



## Mesh motion strategies for the simulation of external gear pumps

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- **Motivation and state of the art**

- **Mesh motion strategy**

  - Profile definition and mesh generation

  - Interface calculation

  - Projection algorithm

  - 2D-3D mesh motion

  - Parallelization

  - Topological changes

- **Implementation**

- **Test cases**

- **Conclusions and future work**



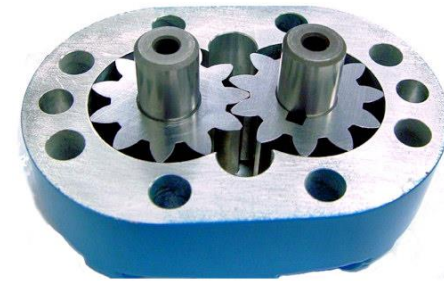
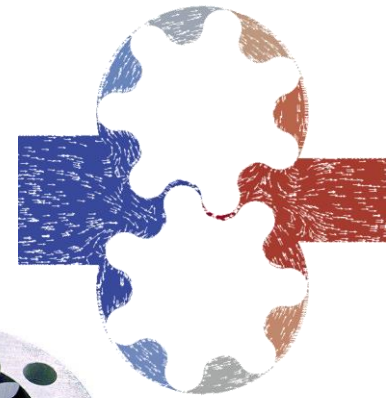
**External gear pumps:**

- High viscosity fluids
- Working pressure up to 210 bar
- Rotation speed up to 3000 rpm
- Mechanical clearance  $\approx 10 \mu m$

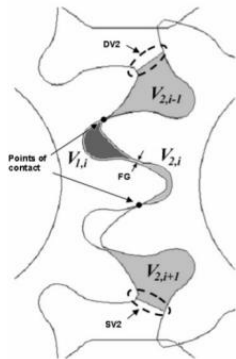
**Crucial predictions:**

- Pressure ripple
- Flow rate pulsations
- Max/min pressure

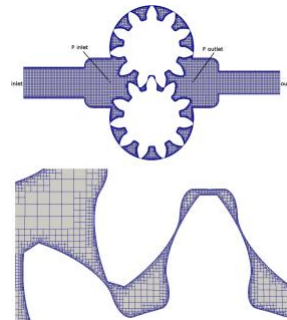
**Simulation strategies:**



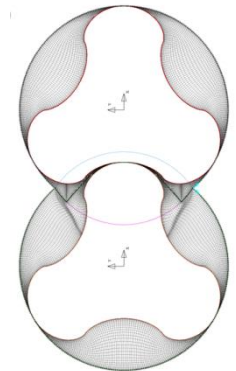
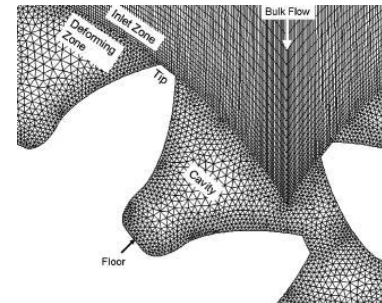
1D-2D simulations



Multiple-mesh approach



User defined dynamic mesh

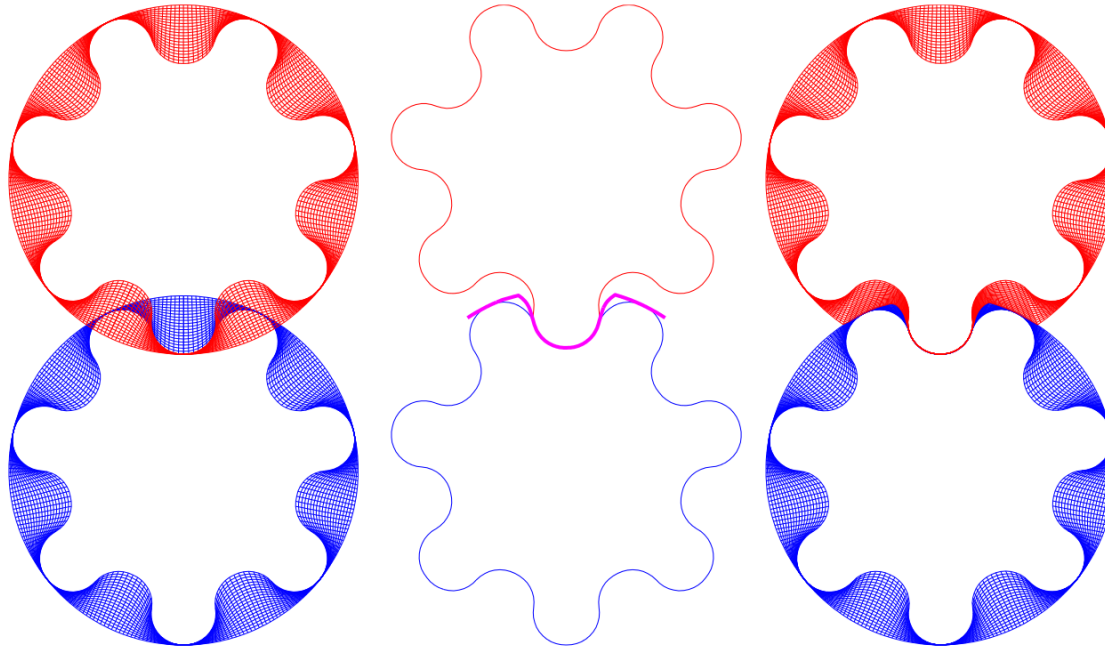




## Overview of the proposed strategy:

Single dynamically changing 2D/3D mesh

- Constant number of cells/points (speed)
- No mesh-to-mesh interpolation (accuracy)
- Automatic mesh generation (extendibility)



1.- Solid rotation of “non projected points”

2.- Calculation of an “interface” for the given angle

3.- Projection of points to the calculated interface

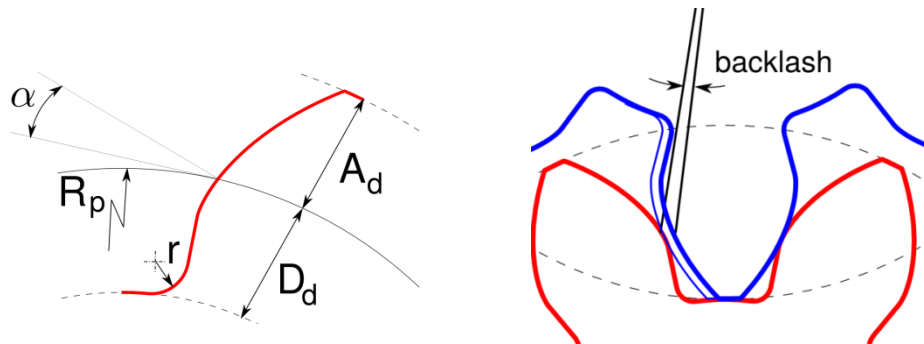


## Profile definition

The user can choose a predefined geometry or provide a list of points

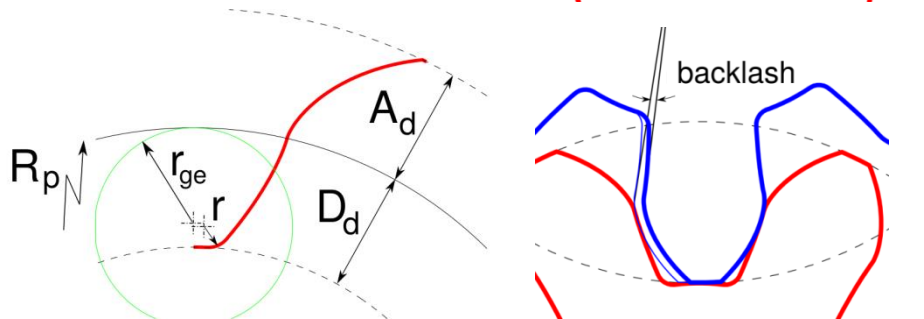
### Involute

- Pressure angle ( $\alpha$ )
- Number of teeth ( $Z$ )
- Backlash angle



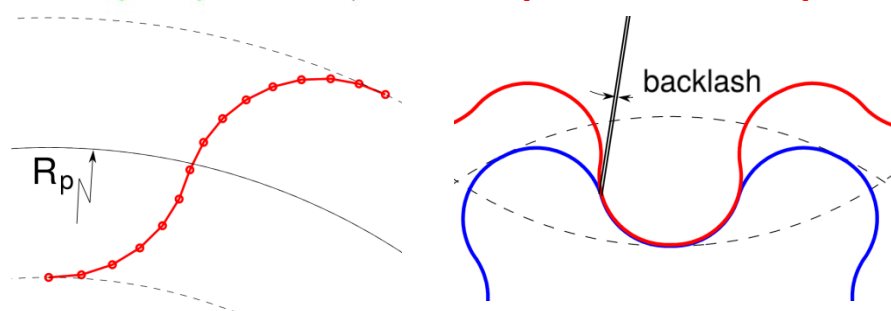
### Cycloidal

- Generating circle radius ( $r_{ge}$ )
- Number of teeth ( $Z$ )
- Backlash angle



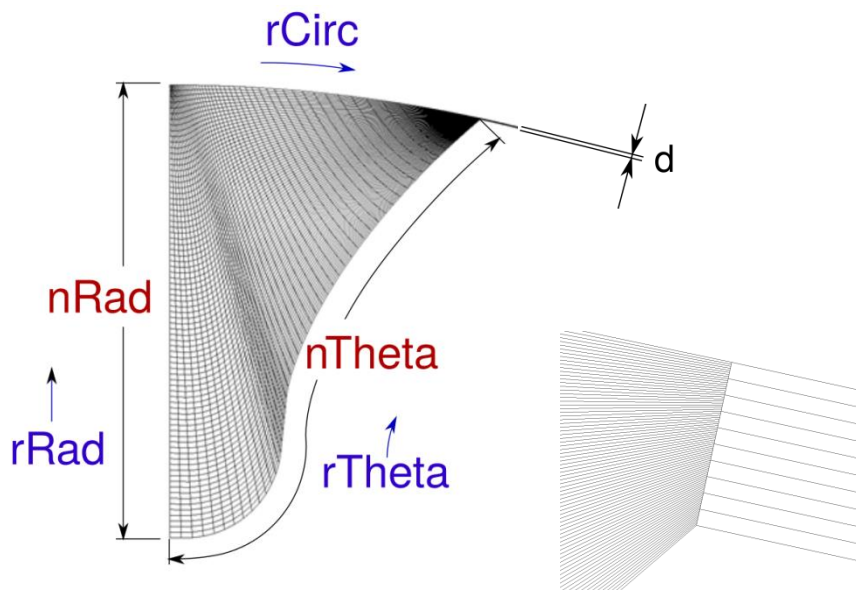
### User-given pointList

- List of points
- Backlash angle

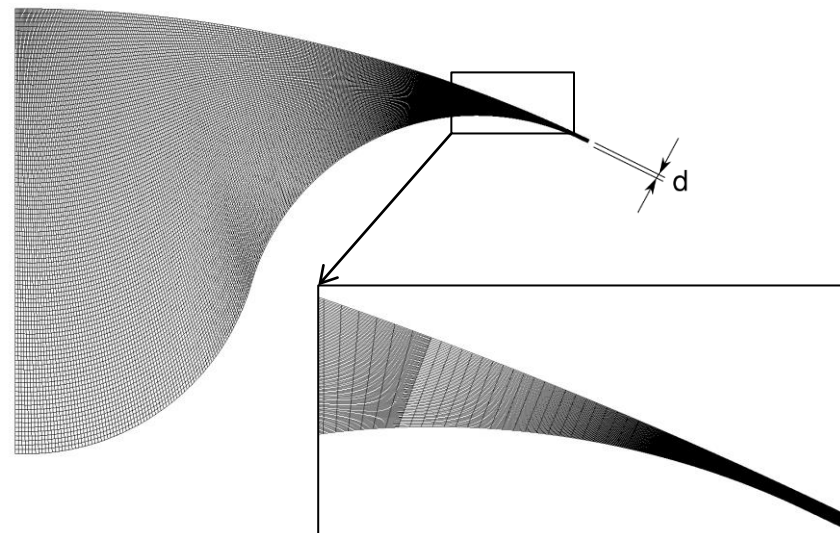




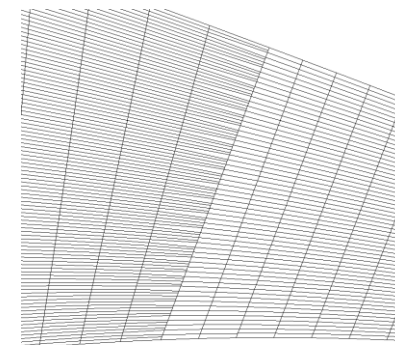
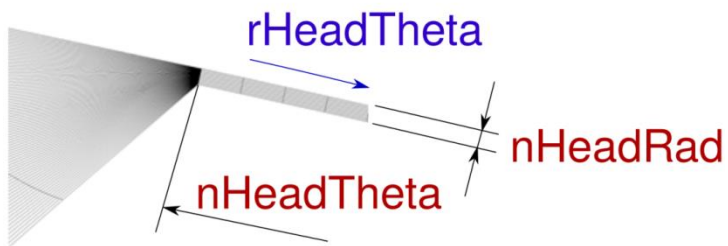
## Generation of initial “non-projected” mesh



User defined number of cells and grading ratios:



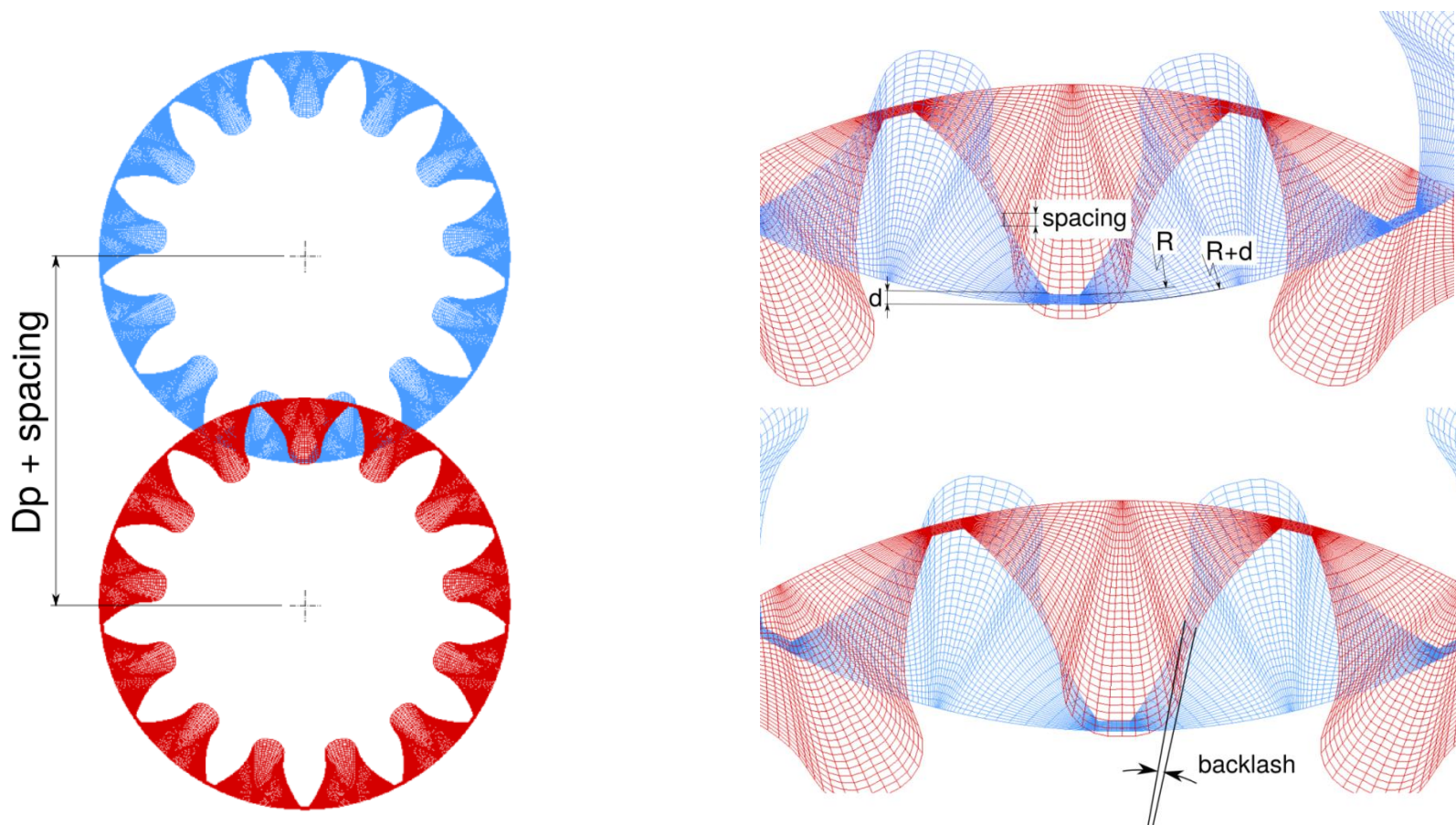
Block splitting with non-conformal interfaces





## Generation of initial “non-projected” mesh

The initial block is repeated to fill both gears.  
A tolerance for the distance between centers is introduced

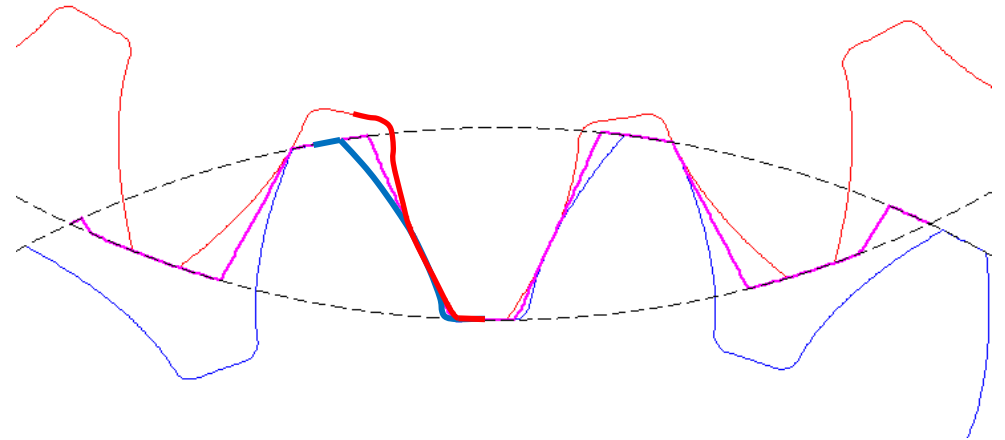




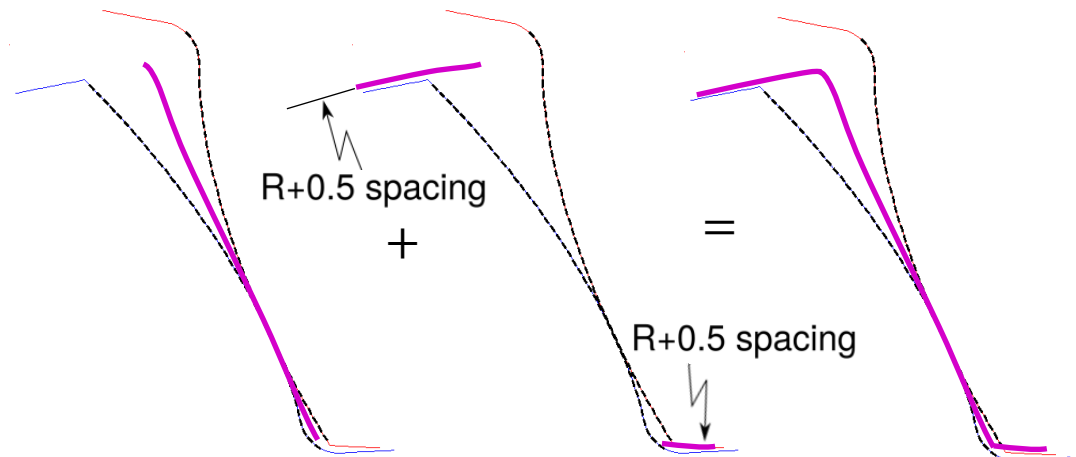
## Interface calculation

### Method1 - Separated profiles

The gearing zone is separated in “half-tooth” couples, which are used to determine “single interfaces”.



Single interfaces are joined with arcs to complete the whole interface.

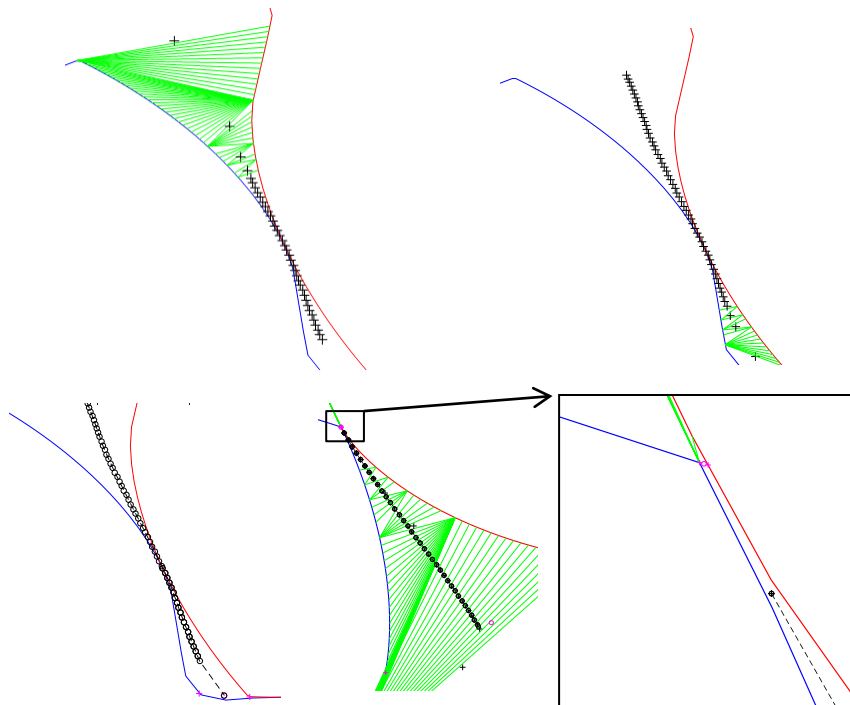




## Method1 - Separated profiles

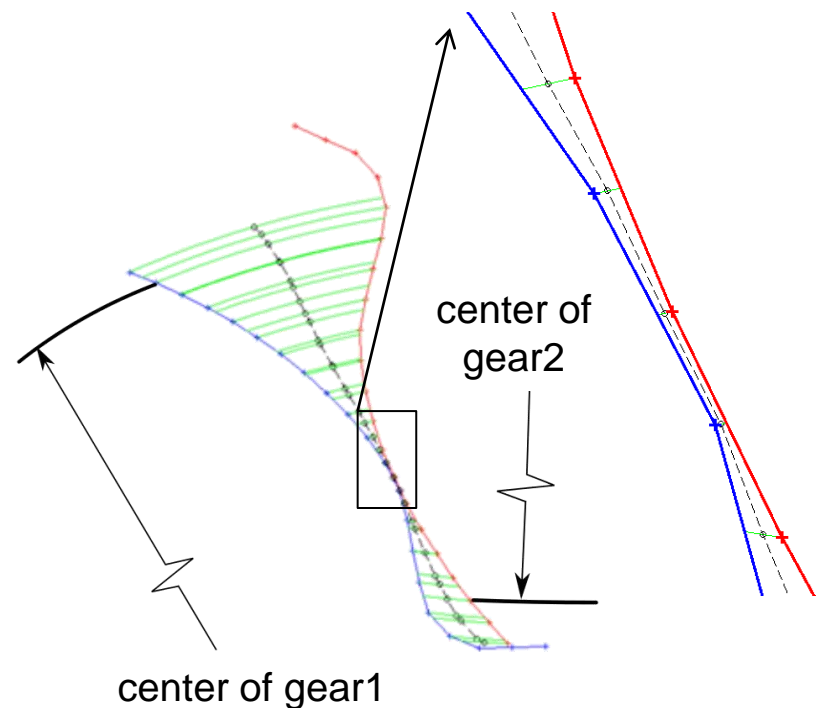
Two possible ways of calculating the “single interfaces”

### Fréchet



Interface is calculated using profiles with  $nPointsInterface$  number of points, which is independent of the number of mesh points

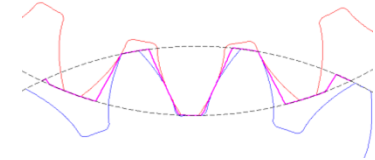
### Arcs



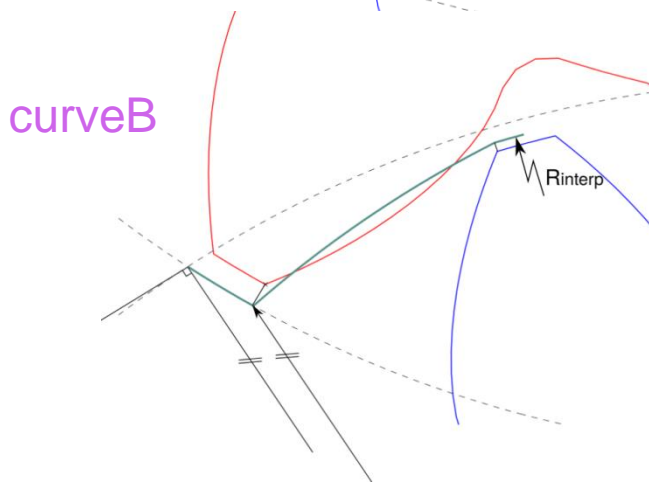
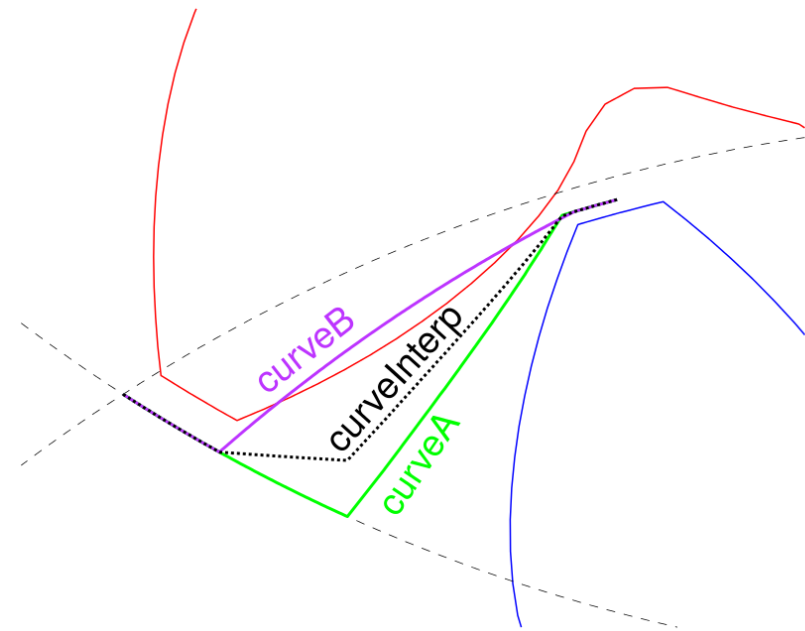
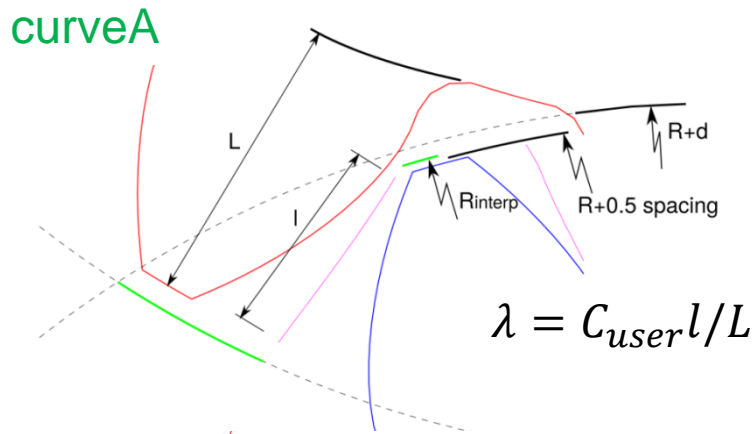
Interface is calculated using the same points as those defining the mesh



## Method1 - Separated profiles



First and last “single interfaces” need to be completed in a different way



Final curve is a blending

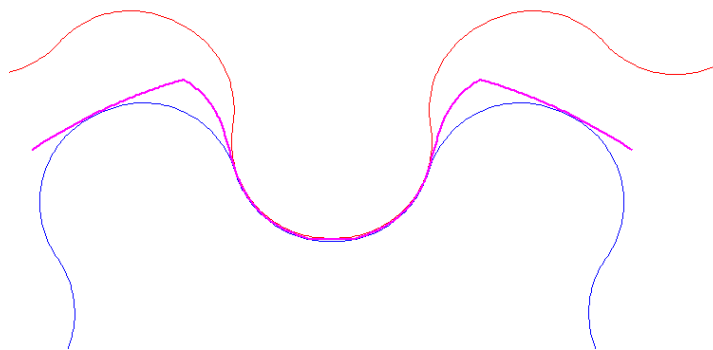
$$curveInterp = \lambda curveA + (1 - \lambda) curveB$$



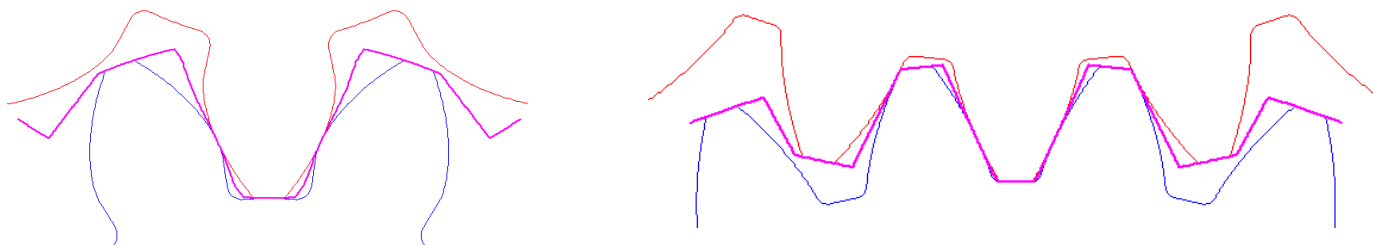
## Method1 - Separated profiles

Some examples:

**Lobe profile:**



**Involute profiles:**



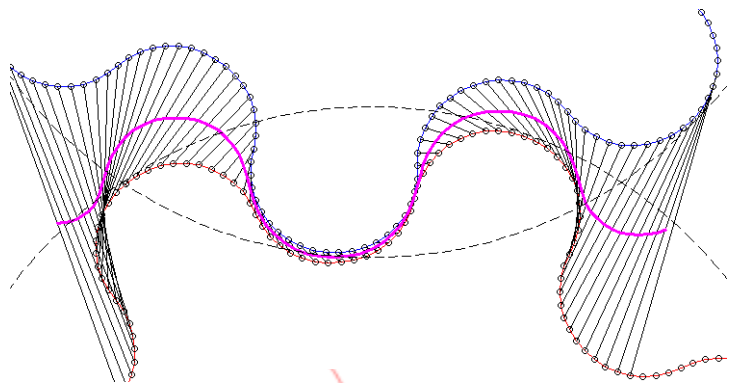
**Cycloid profiles:**



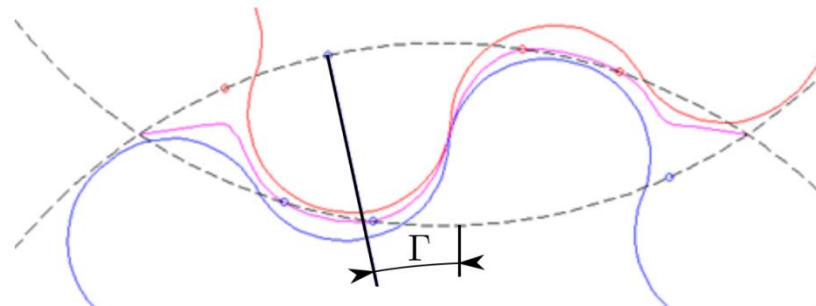


## Interface calculation

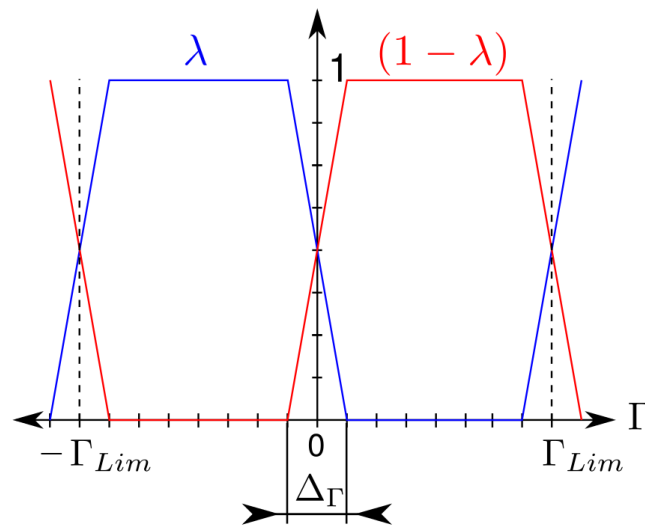
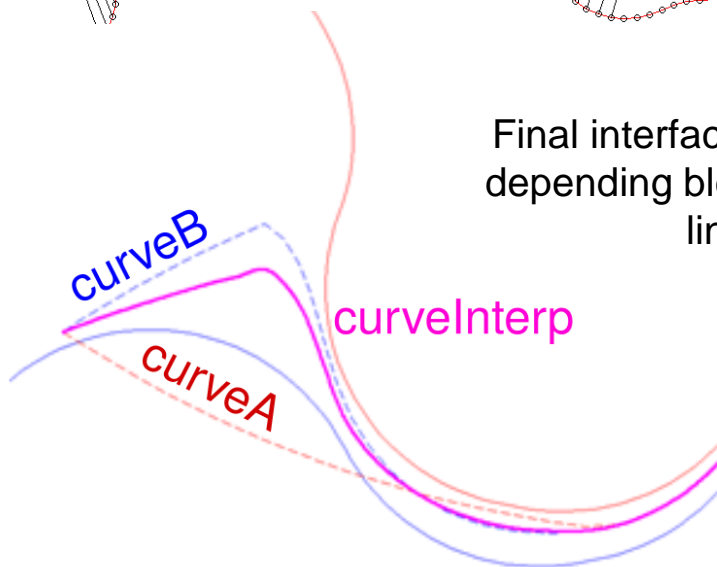
### Method2 – Complete profile



The whole interface is calculated at once



Final interface is an angle-  
depending blend of dashed  
lines

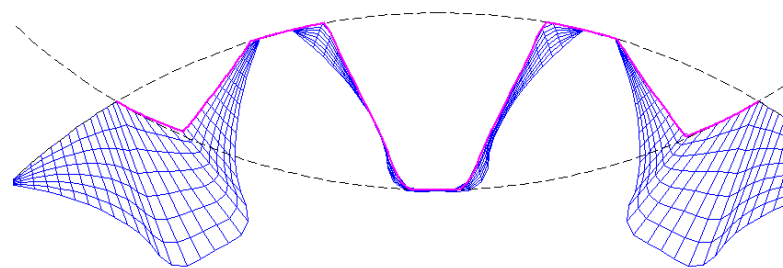
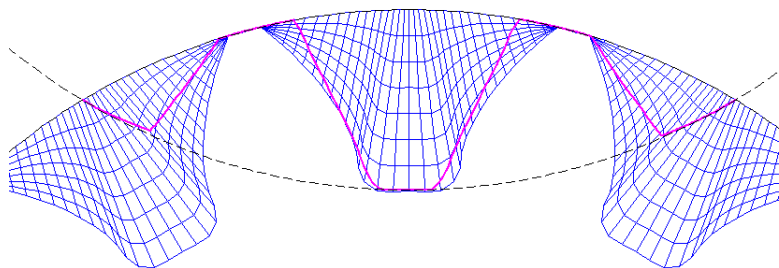


$$curveInterp = \lambda curveB + (1 - \lambda) curveA$$



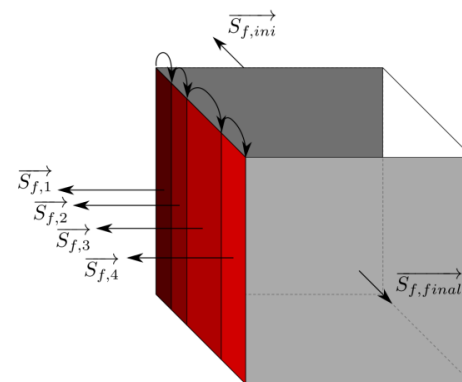
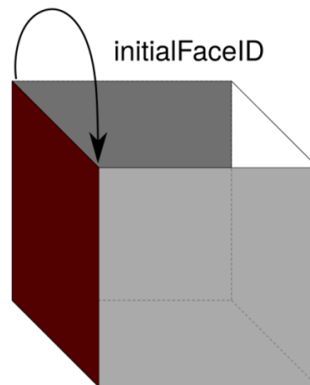
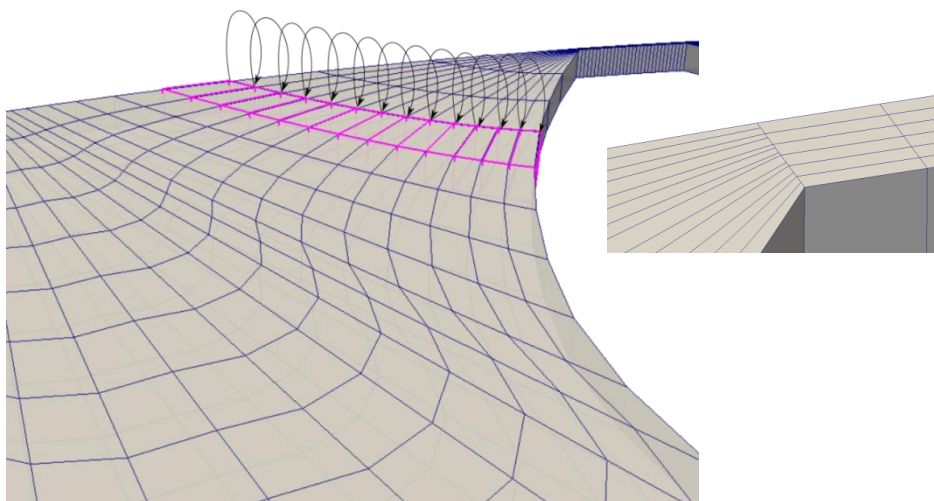
## Projection algorithm

Initial non-projected points are moved to their final projected position



At the beginning of the calculation a matrix containing all ordered point labels of the gears is created

*matrixOfPoints\_[zone][zLevel][circPoint][interiorPI]*



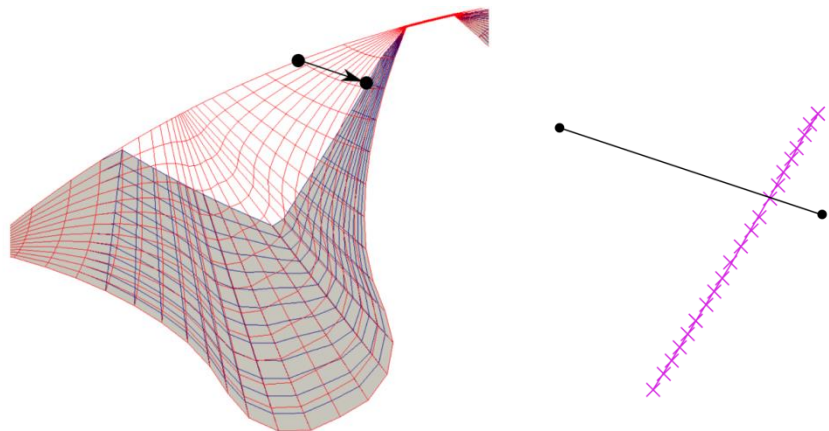
opposingFaceLabel



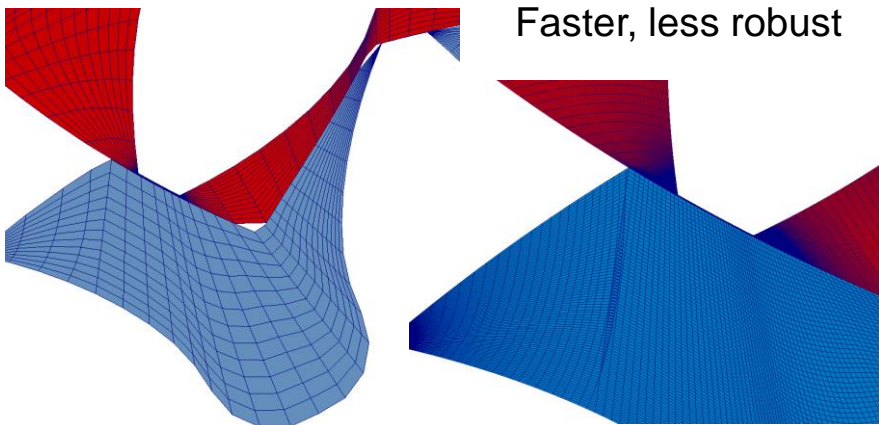
## Projection algorithm

Intersection between the edges of the mesh and the interface is found and points are projected using any of the two following strategies

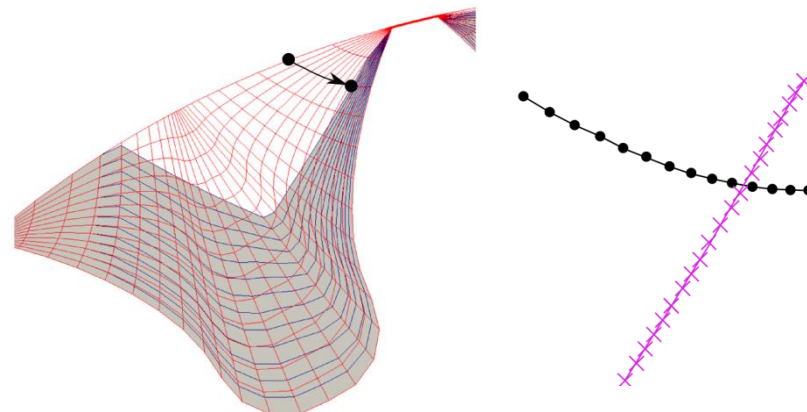
### linearProjection



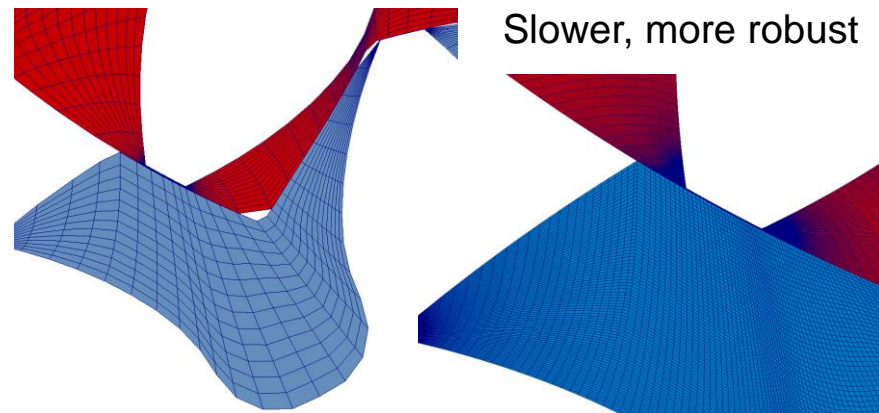
Faster, less robust



### polyLineProjection



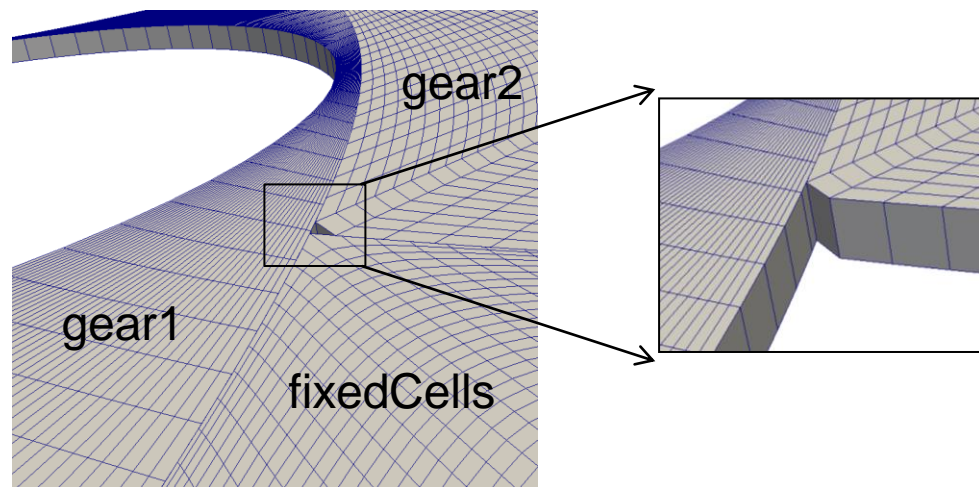
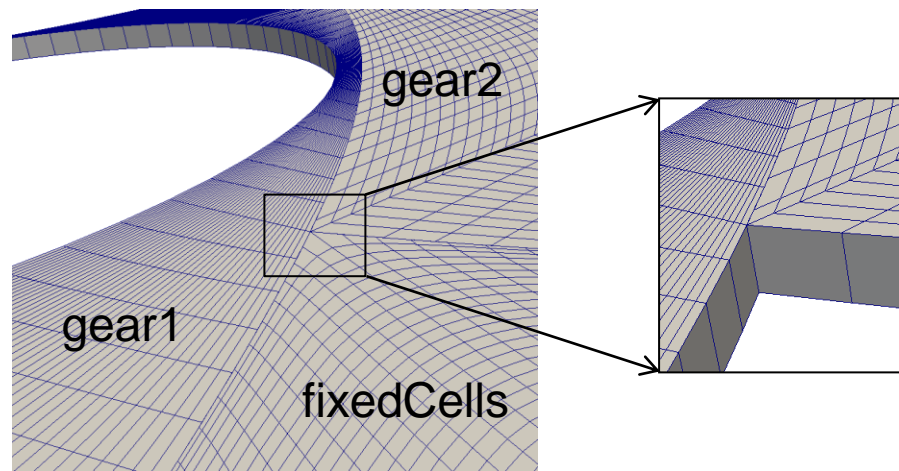
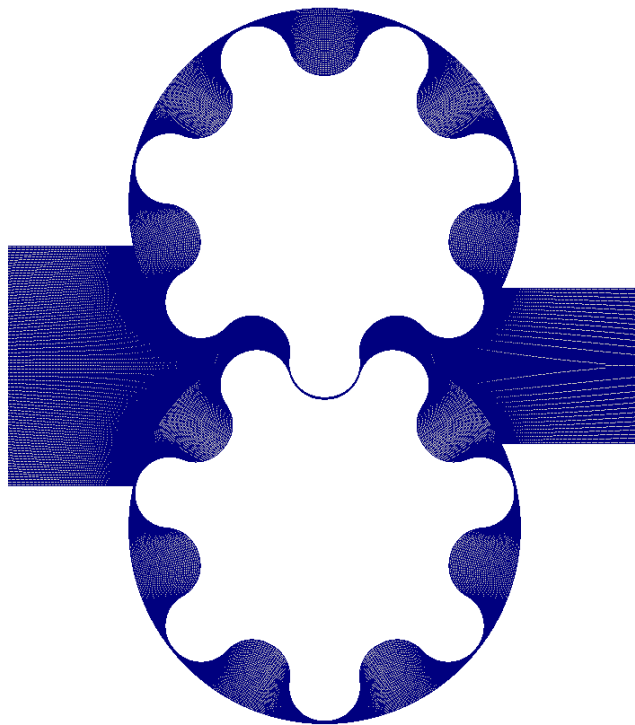
Slower, more robust





## 2D mesh motion

Limit points can be further projected to avoid wholes and facilitate boundary condition treatment

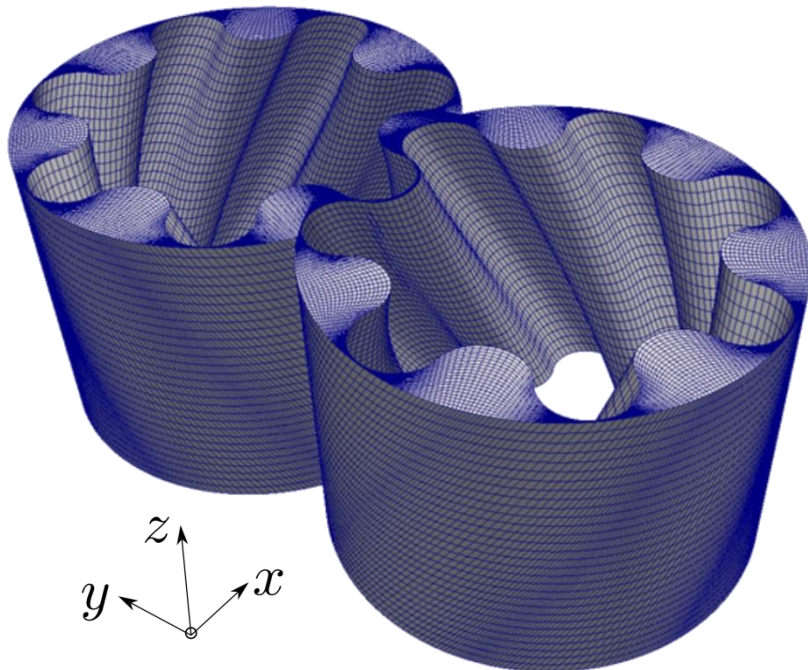




**3D mesh motion** The same strategy can be applied in the 3D case

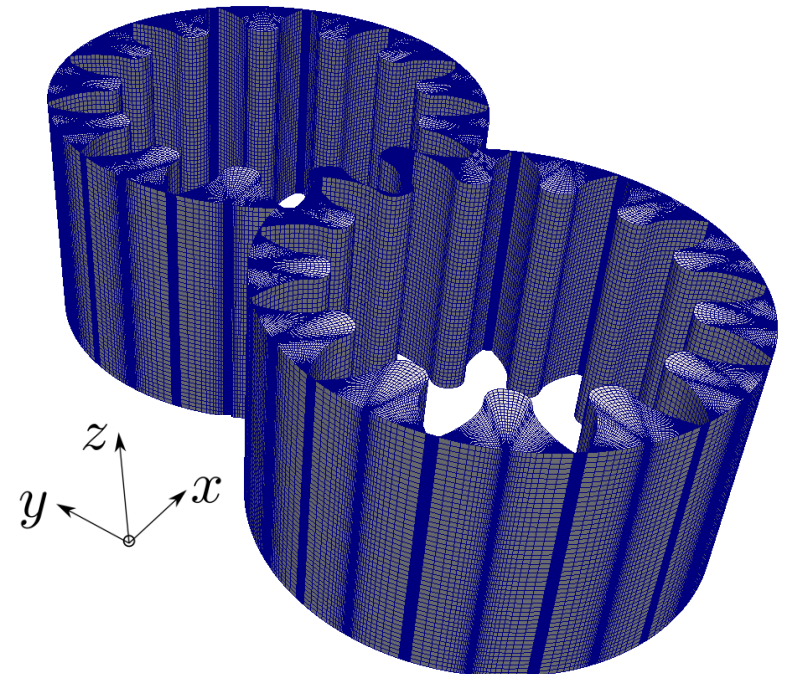
## Helical gears

Points are contained in constant  $z$  planes. Interface calculation and point projection is determined for the points in each  $z$ -Level



## Straight-cut gears

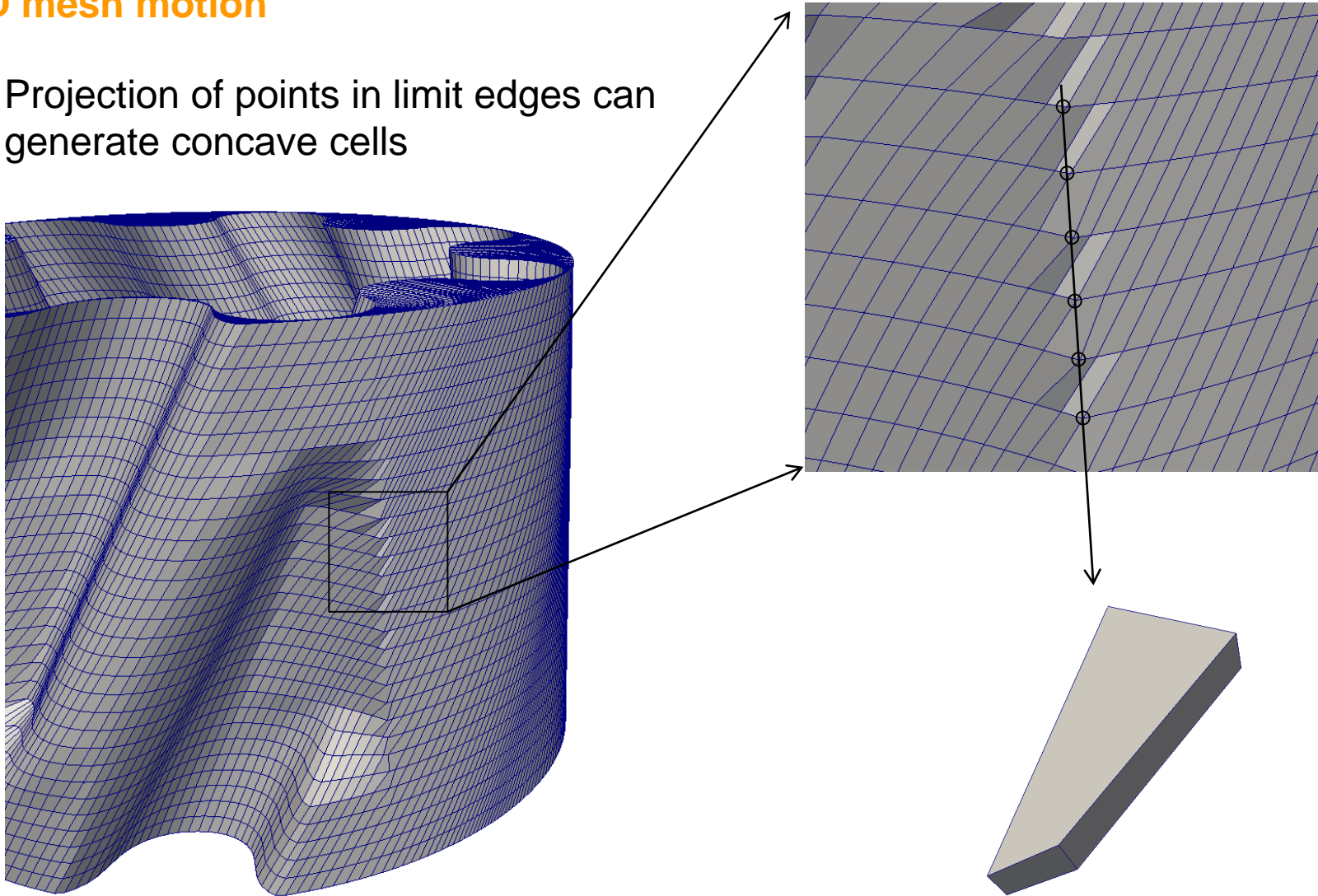
Interface calculation and point projection (final coordinates determination) need to be done just for one  $z$ -Level





## 3D mesh motion

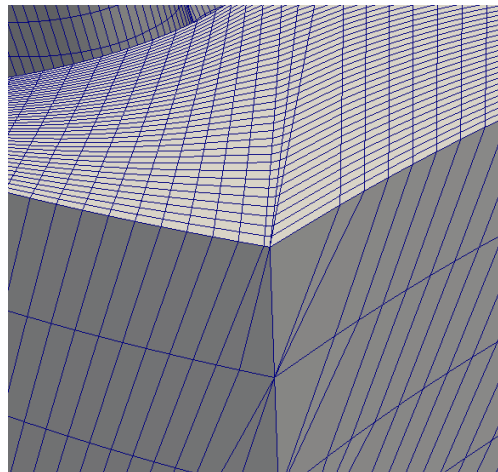
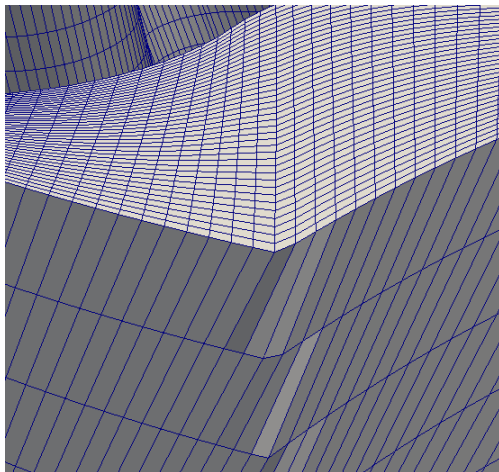
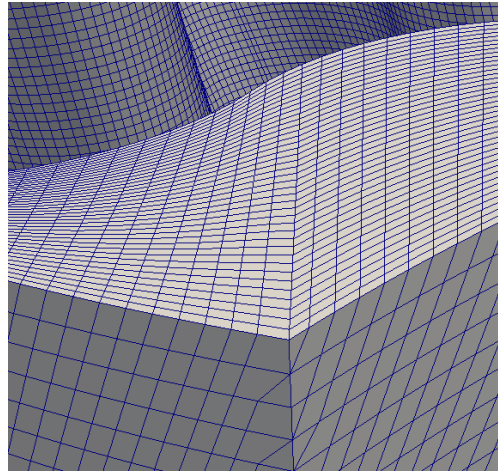
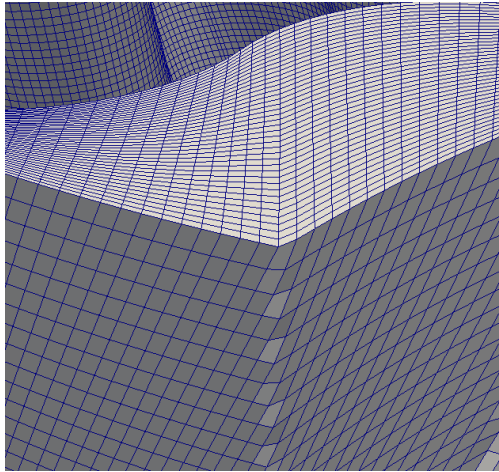
Projection of points in limit edges can generate concave cells



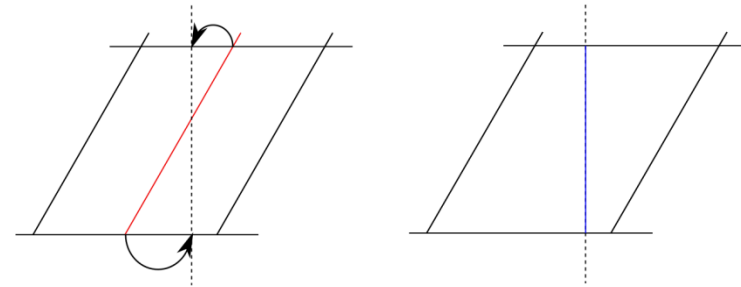


## 3D mesh motion

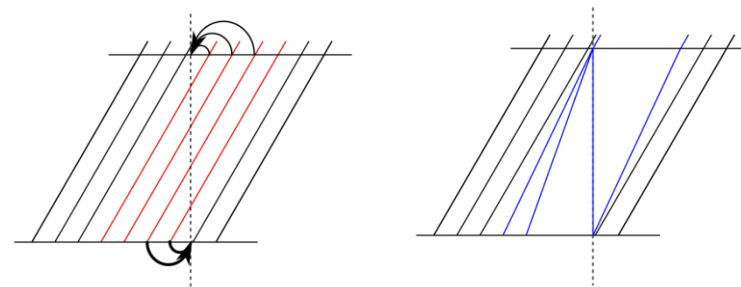
The motion class can optionally project some additional points are projected to the limit edge, generating wedge-like cells



No “zeroArea” faces are created



We choose one edge that will become vertical

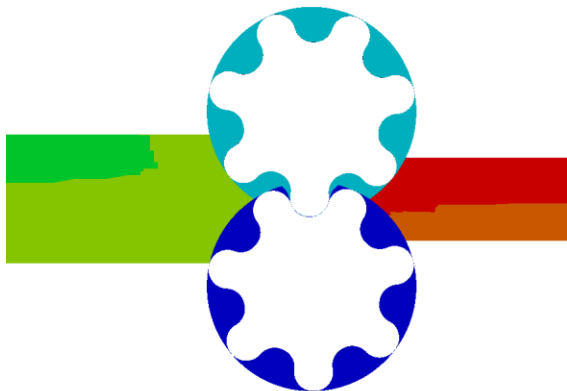




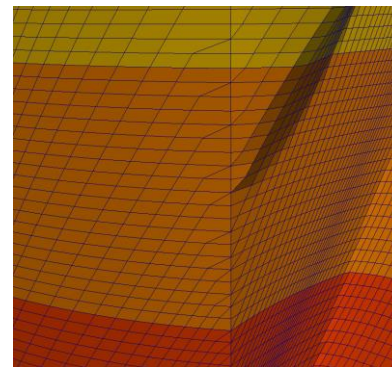
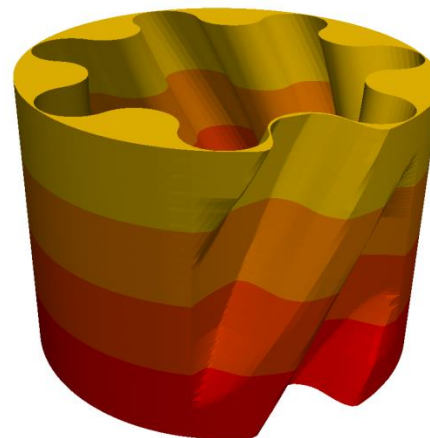
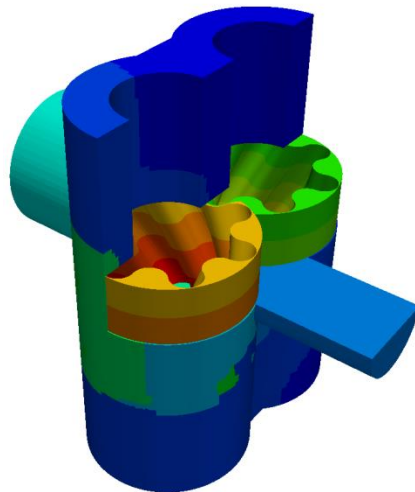
## Parallelization

Cells of each single gear are kept in one processor.  
Rest of the domain can be decomposed with any other strategy (e.g. scotch)

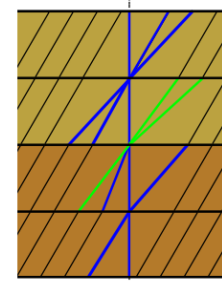
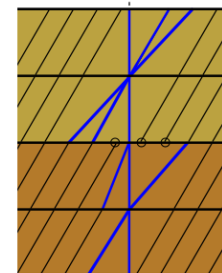
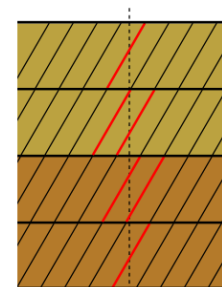
### 2D case



### 3D case



### Synchronization of points

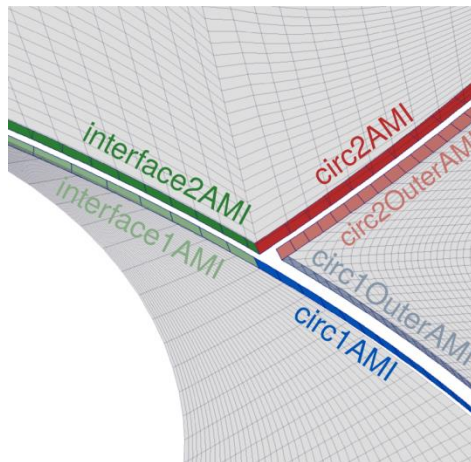
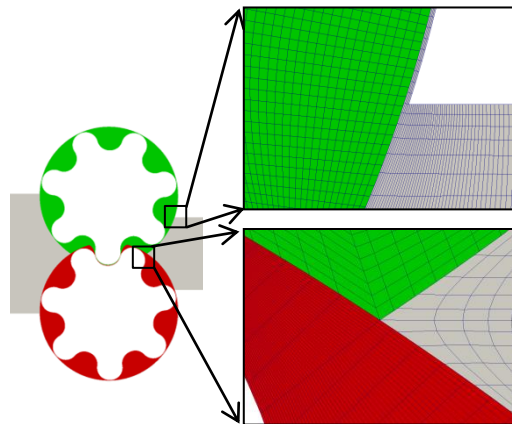




## Topological changes

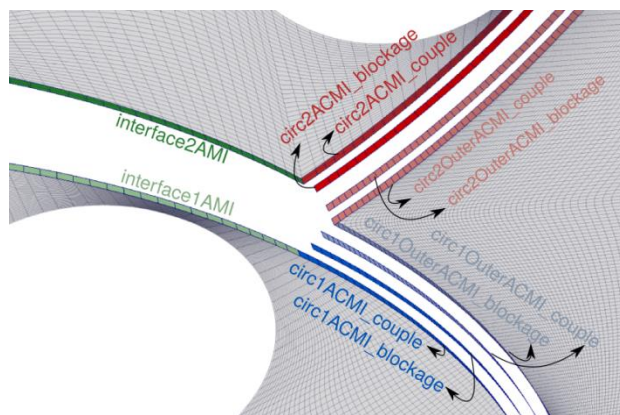
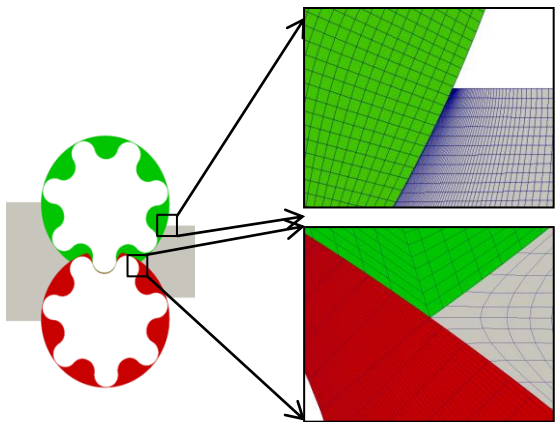
Two possible strategies to treat the boundaries between regions

### Using AMI conditions



When required a face is moved from one patch to another

### Using AMI and ACMI conditions

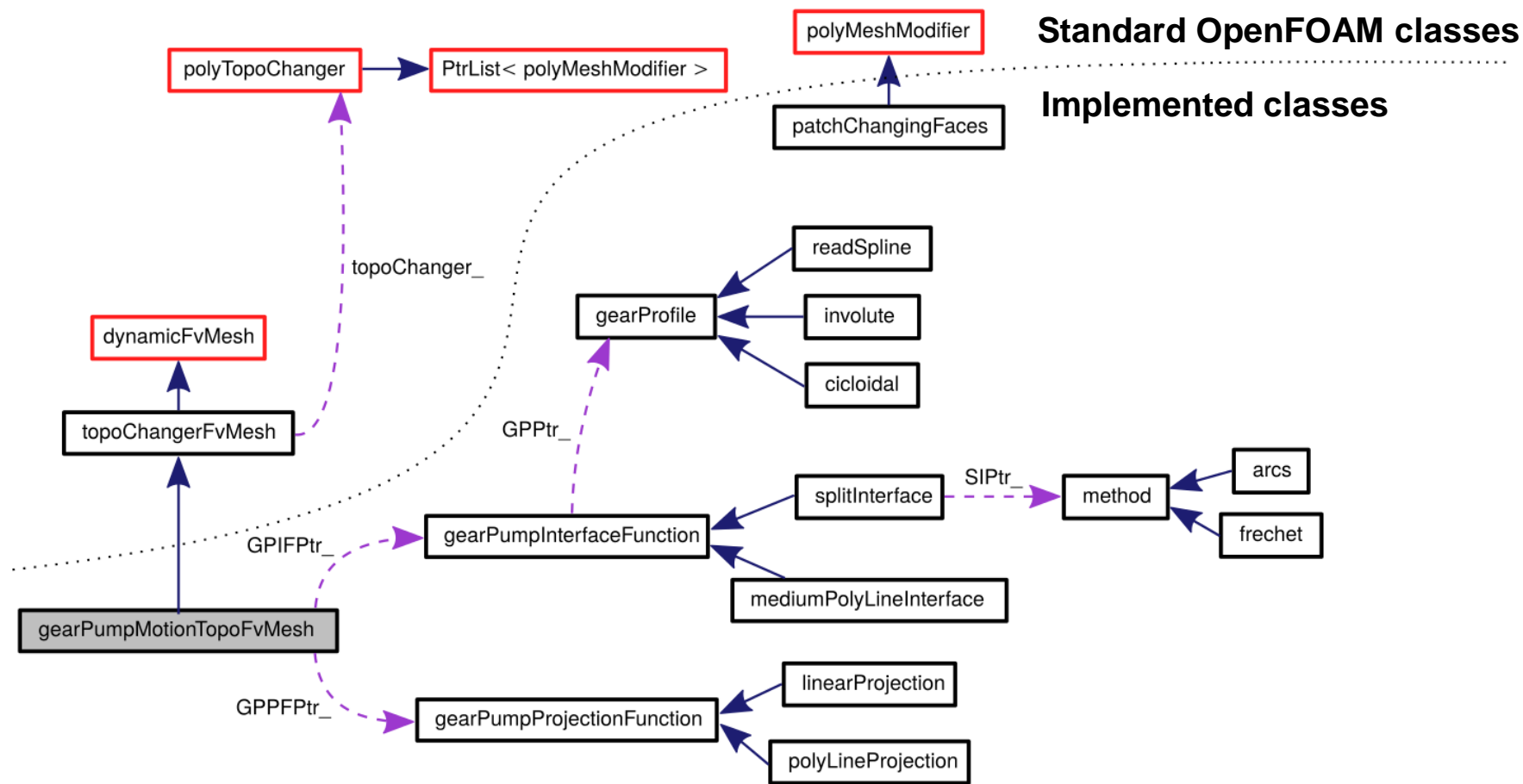


In this case new boundary faces need to be created/deleted



## Collaboration diagram

Implementation is done in the updated release of OpenFOAM-dev

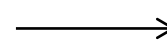


**Mesh motion:**

`dynamicMeshDict`

**Mesh generation:**

`createGearPumpMeshDict`

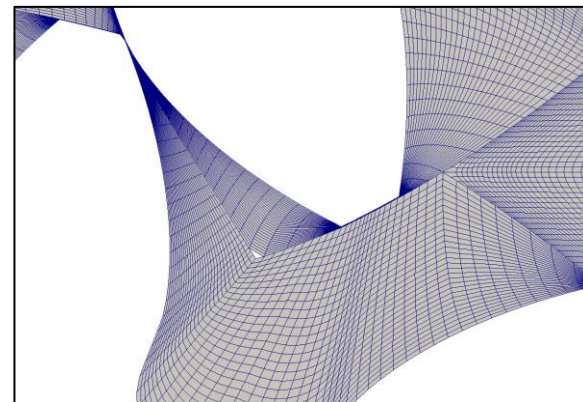
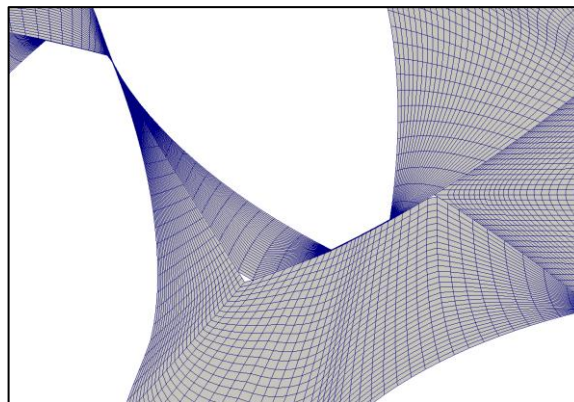
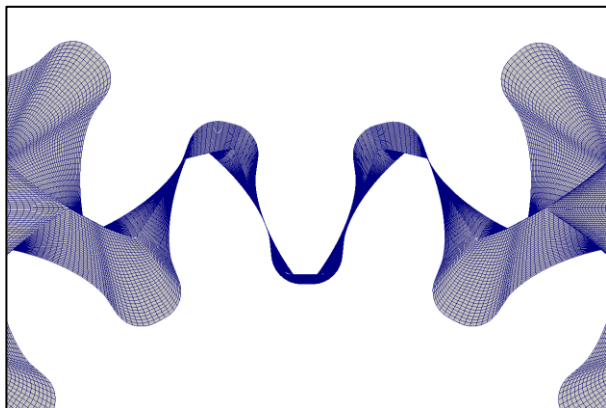


`createGearPumpMesh`

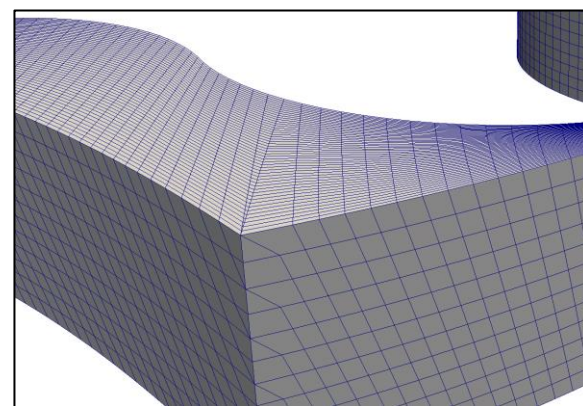
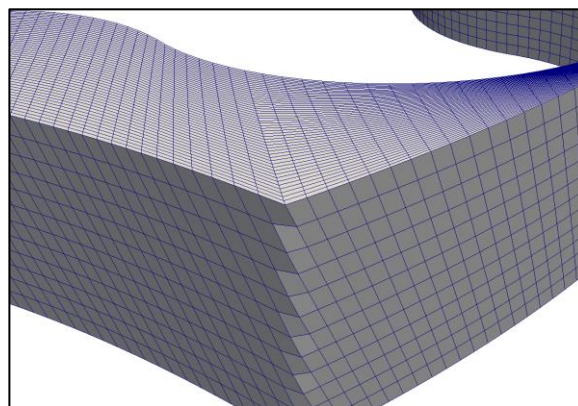
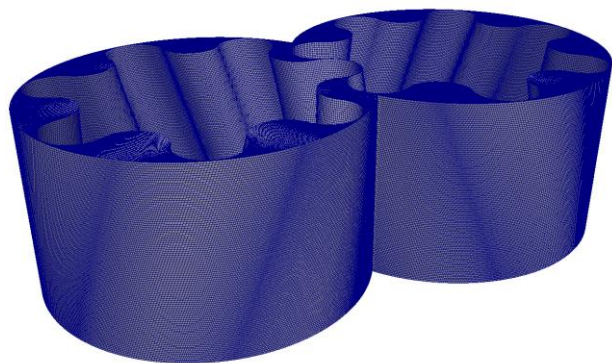


## Mesh motion examples

### 2D involute profile

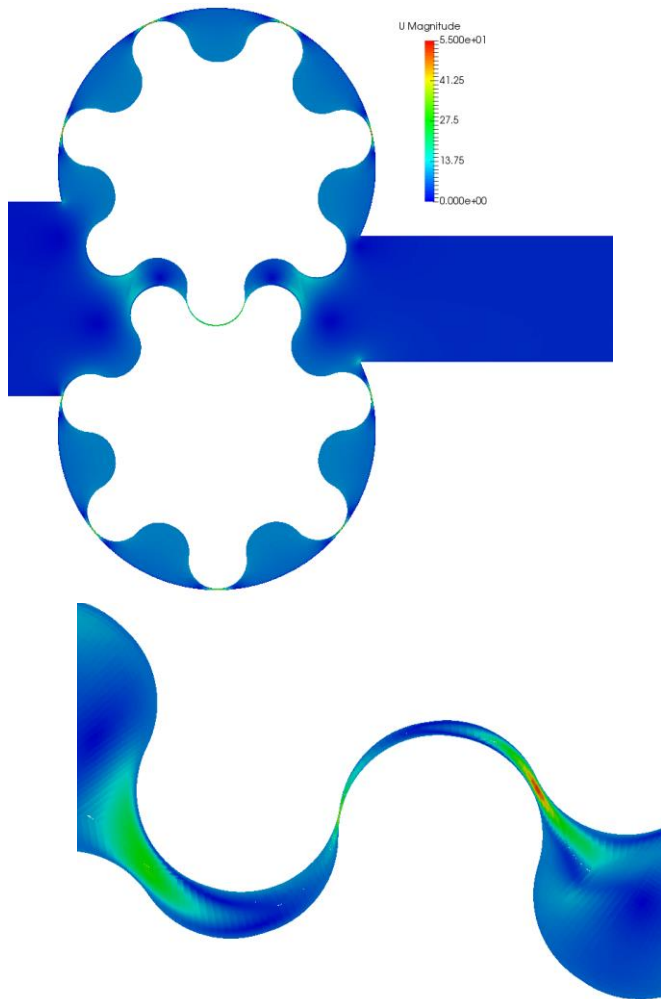


### 3D Lobe profile

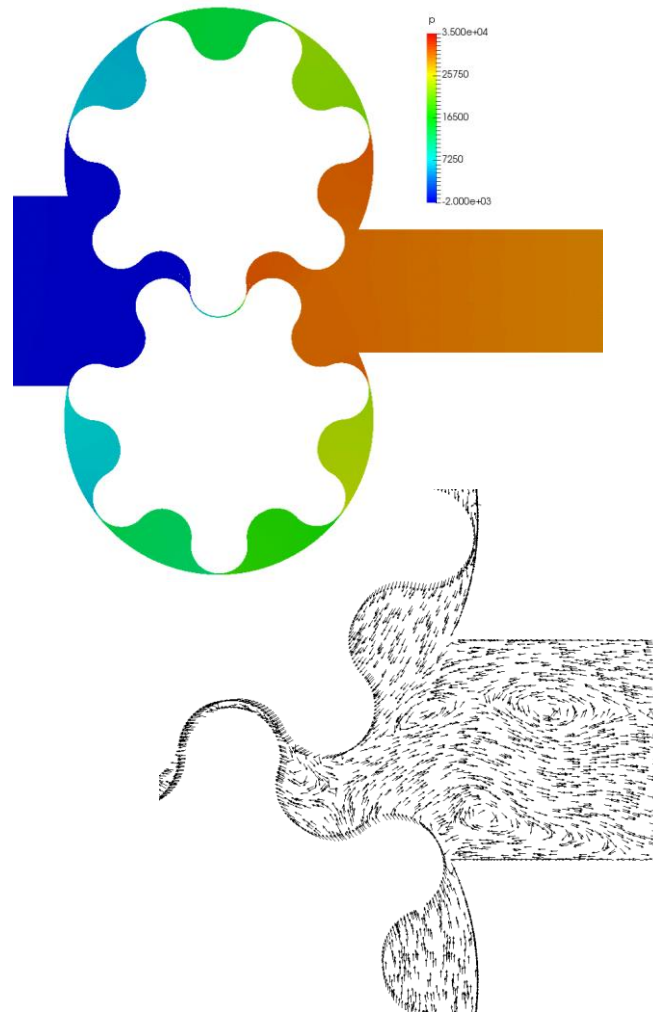




## Simulation example



## 2D lobe-profile simulation



## Case setup

$\rho = 878 \text{ kg/m}^3$   
 $\mu = 5.97 \cdot 10^{-3} \text{ kg/ms}$   
 $tol \approx 100 \mu\text{m}$   
 $n = 3500 \text{ rpm}$   
 $\Delta p \approx 3000 \text{ psi}$

*pimpleDyMFoam*  
(with additional  
*correctPhi* iterations)

$\approx 150000$  cells  
*kOmegaSST* model



## Conclusions

- Development and implementation of a new mesh motion strategy for 2D and 3D simulations of external gear pumps
- Appropriate parallelization and topological changes
- Mesh generation application

## Future work

- Run-time mesh smoothing
- Identification of contact region and appropriate treatment (porous media)
- Testing the influence of tolerances and working conditions in 2D-3D cases





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