the washcoatSolver

- On the basis of the `washcoatSolver` class, different solvers can be implemented and chosen at runtime. For example:

```
template<class MassMdl, class ReacMdl, class HeatMdl>
class BaruahWashcoatSolver
:
    public washcoatSolver,
    public MassMdl,
    public ReacMdl,
    public HeatMdl
{
    ...
}
```

The solver is derived from `washcoatSolver` and templated submodels for the diffusion, reaction and heat-transfer

`BaruahWashcoatSolver` is derived from templated submodels which are run-time selectable:

- MassMdl** : generic model for the diffusion between the fluid and the substrate
- ReacMdl** : generic model for the surface reactions
- HeatMdl** : generic model for the heat release and heat transfer

```
washcoatSolver BaruahWashcoatSolver<constantWsctMassDiffusionModel,
                                     infinitelyFastWsctChemistryModel,
                                     laminarWsctHeatTransferModel>;
```

```
washcoatSolver singleStepWashcoatSolver<constantWsctMassDiffusionModel,
                                         infinitelyFastWsctChemistryModel,
                                         laminarWsctHeatTransferModel>;
```

The washcoat dictionary

```
/*-----*- C++ -*-----*\
|=====|
|  \ \ / F i e l d | OpenFOAM: The Open Source CFD Toolbox |
|  \ \ / O p e r a t i o n | Version: 2.1.x |
|  \ \ / A n d | Web: www.OpenFOAM.org |
|  \ \ / M a n i p u l a t i o n | |
\*-----*/
FoamFile
{
    version      2.0;
    format       ascii;
    class        dictionary;
    location     "constant";
    object       washcoats;
}
// ***** //
```

2 Number of washcoat zones

```
(
    washcoat0
    {
        washcoatSolver BaruahWashcoatSolver<detailedWsctMassDiffusionModel,
                                           infinitelyFastWsctChemistryModel,
                                           laminarWsctHeatTransferModel>;
    }
}
```

Washcoat solver

The washcoat dictionary

```
2  
(  
  washcoat0  
  {  
    ...  
  
    wsctProperties  
    {  
      loading loading [ 1 -2 0 0 0 0 0 ] 0.16;  
      specificSurface specificSurface [ 0 0 0 0 0 0 0 ] 1;  
      thickness thickness [ 0 1 0 0 0 0 0 ] 1.0e-6;  
      porosity porosity [ 0 0 0 0 0 0 0 ] 0.5;  
      rho rho [1 -3 0 0 0 0 0] 2800;  
      Cp Cp [0 2 -2 -1 0 0 0] 897;  
      K K [1 1 -3 -1 0 0 0] 150;  
    }  
  }  
)
```

Washcoat
properties

```
  thermoType  
  {  
    type heWsctThermo;  
    mixture wsctSingleStepReactingMixture;  
    transport constIso;  
    thermo hConst;  
    energy sensibleEnthalpy;  
    equationOfState rhoConst;  
    specie specie;  
  }  
  ...  
)
```

Thermodynamic
model

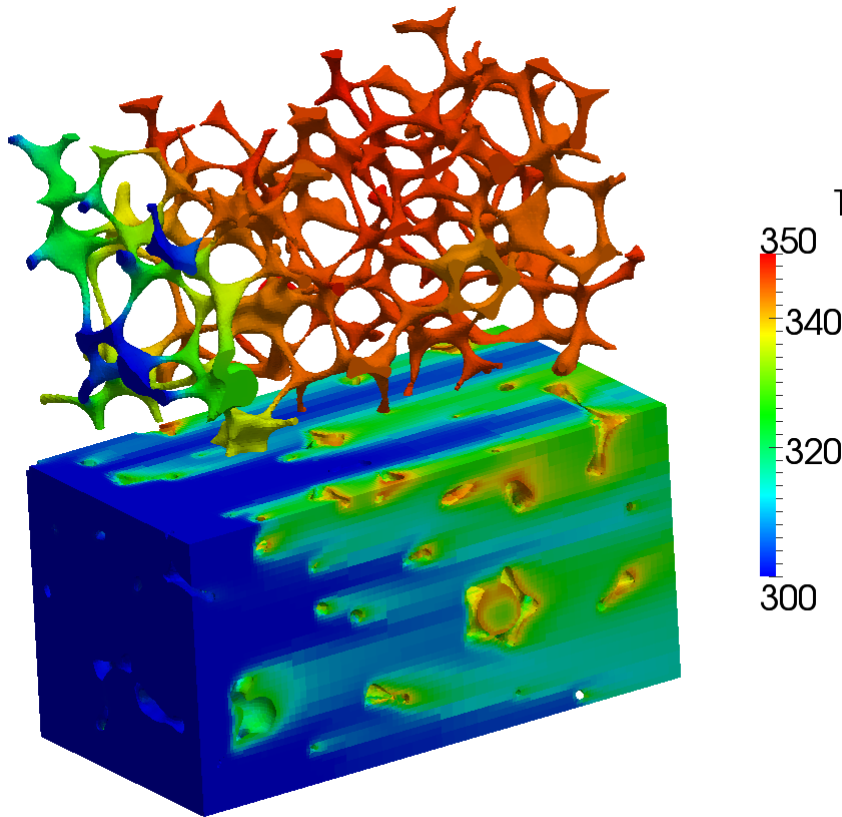
The washcoat dictionary

```
2
(  
  washcoat0  
  {  
    ...  
    species  
    (  
      O2  
      H2O  
      CH4  
      CO2  
      N2  
    );  
    inertSpecie N2;  
    fuel CH4;  
  
    wsctChemistryReader wsctFoamChemistryReader;  
    foamChemistryFile "$FOAM_CASE/constant/wsctReactions.wall1";  
    foamChemistryThermoFile "$FOAM_CASE/constant/thermo.wsct";  
    ...  
  }  
)
```

Species involved in the surface reactions

Reacting flow simulation

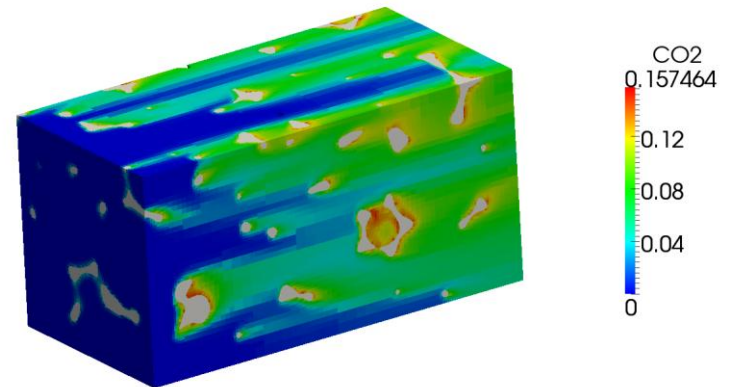
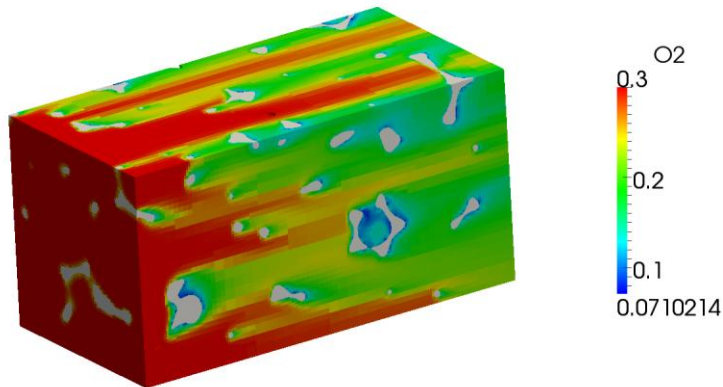
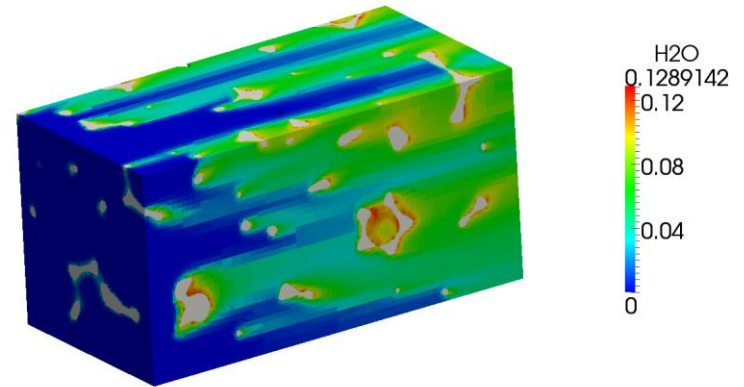
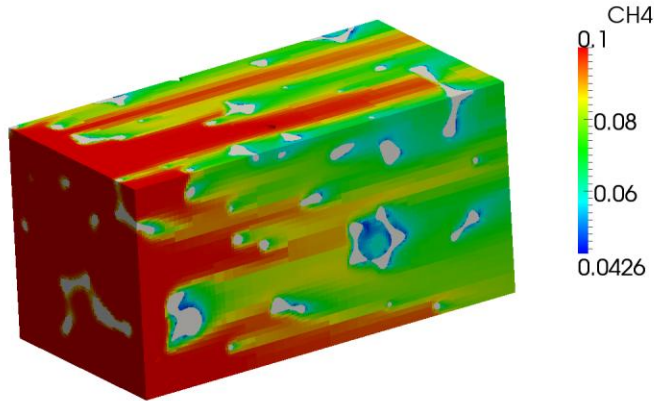
Al foam 95% porosity – 40 ppi / Micro-CT reconstruction



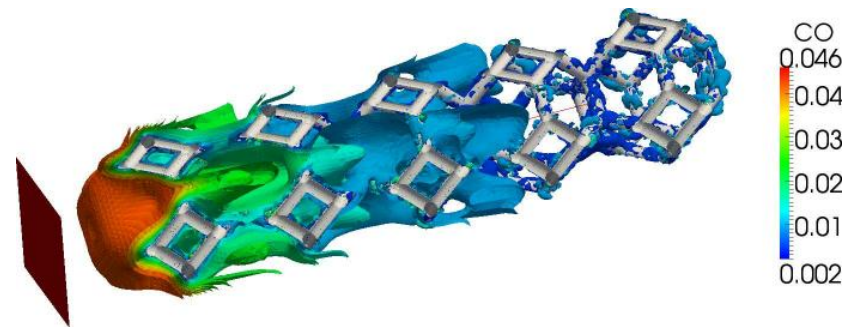
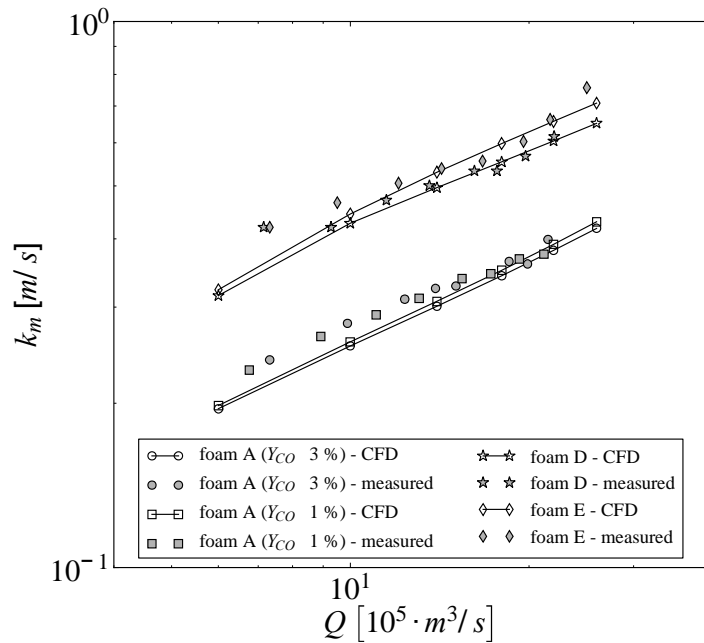
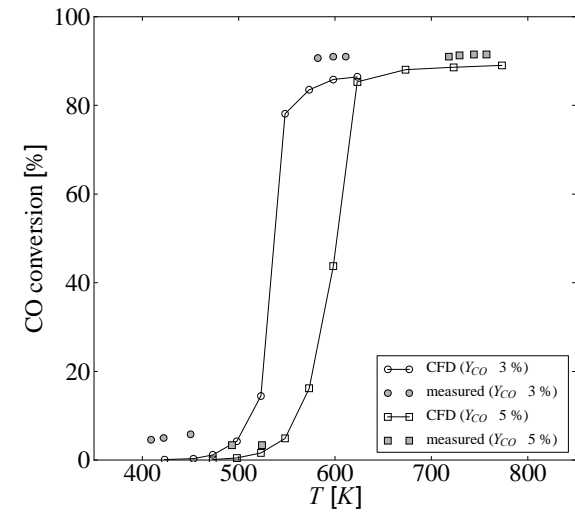
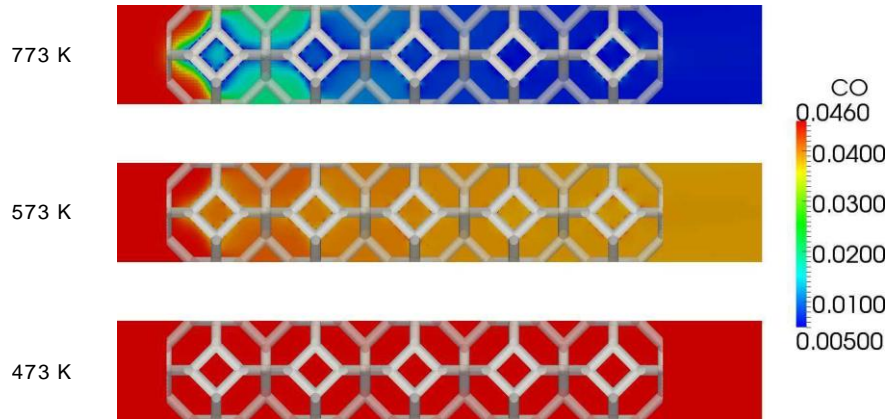
- Surface reaction on washcoat region
- Baruah-like solver
- Infinitely fast reaction model
- Conjugate heat transfer
- Fluid: inlet $T=300\text{K}$
- Solid: fixed $T=300\text{K}$ on the inlet side, adiabatic elsewhere

Reacting flow simulation

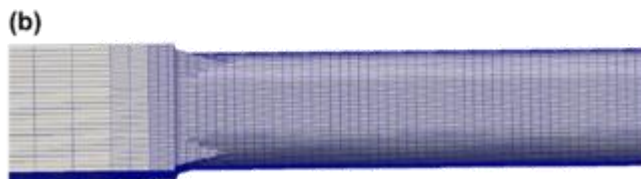
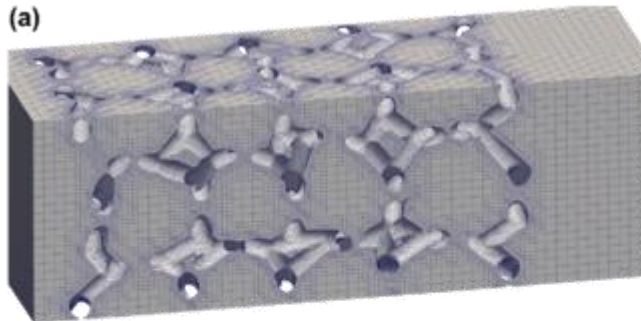
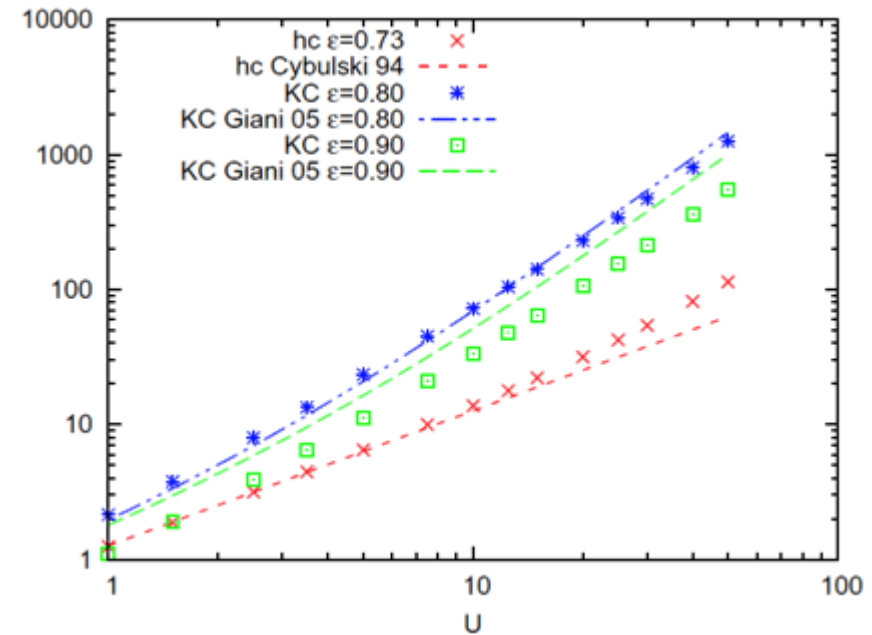
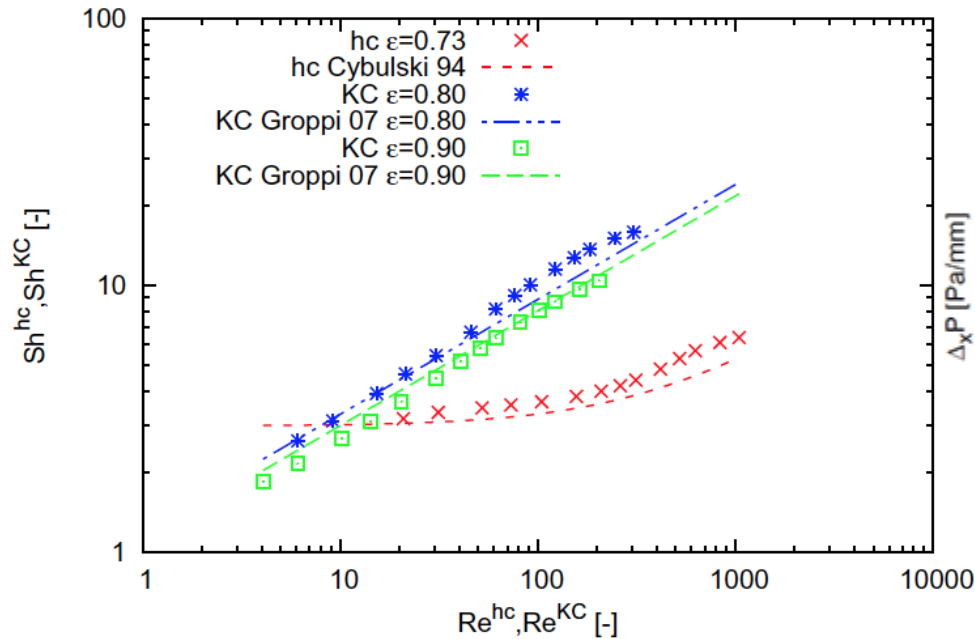
Al foam 95% porosity – 40 ppi / Micro-CT reconstruction



Diffusion limit validation

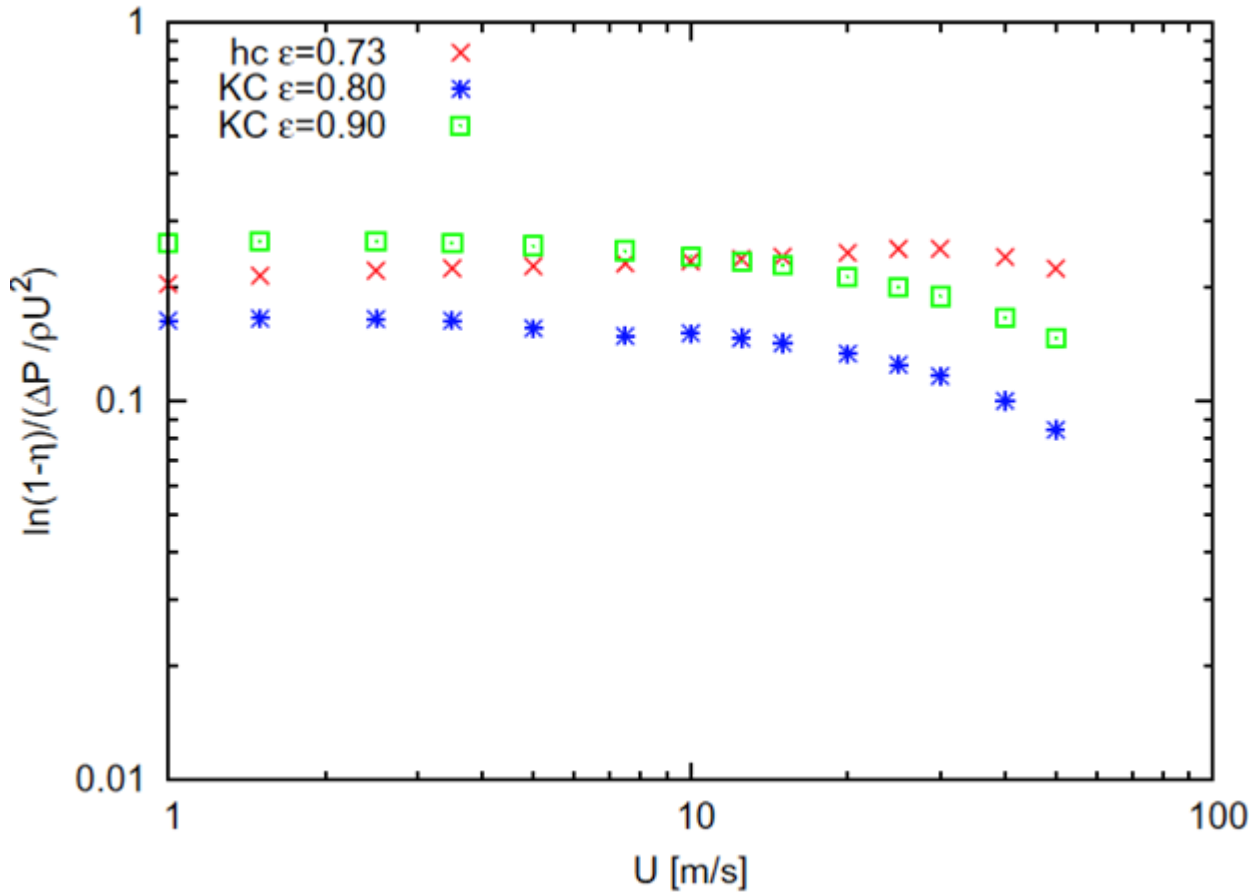


KC vs honeycomb



- The results of simulations compare fairly well with the correlations available in the literature
- There is still not agreement among authors in literature

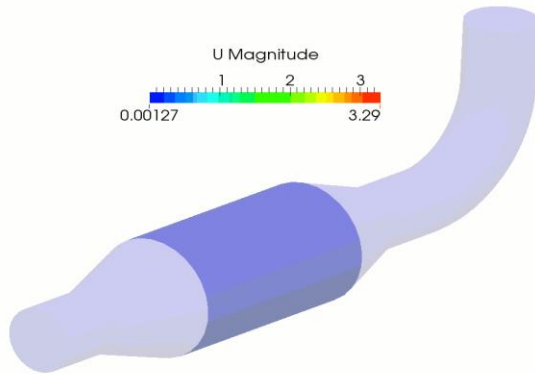
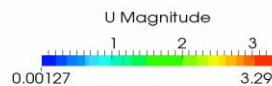
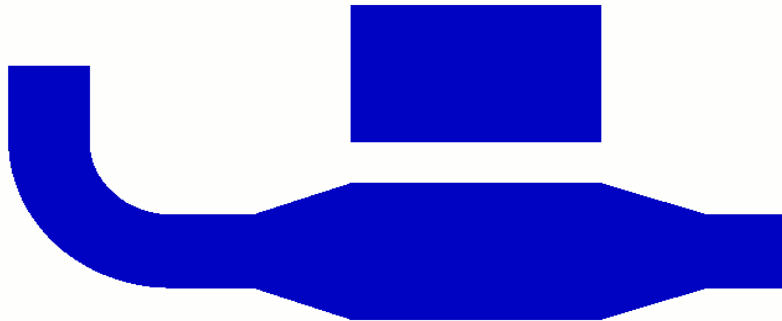
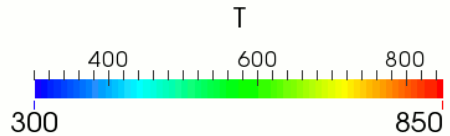
Performance Index: KC vs honeycomb



$$I = \frac{-\ln(1 - \eta)}{\Delta P / (\rho u^2)}$$

- The open cell foam exhibit a better performance if:
 - porosity is high
 - velocity is low (Darcean velocity)

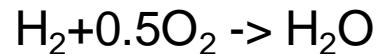
Application example: TWC



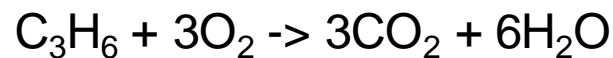
CO oxidation



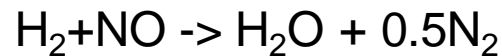
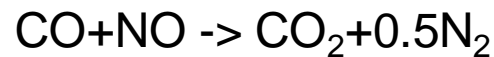
H₂ oxidation



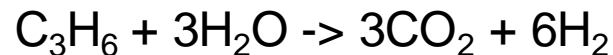
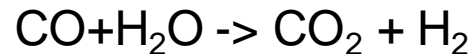
HC oxidation



NO_x reduction

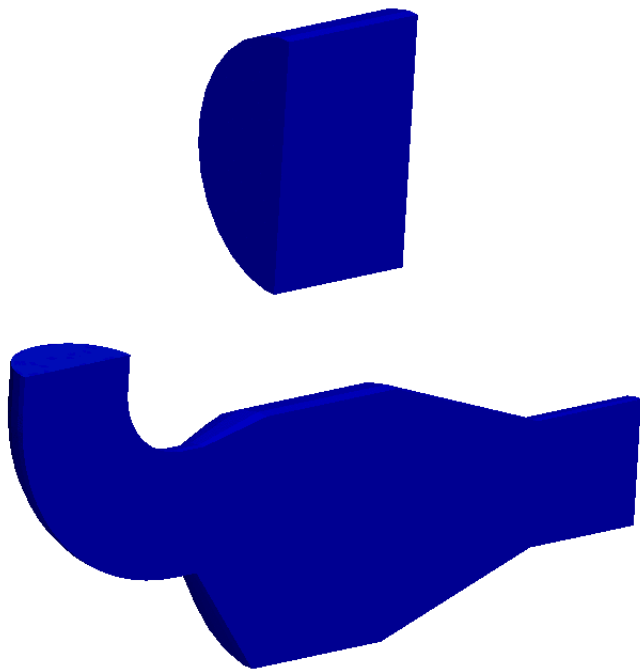


Steam water reforming



Full scale: honeycomb vs open cell foam

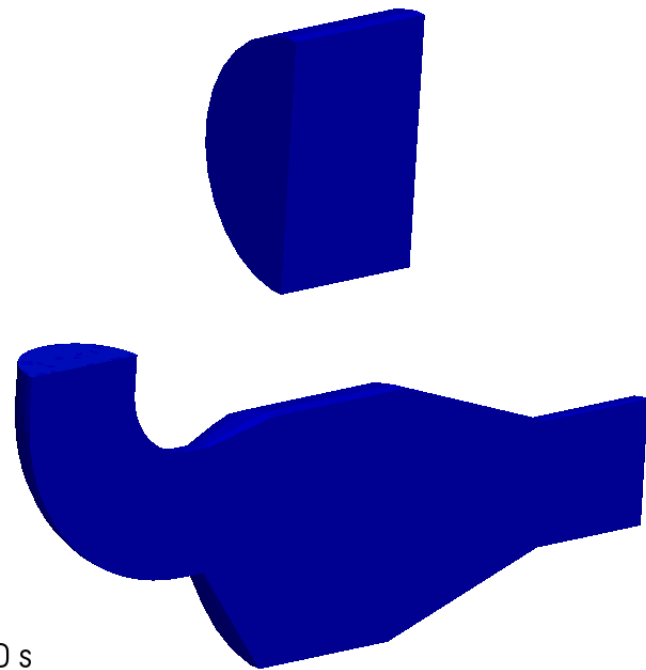
NEDC cycle of a 2.0 L engine (4 Cyl, naturally aspirated) simulated imposing the measured exhaust gas T and mass flow at the engine flange.



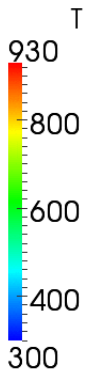
HONEYCOMB



Time: 0 s

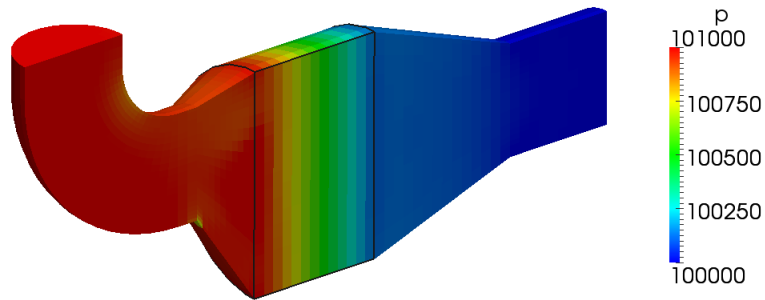
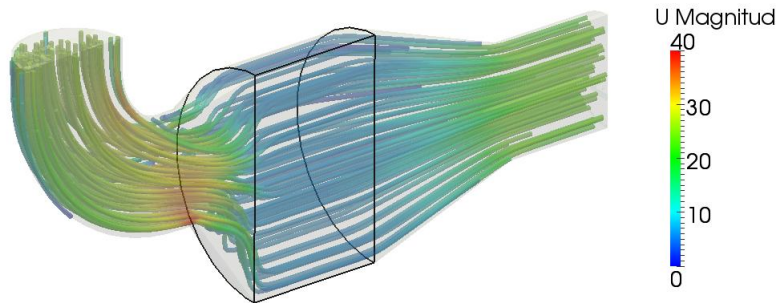


OPEN CELL FOAM

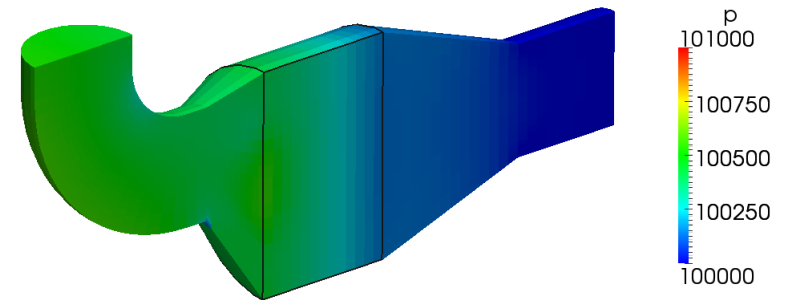
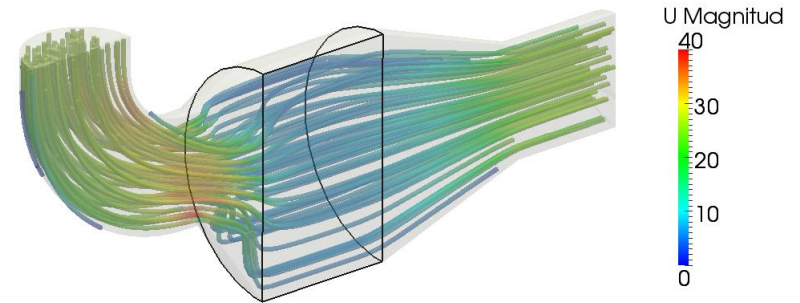


Full scale: honeycomb vs open cell foam

HONEYCOMB

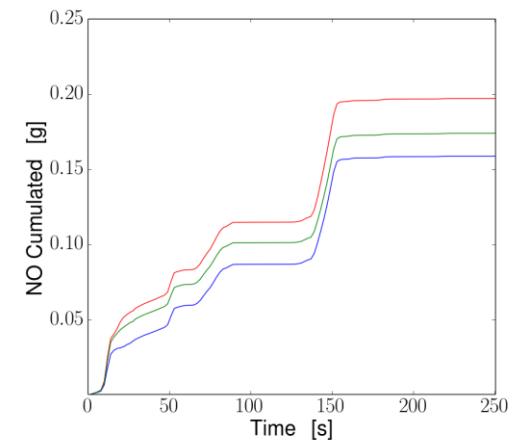
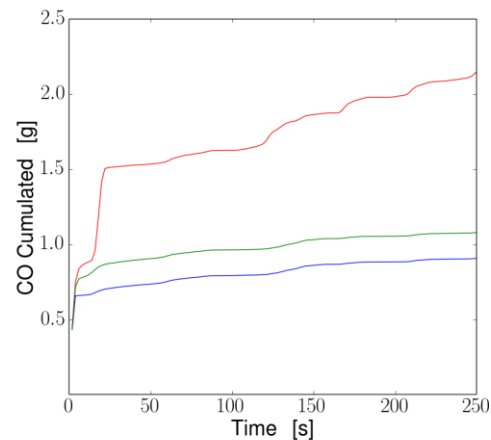
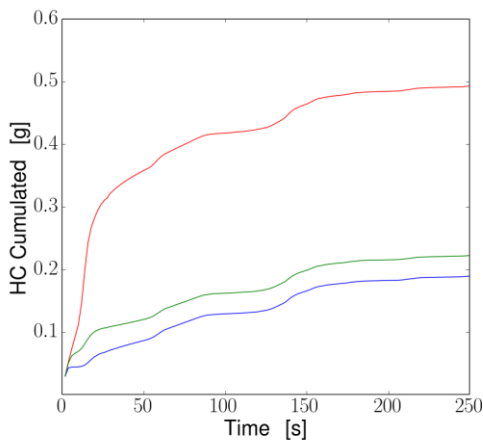
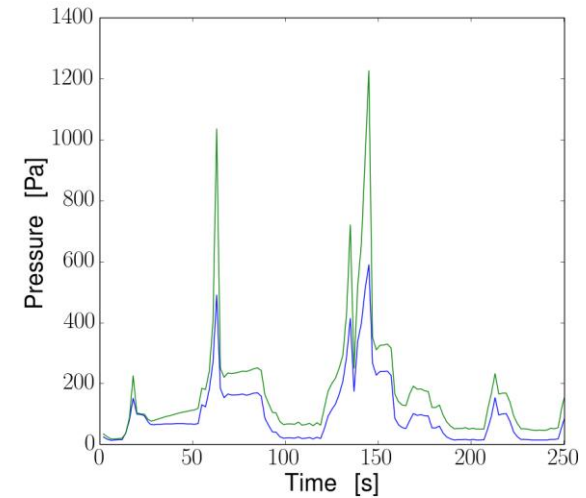
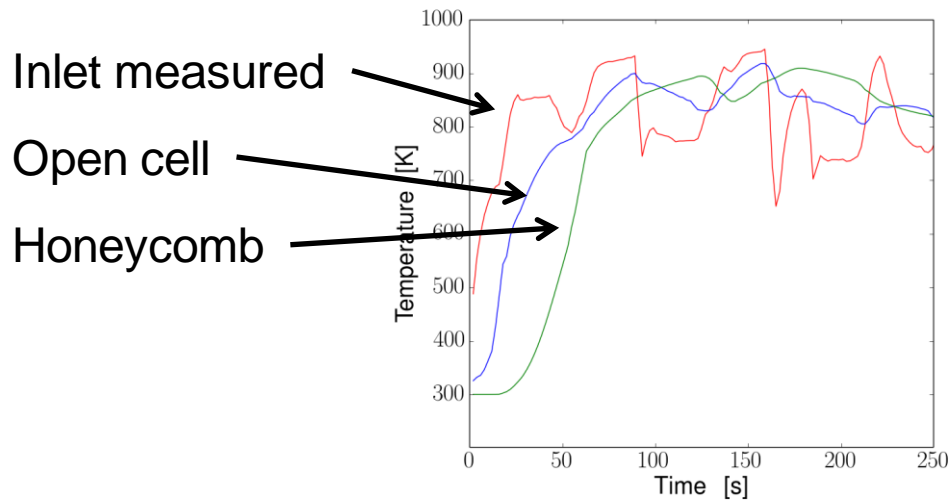


OPEN CELL FOAM



Full scale: honeycomb vs open cell foam

- NEDC cycle (first 300 seconds) with two different technologies

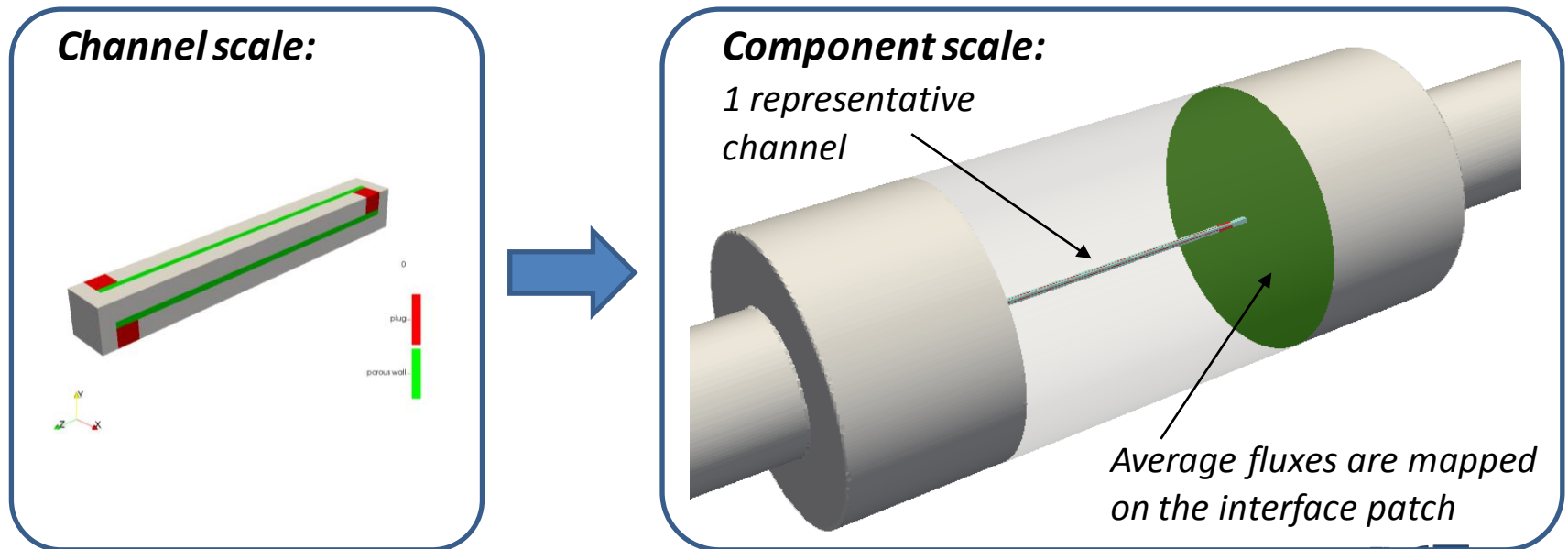


Conclusions and ... work in progress

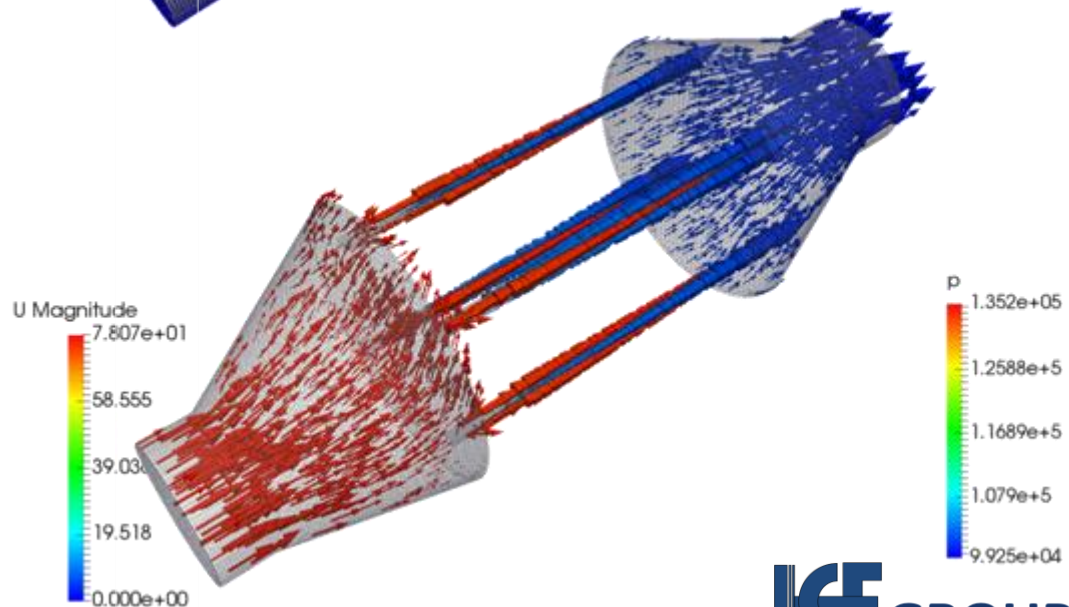
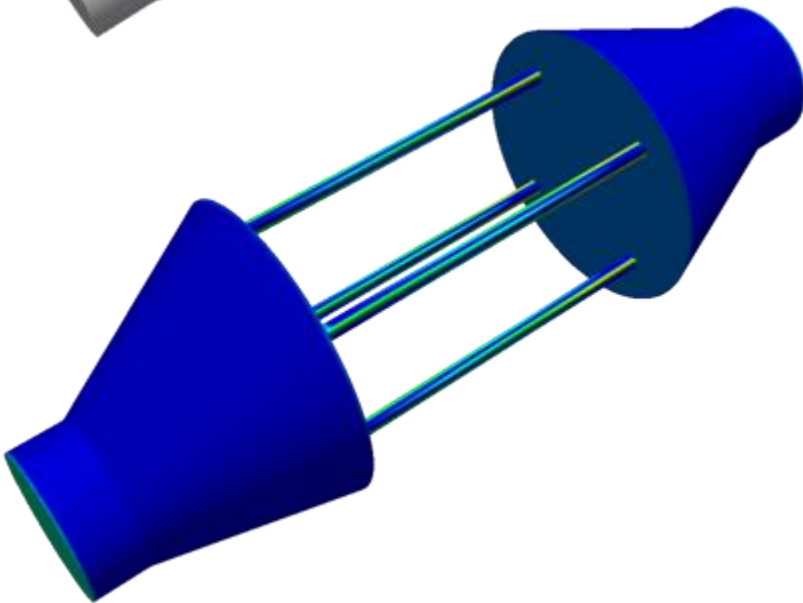
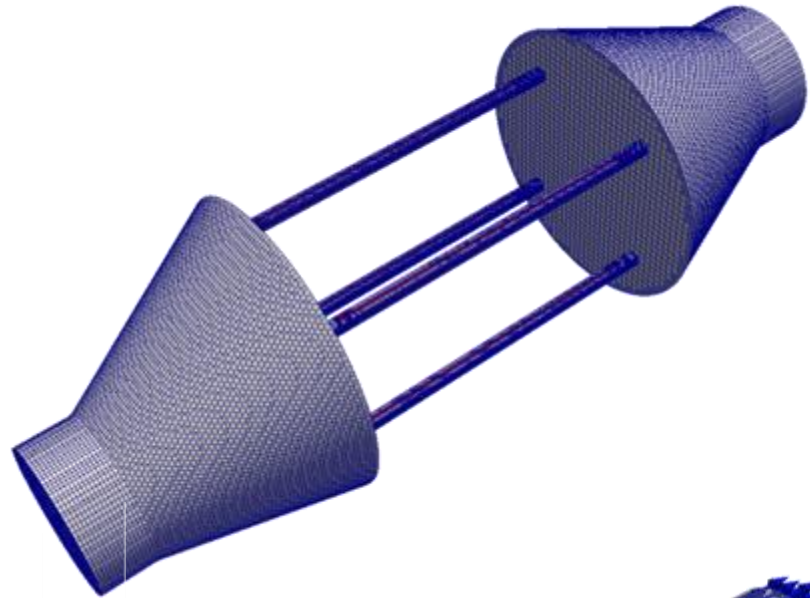
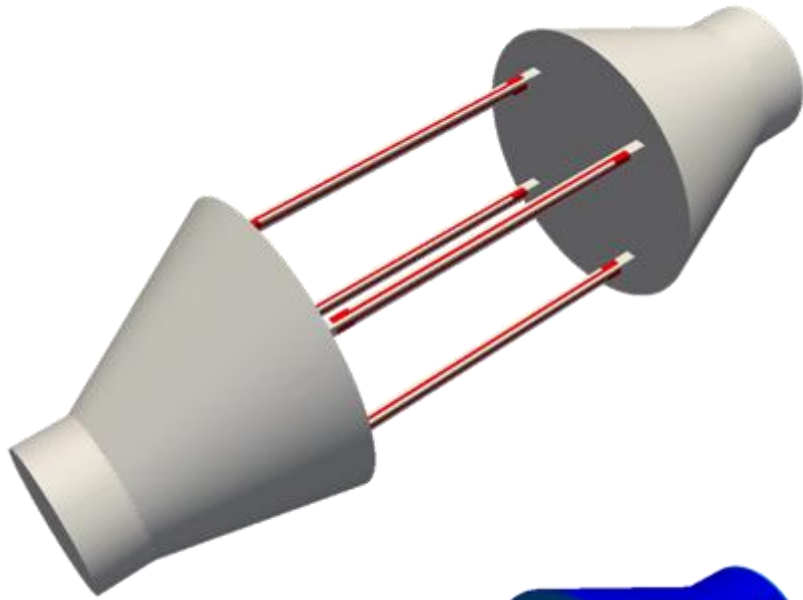
- ✧ Implementation of a fully coupled surface reacting model applicable to microstructure or channel scale simulations
- ✧ Averaging techniques have made possible full scale simulations in a consistent way with the microscale approach
- ✧ Full scale simulation of open cell substrates are fundamental to better understand the effectiveness of a solution with respect to a consolidated technology

WIP: Channel scale DPF/GPF or CAT

- The monolith is divided in sectors and where fluid-dynamic equations are solved on a single representative couple of channels.
- Fluxes are mapped on the remaining portion of the sector not connected to the representative channel.



WIP: Channel scale DPF/GPF or CAT



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- Prof. Gavin Tabor
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