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INDEPENDENT RESEARCH

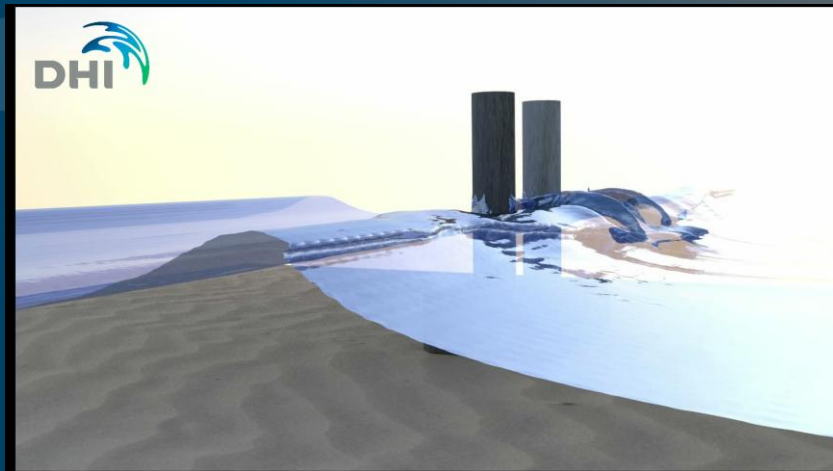
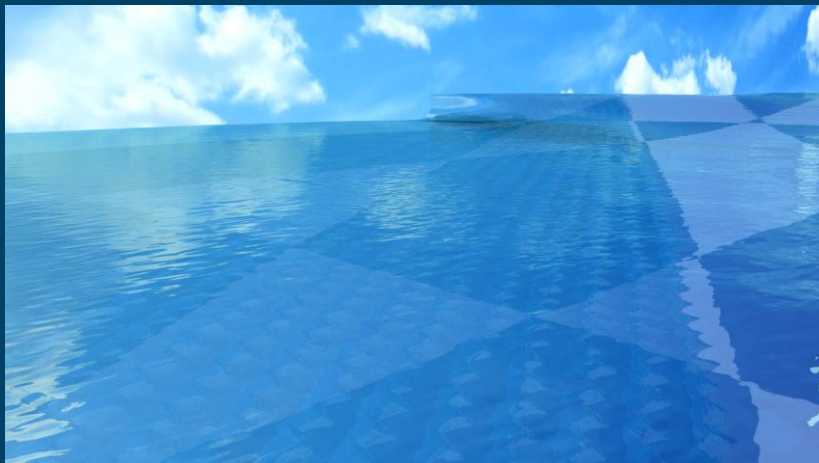
IsoAdvect

A new geometric VOF method for arbitrary meshes

Johan Rønby, Ports & Offshore Technology, DHI
Henrik Bredmose, DTU Wind Energy, Technical University of Denmark
Hrvoje Jasak, FSB, University of Zagreb

OFW11, June 26-30, Guimarães, Portugal

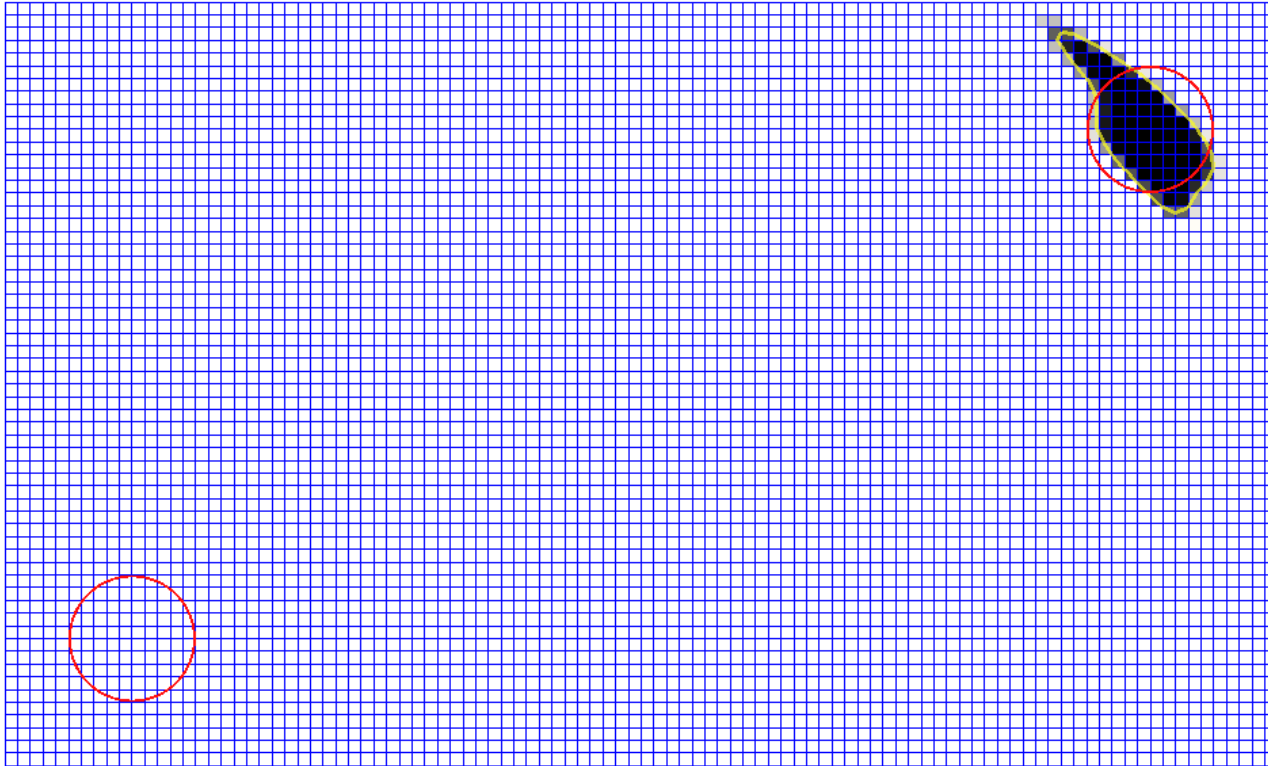




Our experience is that interFoam works well for waves but...

- Tends to give too large and too early wave breaking
- Produces spurious velocities at interface
- Requires very small time steps (CFL~0.1)
- Only converges slowly with mesh refinement

A simple VOF test



Disk advected in
velocity field
 $U = (1, 0.5)$

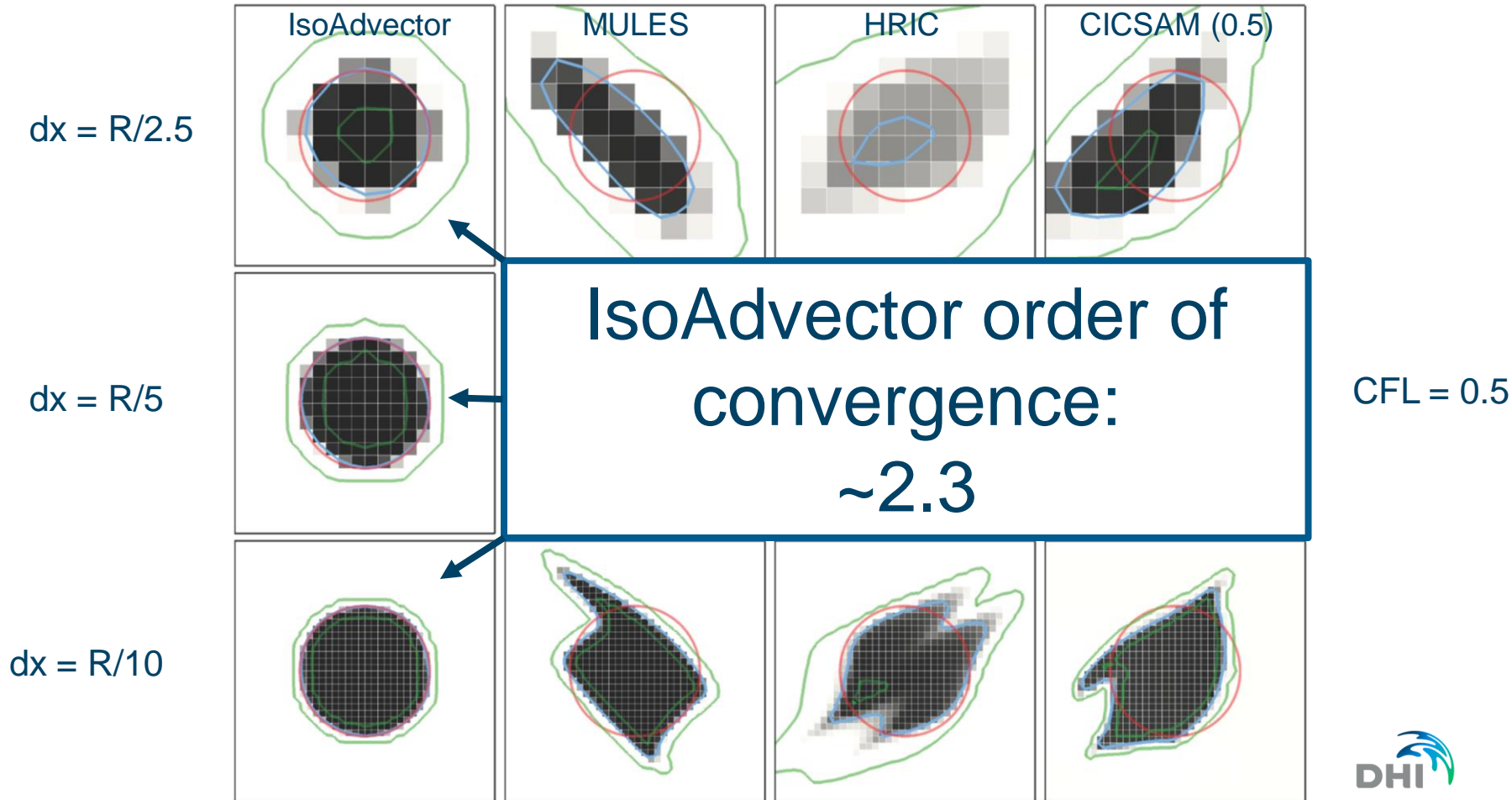
With MULES
(interFoam)

$CFL = 0.5$

...

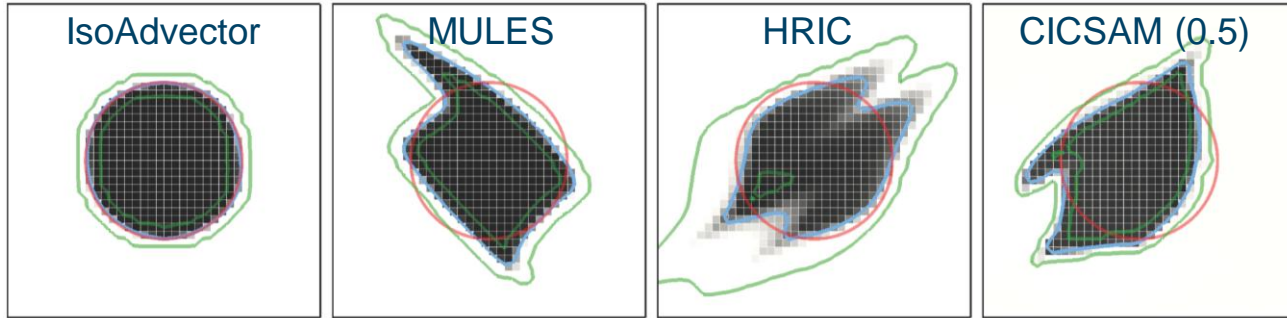
Very poor shape
preservation

Disc in uniform flow on hex mesh – refining mesh...

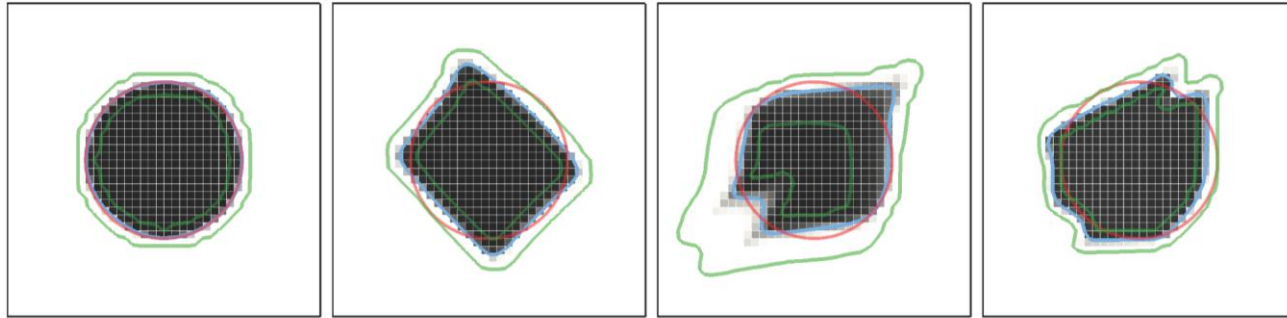


Disc in uniform flow on hex mesh – smaller time steps...

CFL = 0.5

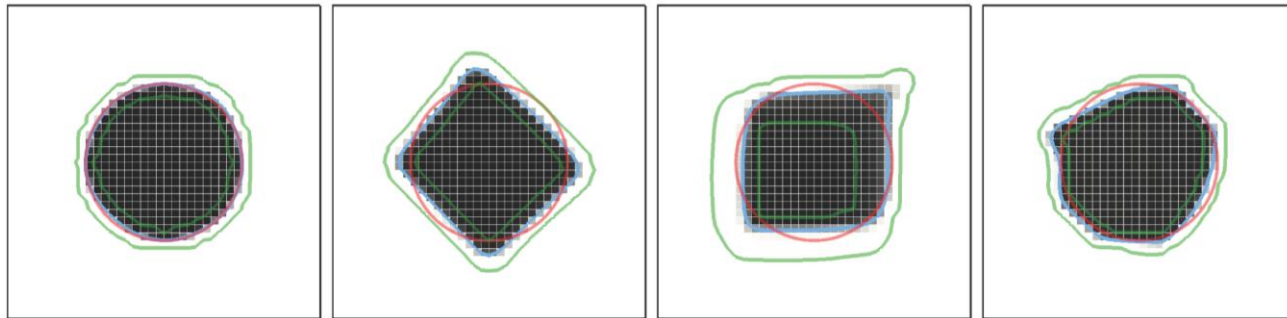


CFL = 0.2



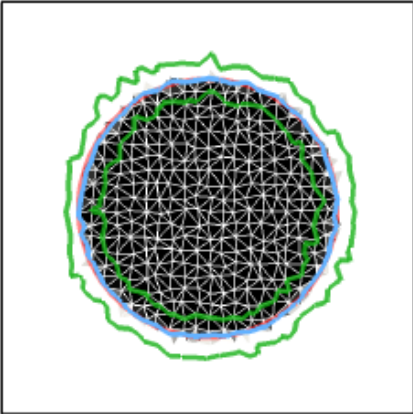
$dx = R/10$

CFL = 0.1

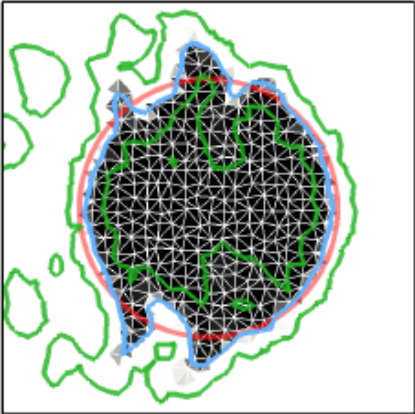


Unstructured meshes

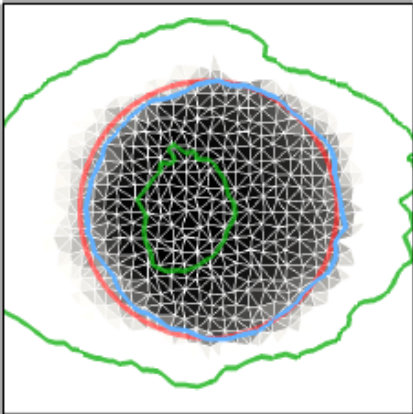
IsoAdvect



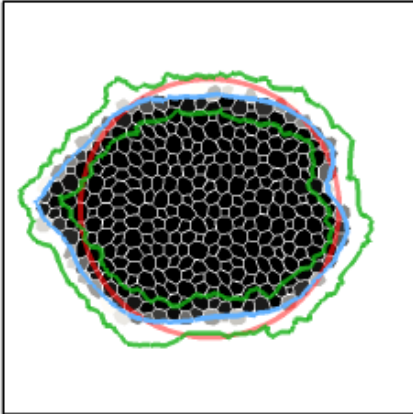
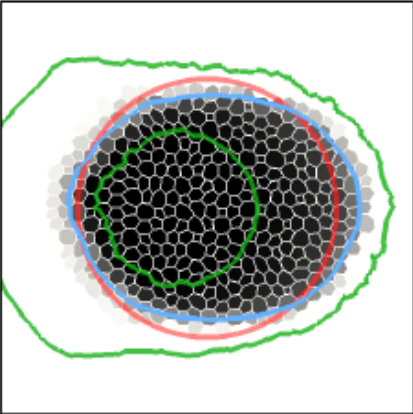
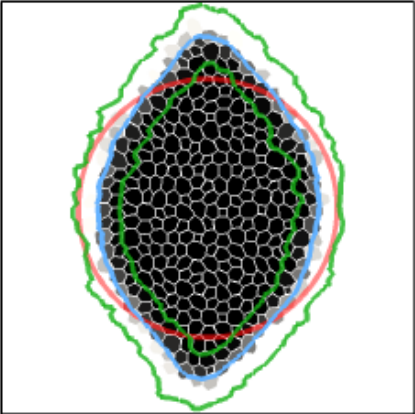
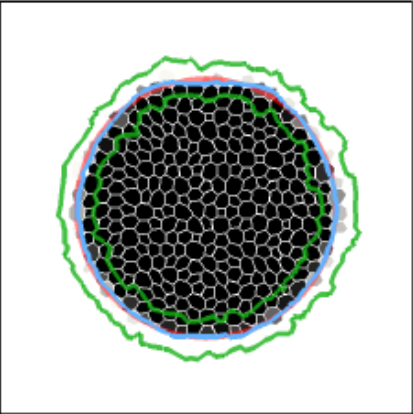
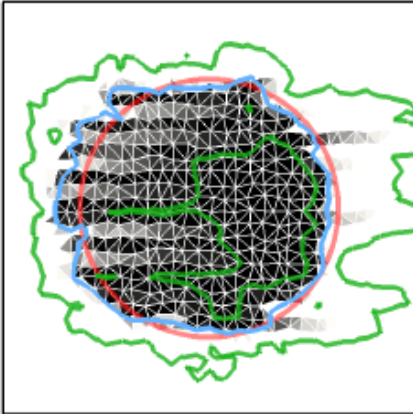
MULES



HRIC



CICSAM



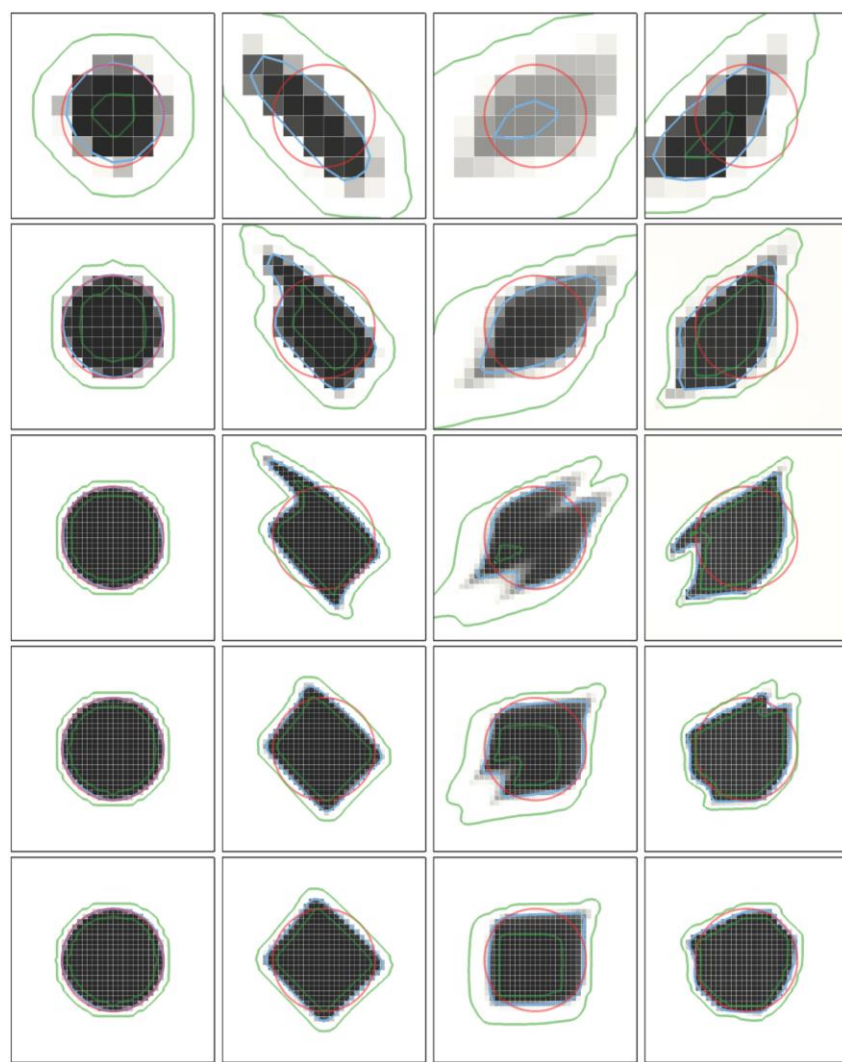
CFL = 0.5

Efficiency

Calculation times in seconds (1 core)

| (Nx,Co) | isoAdvect | MULES | HRIC | CICSAM |
|-----------|-----------|-------|-------|--------|
| (30,0.5) | 0.23 | 0.52 | 0.22 | 0.19 |
| (60,0.5) | 0.86 | 2.16 | 0.94 | 0.87 |
| (120,0.5) | 4.03 | 12.42 | 5.28 | 4.49 |
| (120,0.2) | 7.22 | 28.28 | 9.46 | 8.4 |
| (120,0.1) | 12.53 | 55.13 | 16.82 | 14.61 |

IsoAdvect is slightly faster than HRIC and CICSAM, and 2-4 times faster than MULES



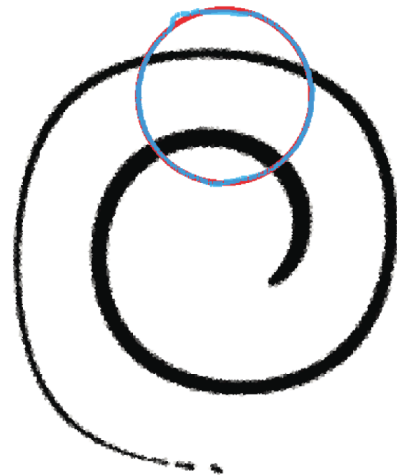
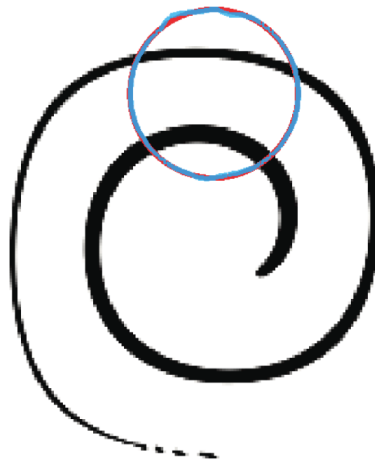
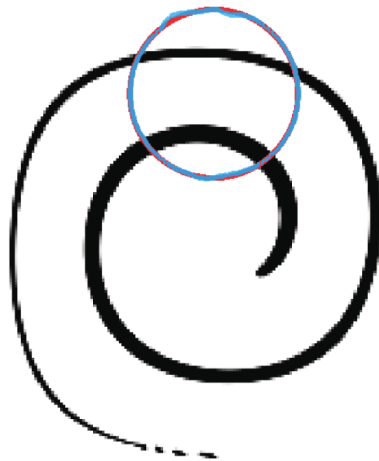
Spiralling Disk

Square cells

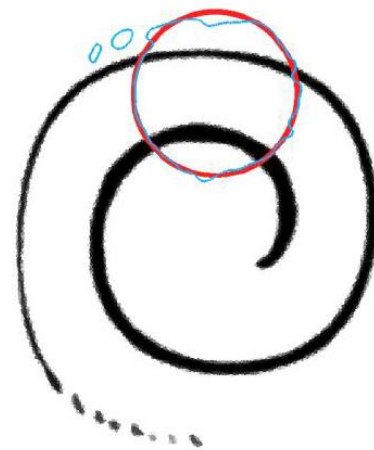
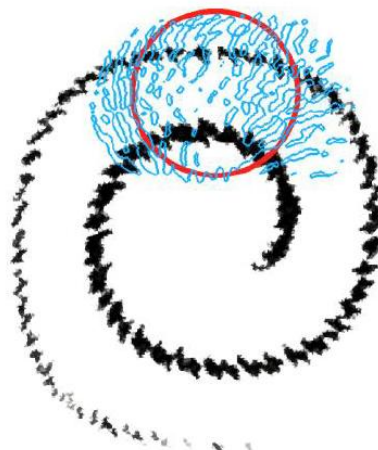
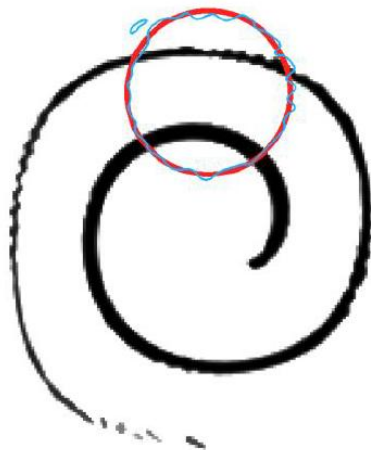
Triangular cells

Polygonal cells

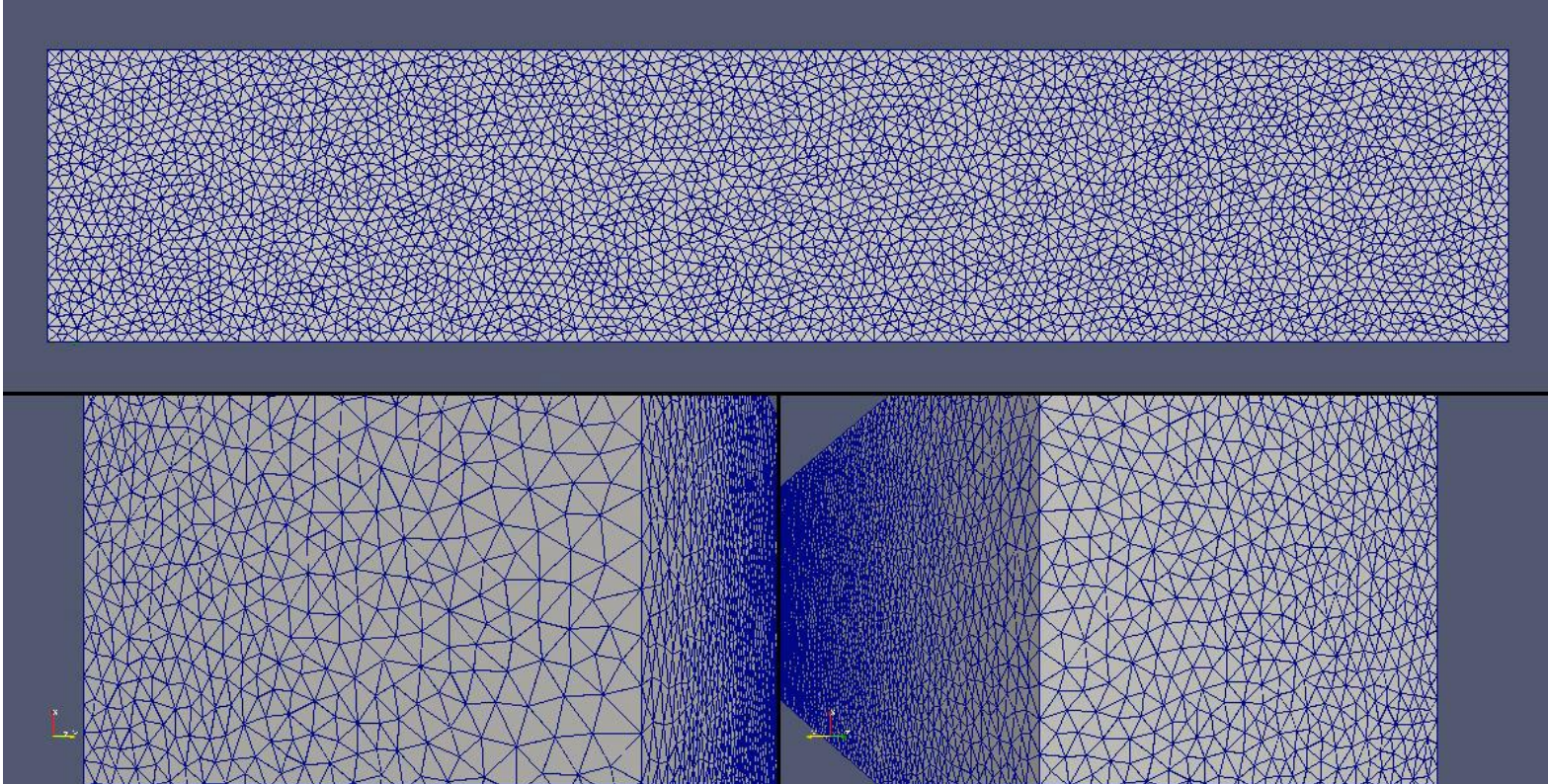
IsoAdvect, CFL = 0.5



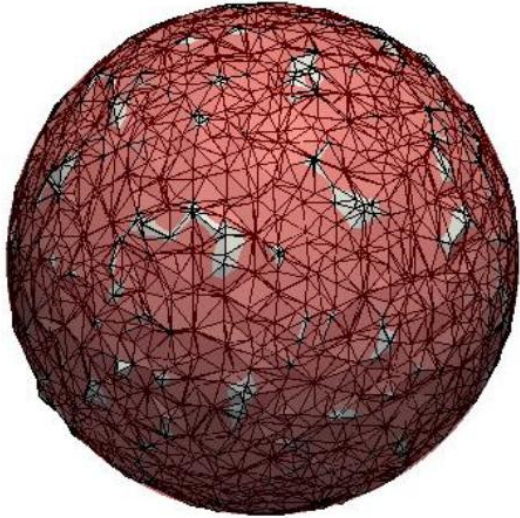
MULES, CFL = 0.1



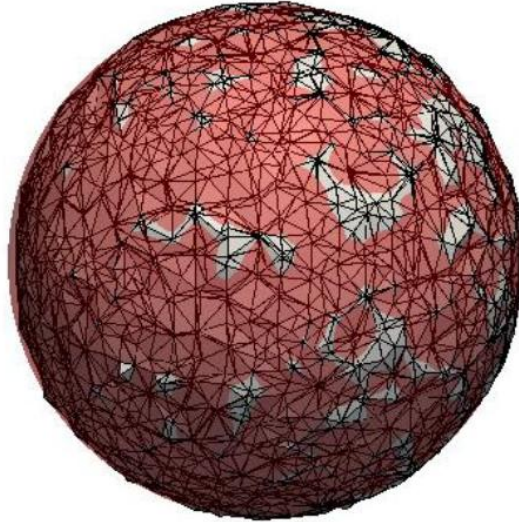
Sphere in uniform flow on random tet mesh



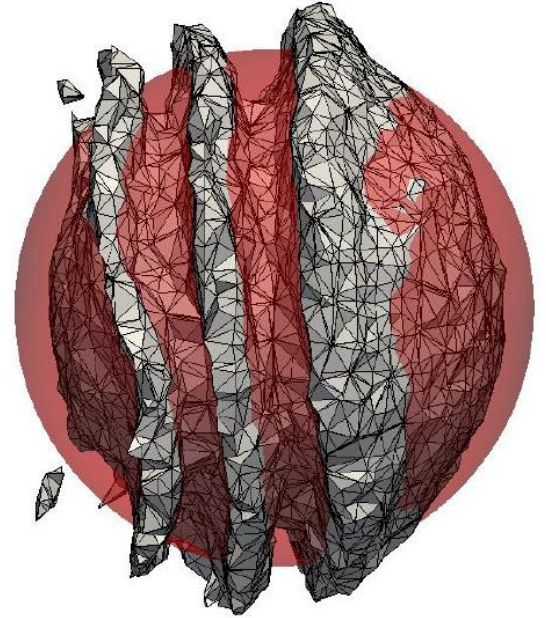
Sphere in uniform flow on random tet mesh



Exact

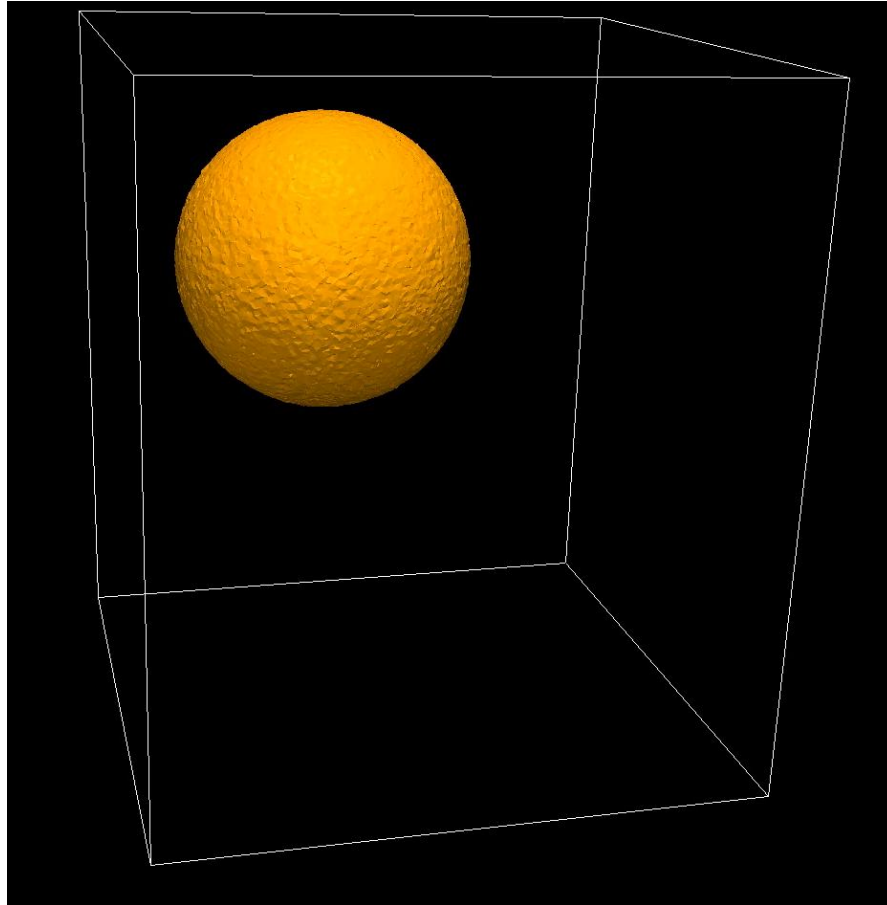


IsoAdvectored



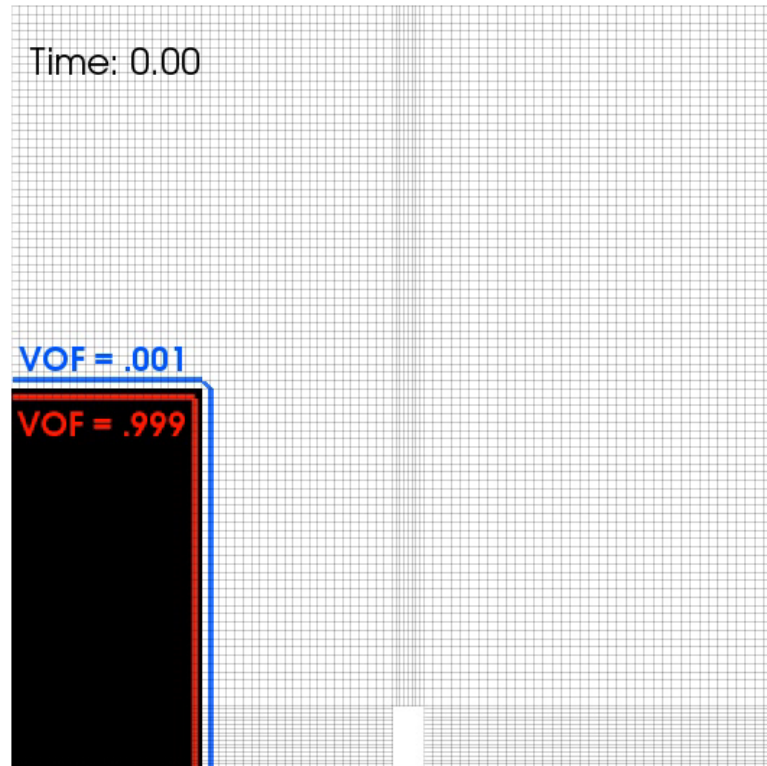
MULES

Sphere in non-uniform 3D flow on random tet mesh

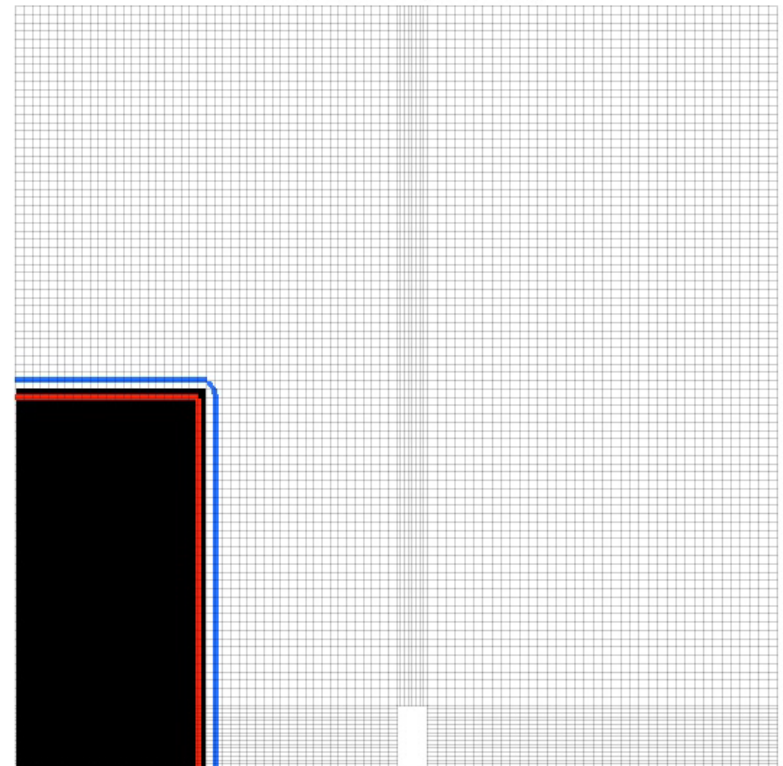


damBreak – IsoAdvectord versus MULES

"interFlow" (IsoAdvectord)

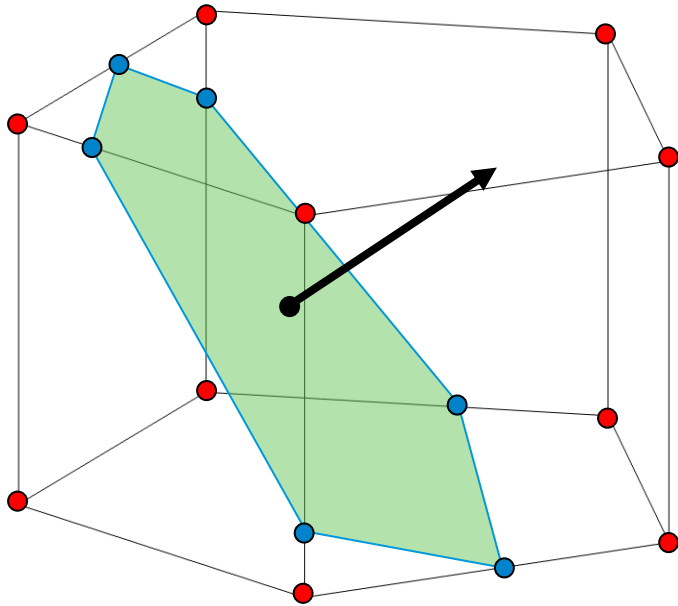


interFoam (MULES)

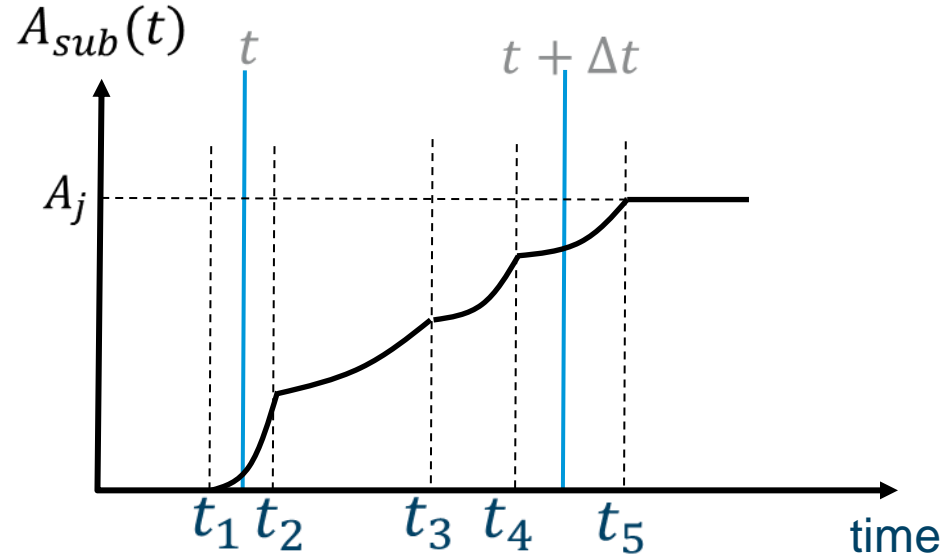
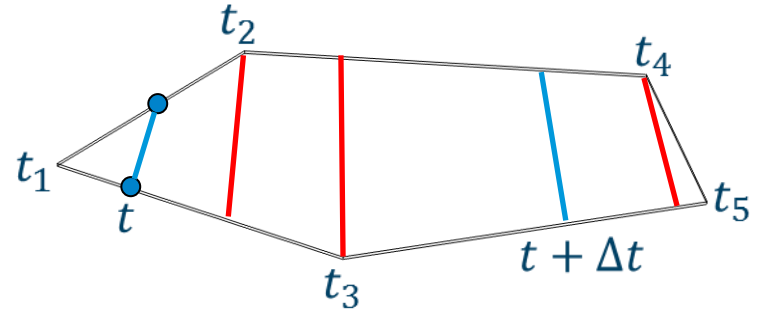


The IsoAdvect concept

Idea 1: The *isoface*



Idea 2: The *face-interface intersection line*



IsoAdvectord summary

- Explicit geometric VOF scheme for interface advection on arbitrary meshes
- Beats MULES and other algebraic VOF schemes both on accuracy and speed
- Code will be available on github.com soon
- Implementation in your own `interFoam` type solver is a one-liner (well, almost)
- Google "IsoAdvectord" to find RSOS preprint on arxiv.org and youtube channel

Thank you



Zalesak's (notched) disk

CFL = 0.1



CFL = 0.5



CFL = 1.0



CFL = 1.5



$dV = -7.7e-11\%$

$dV = -2.2e-08\%$

$dV = 2.7e-06\%$

$dV = 0.00012\%$

E1 = 3.5%

E1 = 2.9%

E1 = 3.5%

E1 = 6.5%

Unbound = $8e-17$

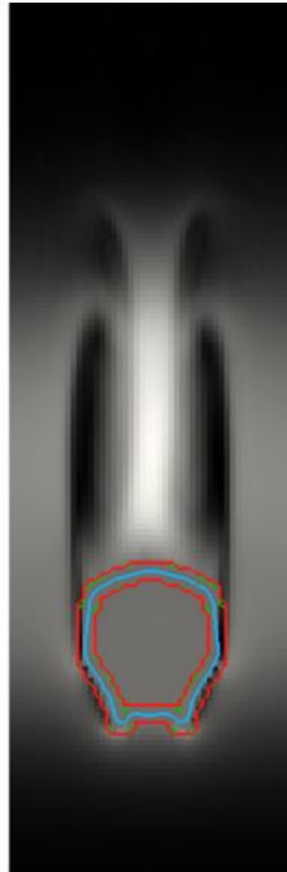
Unbound = $1.1e-16$

Unbound = $3.9e-08$

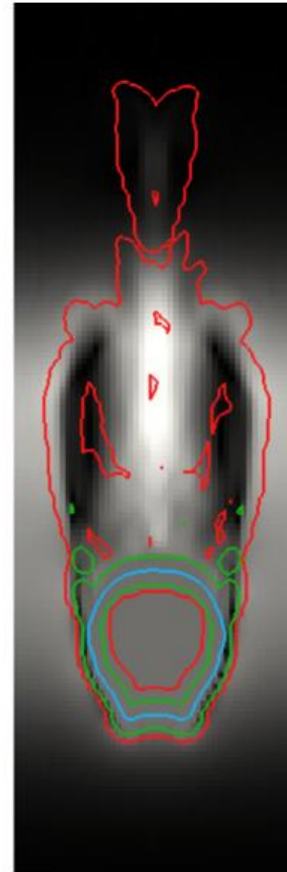
Unbound = $5.7e-09$

Water droplet falling in air

IsoAdvect



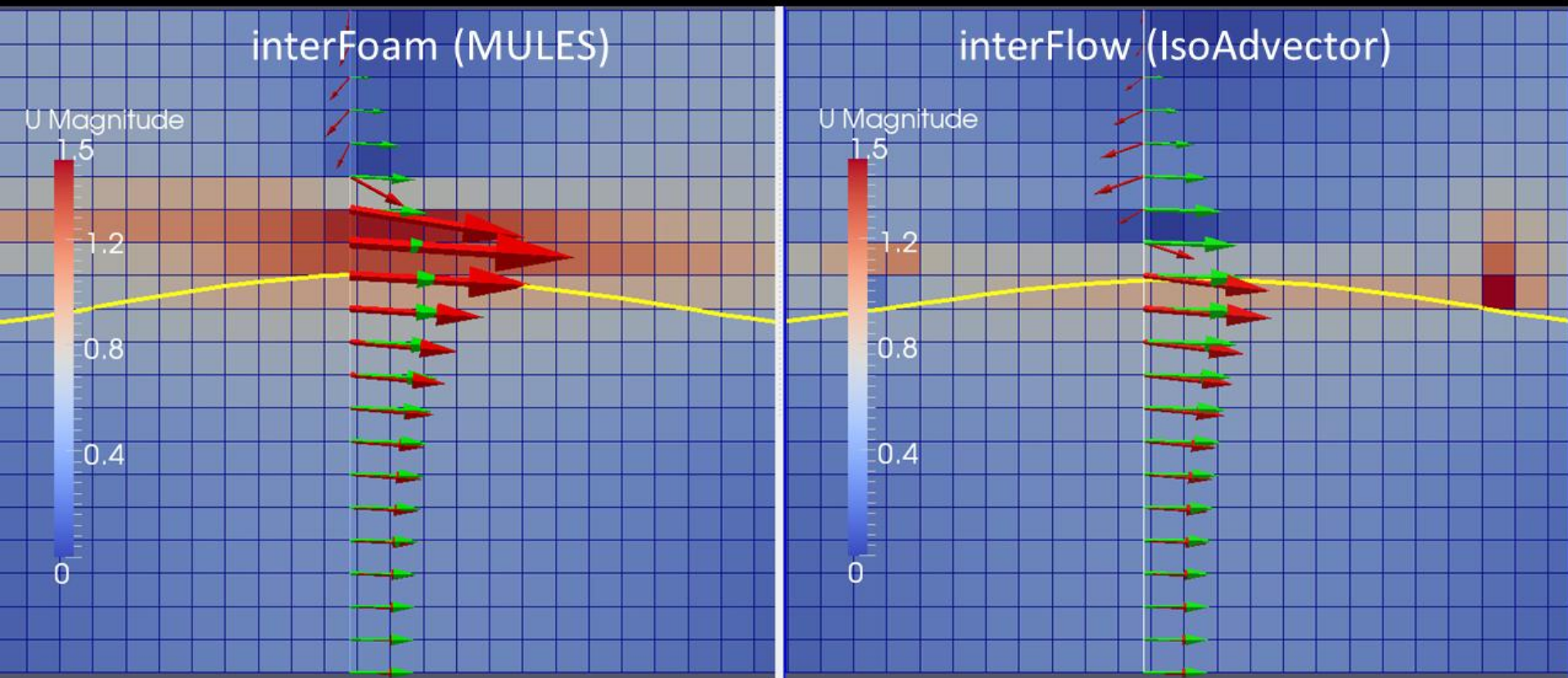
MULES



alpha1
contours:
1e-6
1e-3
0.5
1-1e-3
1-1e-6

U Magnitude
16,01372
16
12
8
4
7.564e-6

Velocity profile for stream function wave

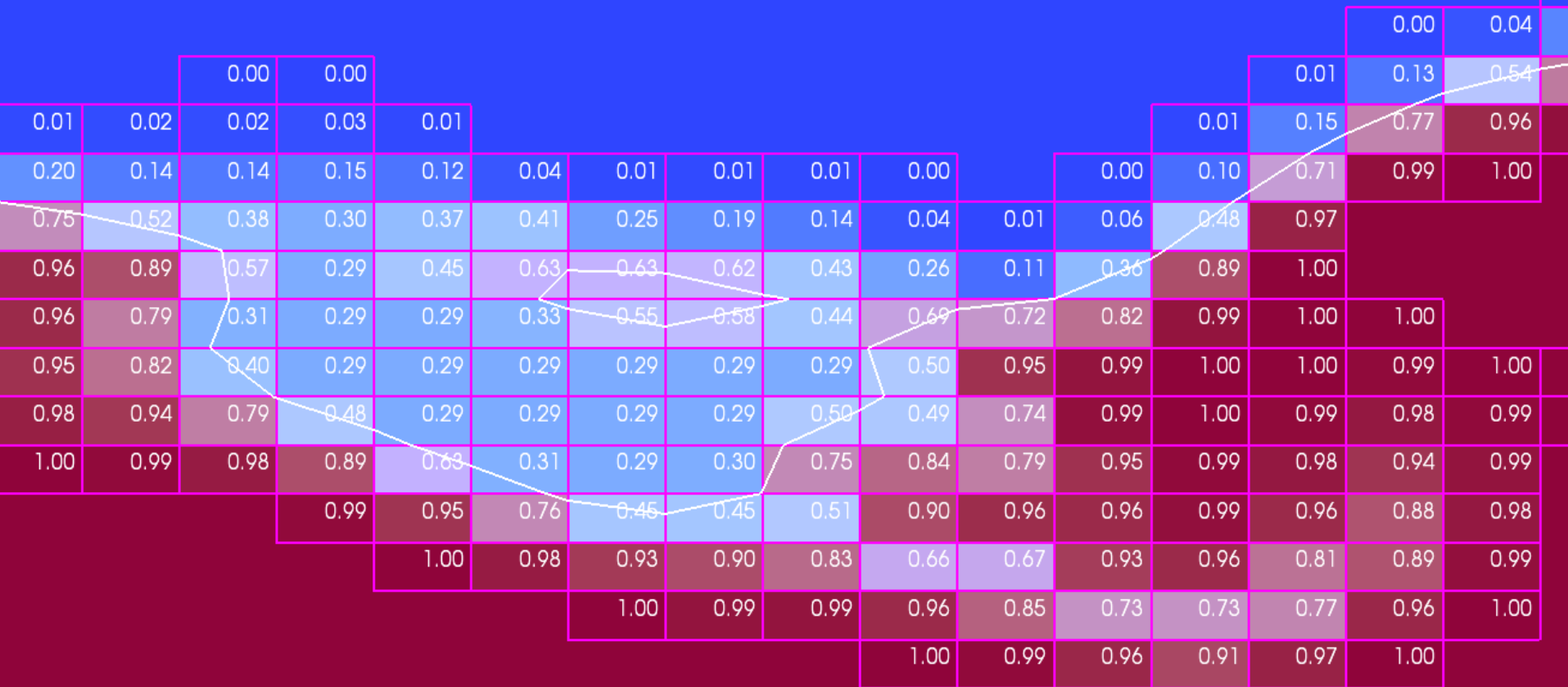


Green arrows: Theoretical profile. Red arrows: Actual profile. Yellow contour: Free surface.

Wave input: $D = 1\text{m}$, $H = 0.3\text{m}$, $T = 3\text{s}$

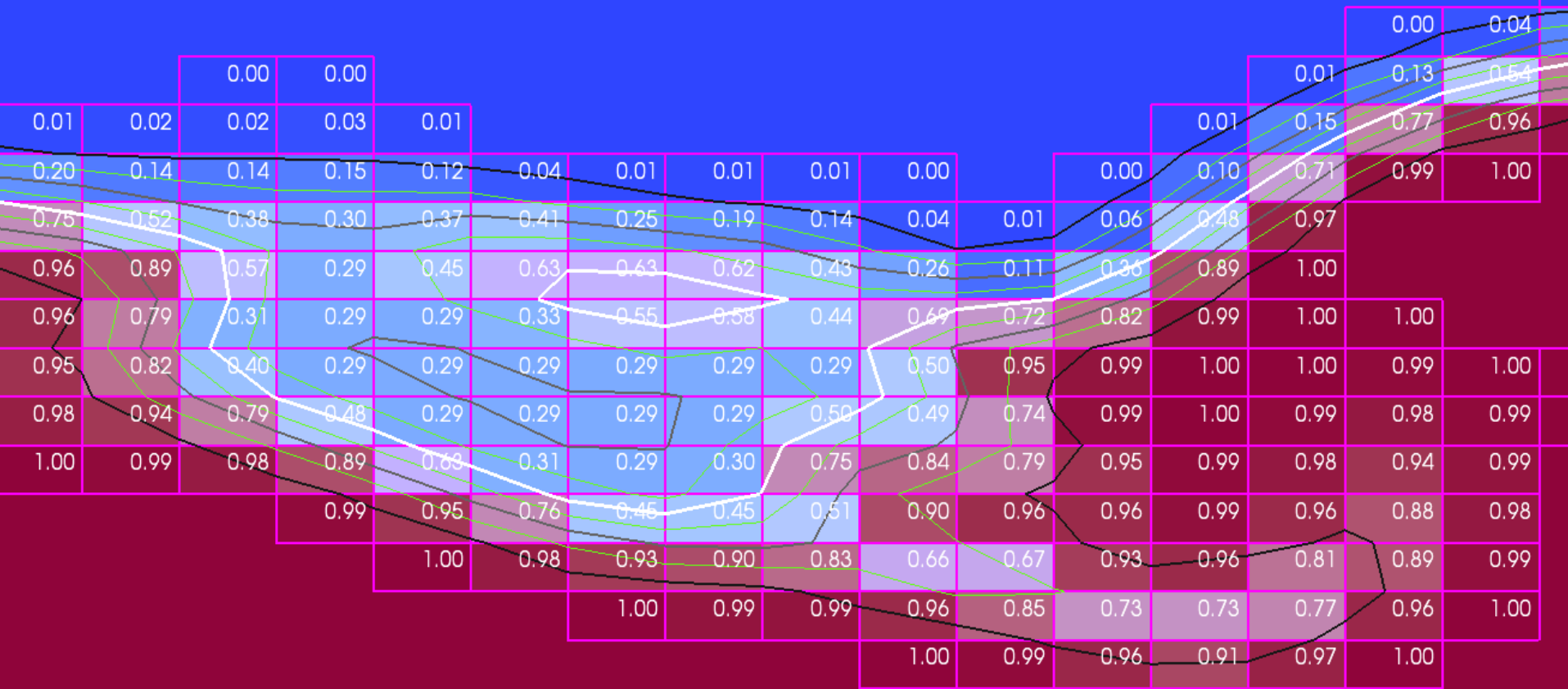
The IsoAdvecter concept

Idea for interface reconstruction from VOF data: Use isosurfaces



$\alpha = 0.5$ isosurface generally cuts cells incorrectly

But for each cell there is *some* isovalue cutting it correctly

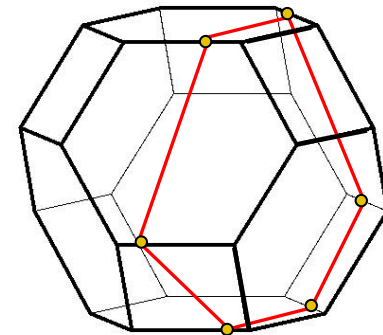
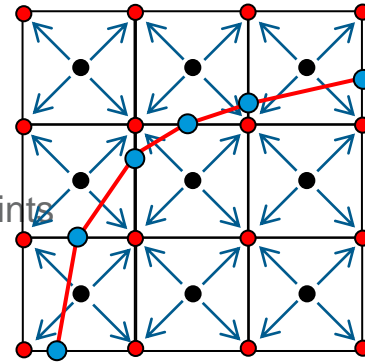


How to calculate an isosurface from volume fraction data?

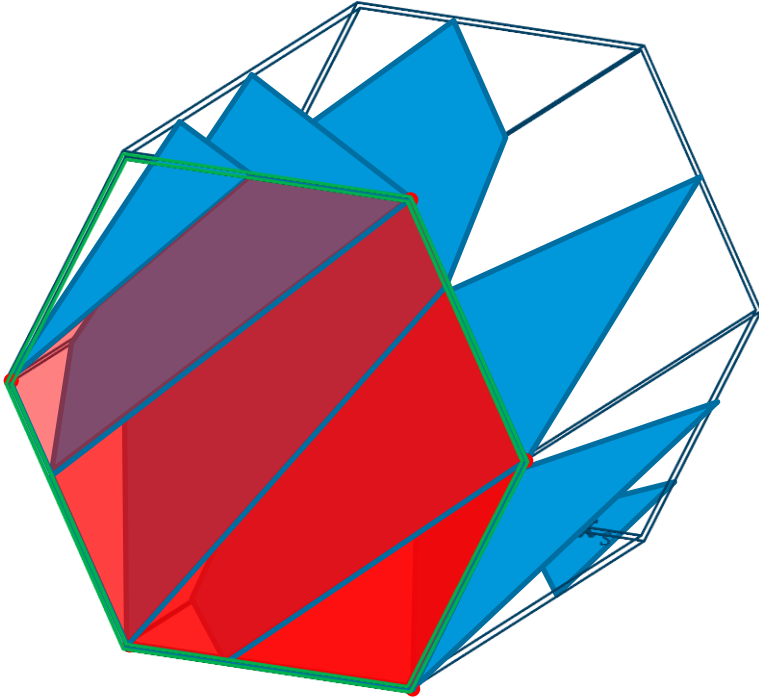
Steps:

1. Interpolate VOF cell data to *vertices*
2. For each *edge* find cutting point by linear interpolation using *isovalue*
3. For each cut cell form isosurface by connecting edge cutting points

Gives surface position and orientation inside cells on *arbitrary unstructured* 3D meshes



Estimating face-interface intersection line during time step



At time t cell i is a *surface cell* if $\epsilon < \alpha_i(t) < 1 - \epsilon$ (typically we use $\epsilon = 10^{-8}$).

We calculate its *isoface*, that is, the isosurface confined to the cell volume and with isovalue consistent with $\alpha_i(t)$.

This cell specific isovalue is currently found by binary search.

The isoface has a well-defined face centre, \mathbf{x}_s , and unit face normal, \mathbf{n}_s , together defining a plane.

We interpolate the velocity data, \mathbf{U} , to the isoface centre, \mathbf{x}_s , to get its velocity, $\mathbf{U}_s(t)$.

We dot $\mathbf{U}_s(t)$ with the isoface unit normal, \mathbf{n}_s , to get the isoface velocity normal to itself, $U_n = \mathbf{U}_s \cdot \mathbf{n}_s$.

Now for every vertex, \mathbf{x}_v , of every a face we can estimate the interface time of arrival as $t_v = (\mathbf{x}_v - \mathbf{x}_s) \cdot \mathbf{n}_s / U_n$.

The submerged face area

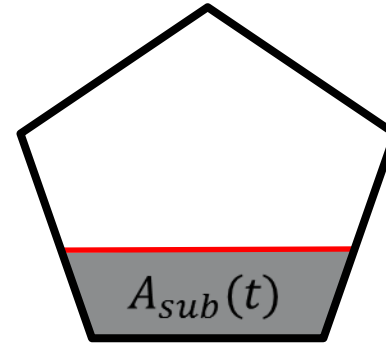
$$\Delta V_j(t, \Delta t) \equiv \int_t^{t+\Delta t} \int_{F_j} I(\mathbf{x}, \tau) \mathbf{U}(\mathbf{x}, \tau) \cdot d\mathbf{S} d\tau \approx \frac{\phi_j(t)}{|\mathbf{S}_j|} \int_t^{t+\Delta t} A_{sub}(\tau) d\tau$$

Volumetric face flux:

$$\phi_j(t) \equiv \int_{F_j} \mathbf{U}(\mathbf{x}, t) \cdot d\mathbf{S}$$

Submerged face area

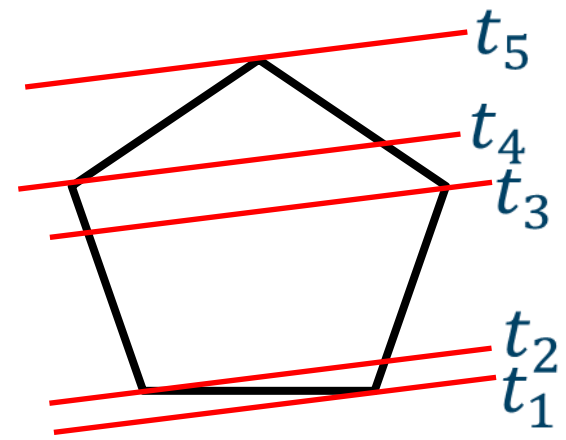
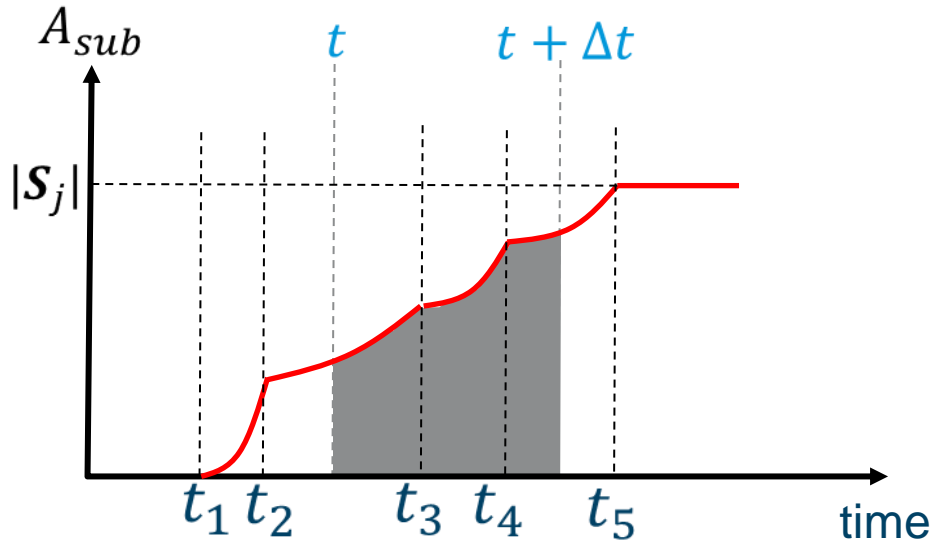
$$A_{sub}(t) \equiv \int_{F_j} I(\mathbf{x}, t) dA$$



Face F_j

Time integrated submerged face area

$$\Delta V_j(t, \Delta t) \approx \frac{\phi_j(t)}{|S_j|} \int_t^{t+\Delta t} A_{sub}(\tau) d\tau$$



We estimated $F_j \cap S(t)$ lines at vertex intersection times t_1, t_2, t_3, \dots

Assume steady line motion in between

Then in sub time intervals

$A_{sub}(\tau) = a\tau^2 + b\tau + c$
with a, b, c given by vertices.

Analytical time integral!

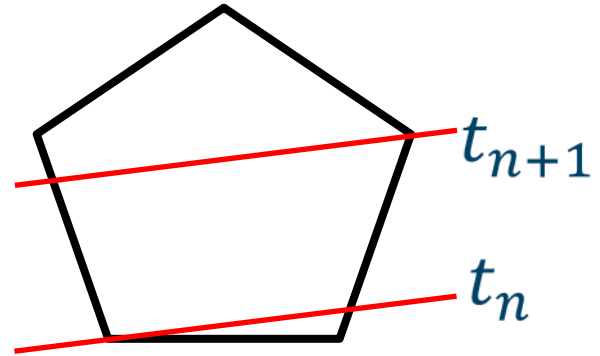
IsoAdvect concept summary

$$\alpha_i(t + \Delta t) = \alpha_i(t) - \frac{1}{V_i} \sum_{F_j \in \partial C_i} \Delta V_j(t, \Delta t)$$

$$\Delta V_j(t, \Delta t) \equiv \int_t^{t+\Delta t} \int_{F_j} I(\mathbf{x}, \tau) \mathbf{U}(\mathbf{x}, \tau) \cdot d\mathbf{S} d\tau$$

$$\approx \frac{\phi_j(t)}{|S_j|} \int_t^{t+\Delta t} A_{sub}(\tau) d\tau$$

$$\approx \frac{\phi_j(t)}{|S_j|} \sum_{n=1}^{M-1} \left[\frac{1}{3} a_n \tau^3 + \frac{1}{2} b_n \tau^2 + c_n \tau \right]_{\tau = t_n}^{t_{n+1}}$$



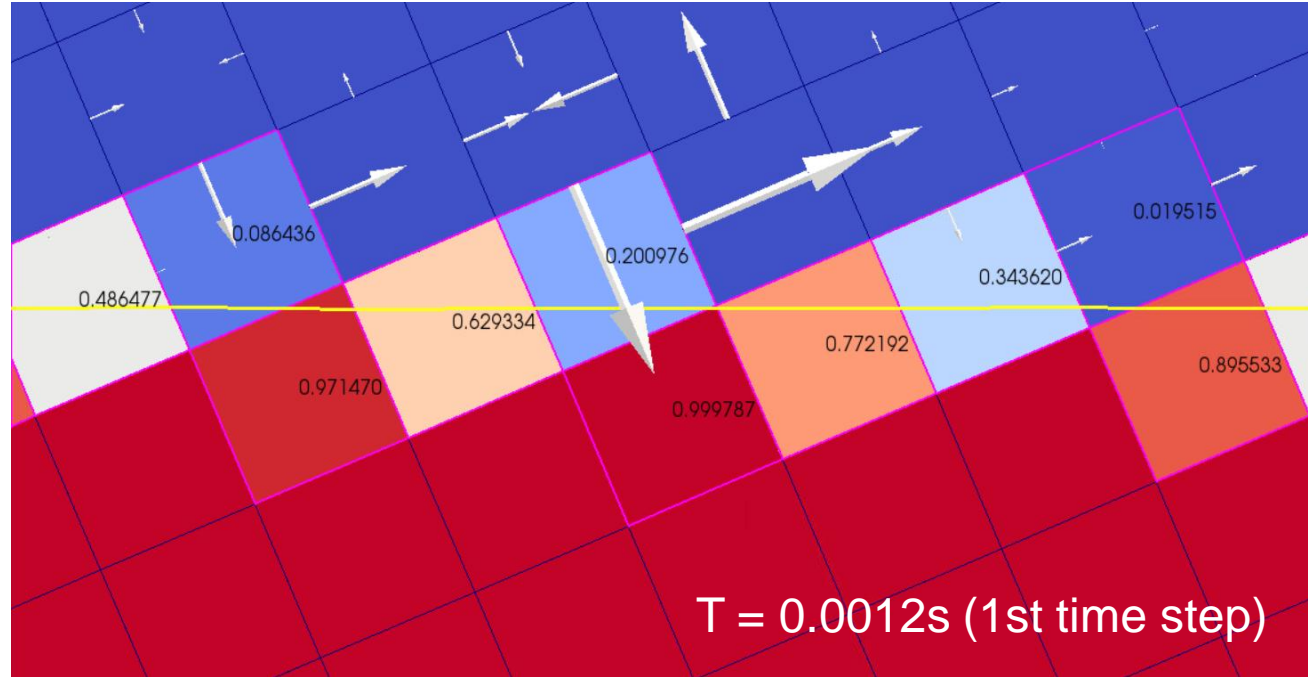
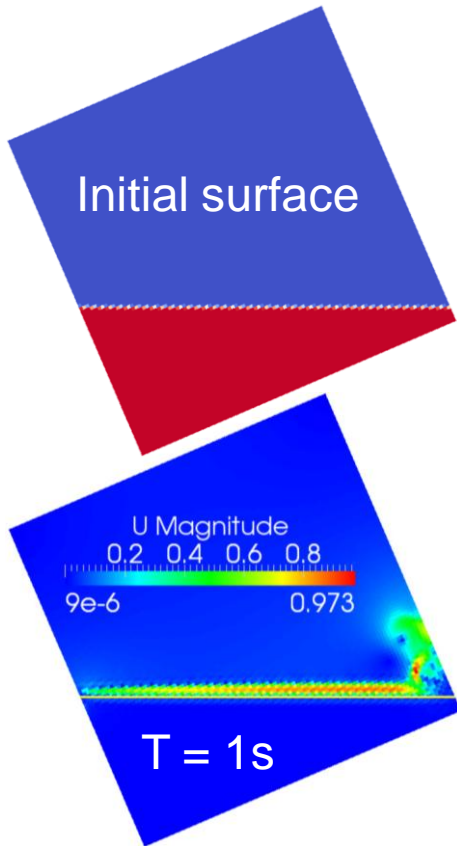
a_n , b_n and c_n given by quadrilateral corners of two subsequent vertex-interface encounters.

face-interface
intersection lines and
times calculated using
isosurfaces

Optional bounding procedure

- Sum up all face dV_j 's for cell i to get change in α_i during time step
- Check if more water is added than there is room for (overflowing) or more water is removed than is available in the cell (over-emptying)
- If this is the case adjust dV_j for all cell faces cut by isoface so that cell is exactly filled/emptied. This is currently done by using the dV_j 's of these faces as weights of total added/removed water rather than as absolute water volumes.
- Because it is the dV_j 's that are modified, this step does not compromise volume conservation.
- For practical reasons it is convenient to have the option to snap α_i 's to 0 or 1

Inconsistency in interFoam pressure handling



Tilted 1m x 1m box with initial flat water

Pressure equation in interFoam (pEqn.H)

```
2 volScalarField rAU("rAU", 1.0/UEqn.A());
3 surfaceScalarField rAUf("rAUf", fvc::interpolate(rAU));
4
5 volVectorField HbyA("HbyA", U);
6
7
8 surfaceScalarField phiHbyA
9 (
10     "phiHbyA",
11     (fvc::interpolate(HbyA) & mesh.Sf())
12     + fvc::ddtPhiCorr(rAU, rho, U, phi)
13 );
14
15 adjustPhi(phiHbyA, U, p_rgh);
16 phi = phiHbyA;
17
18 surfaceScalarField phig
19 (
20     (
21         fvc::interpolate(interface.sigmaK())*fvc::snGrad(alpha1)
22         - ghf*fvc::snGrad(rho)
23     ) * rAUf * mesh.magSf()
24 );
25
26 phiHbyA += phig;
27
28 while (pimple.correctNonOrthogonal())
29 {
30     fvScalarMatrix p_rghEqn
31     (
32         fvm::laplacian(rAUf, p_rgh) == fvc::div(phiHbyA)
33     );
```

To numerically take the gradient of a jump function is asking for trouble

$$\nabla \cdot \int_{C_i} (\mathbf{g} \cdot \mathbf{x}) \nabla \rho \, dV =$$

$$\sum_{face\ j} \int_{F_j} (\mathbf{g} \cdot \mathbf{x}) \nabla \rho \cdot d\mathbf{S}$$

$$\nabla \rho = (\rho_2 - \rho_1) \hat{\mathbf{n}}_S \delta(\mathbf{x} - \mathbf{x}_S)$$

$$\int_{F_j} (\mathbf{g} \cdot \mathbf{x}) \nabla \rho \cdot d\mathbf{S} =$$

$$(\rho_2 - \rho_1) \int_{F_j \cap S} (\mathbf{g} \cdot \mathbf{x}) \hat{\mathbf{n}}_S \cdot d\mathbf{S}$$

Solution depends on choice of $z = 0$

interFoam/pEqn.H:

```
surfaceScalarField phig
(
    (
        fvc::interpolate(interface.sigmaK())*fvc::snGrad(alpha1)
        - ghf*fvc::snGrad(xho)
    ) * rAUf * mesh.magSf()
);

phiHbyA += phig;
```

Stream function wave in 15m flume and 1m depth.
Wave height = 0.2m, period = 1s, length = 1.684m)

ExecutionTime
= 4921.02 s

Seabed at $y = -1.0\text{m}$



Velocity profiles at $x = 0$ and 6.736m .
Alpha1 contours: (0.01; 0.5; 0.99)

ExecutionTime
= 4072.95 s

Seabed at $y = -1.2\text{m}$

Time: 0.00