

MHD supersonic flow control simulation in OpenFOAM

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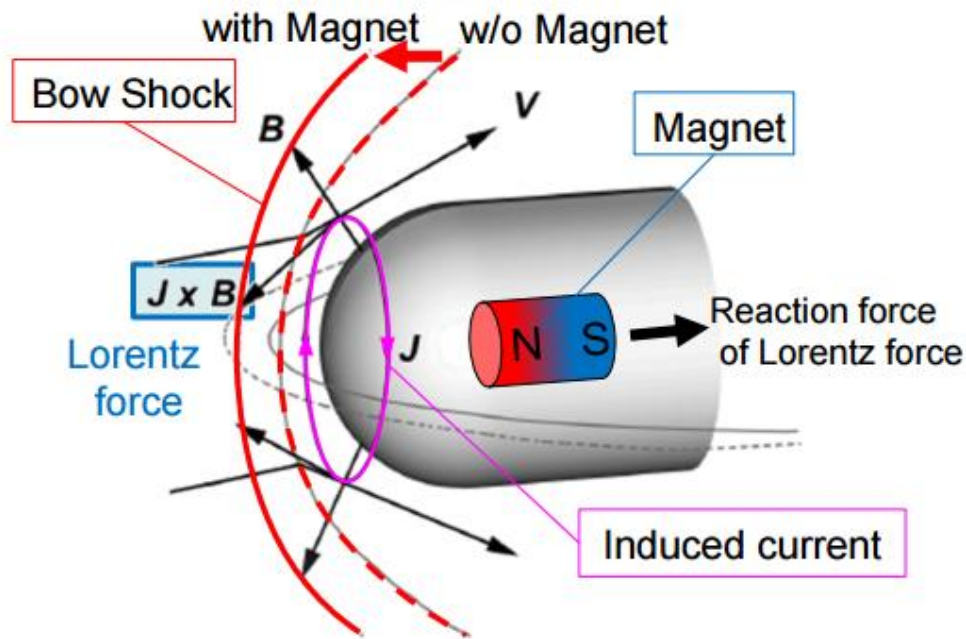
MHD flow control concept

Magnetic field interacts with weakly ionized plasma between the bow shock and the body:

- Lorentz force
- Joule heating

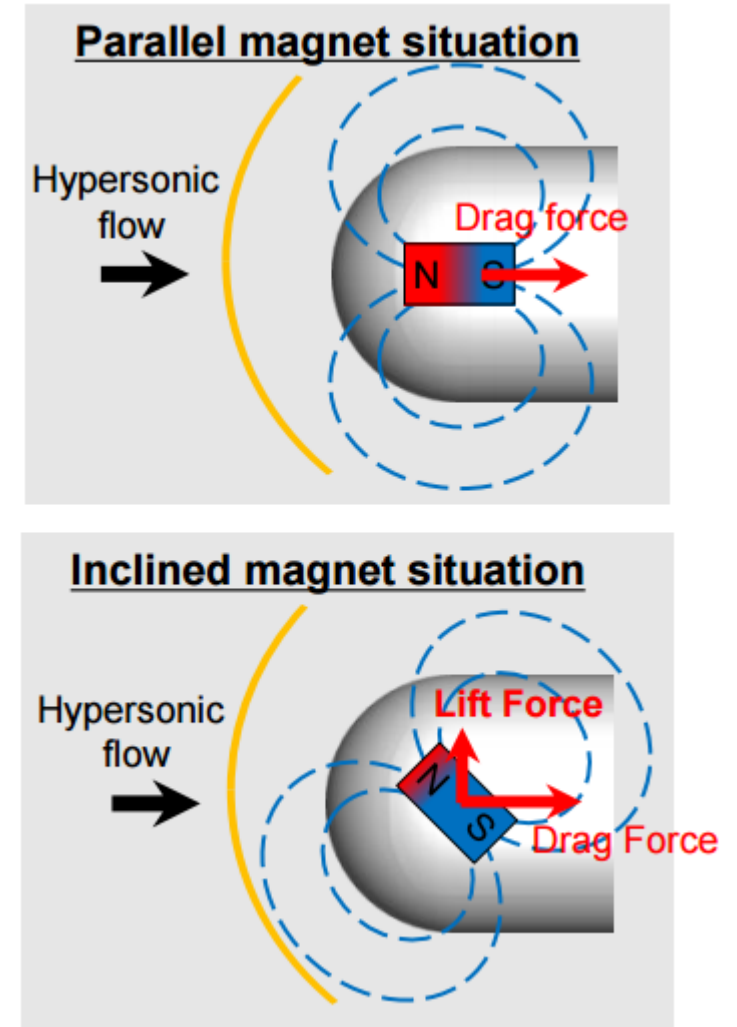
Effects:

- Reduction of aerodynamic heating
- Enhancement of drag force
- Widening of shock layer



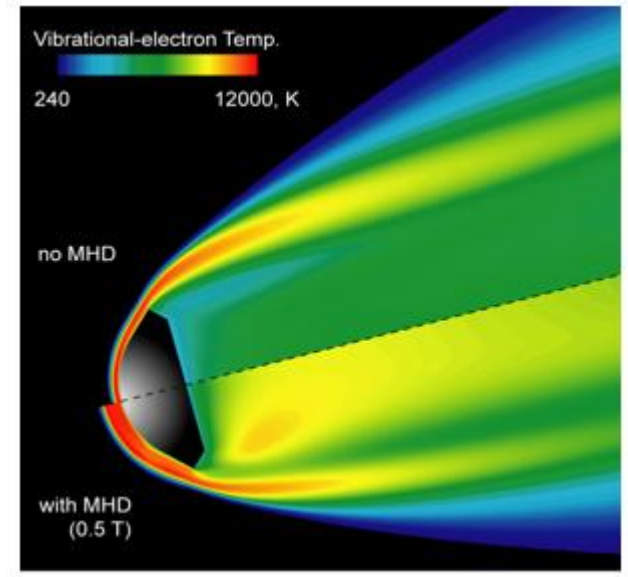
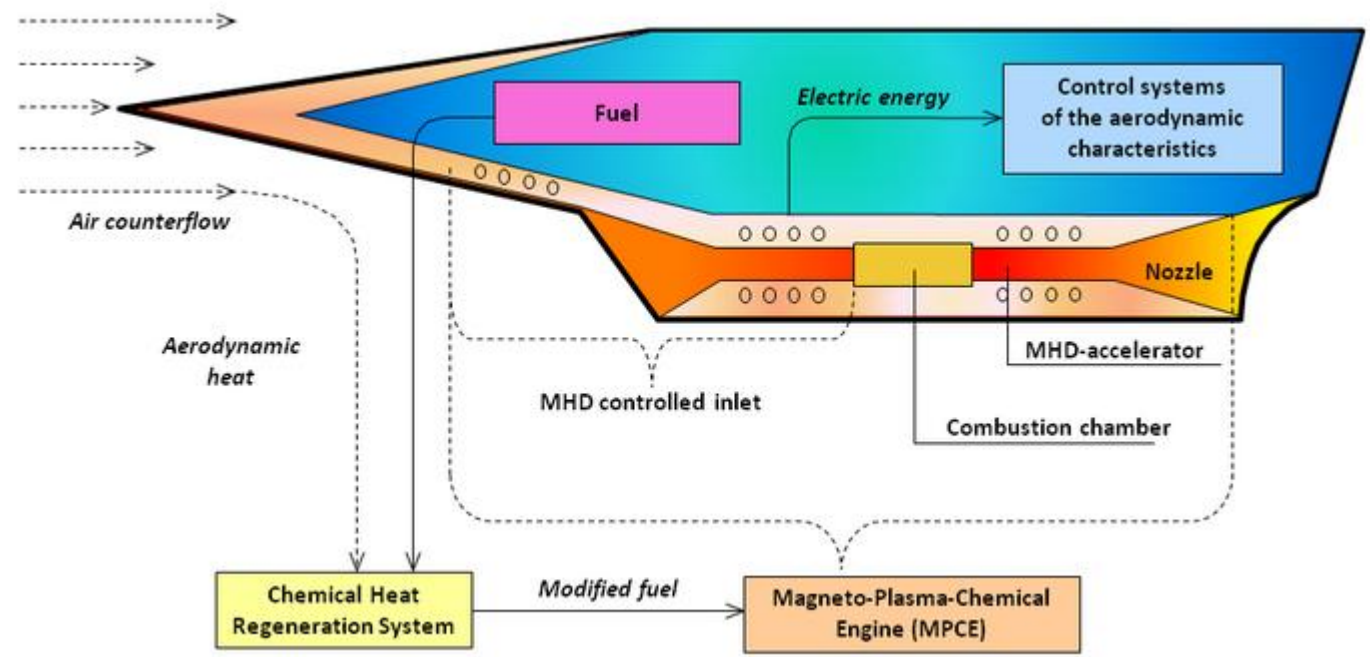
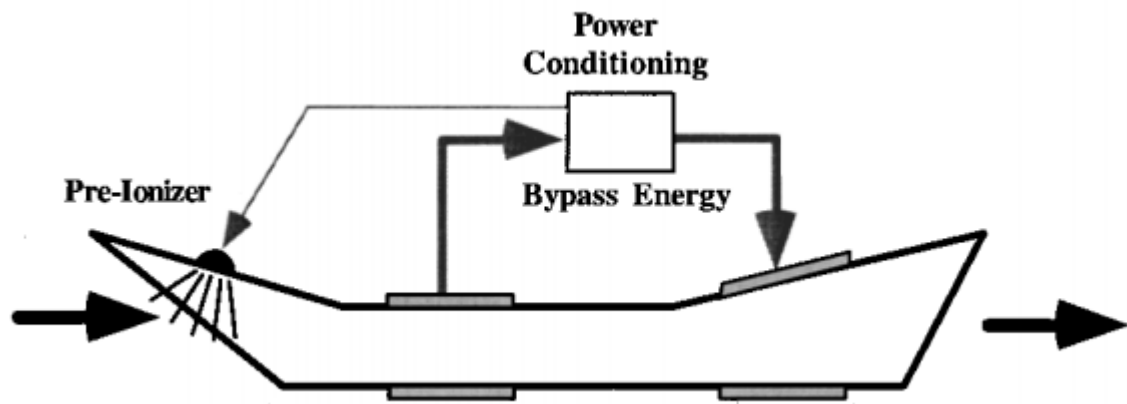
*Y Nagata, K Yamada, T Abe

Controlling reentry flight trajectory

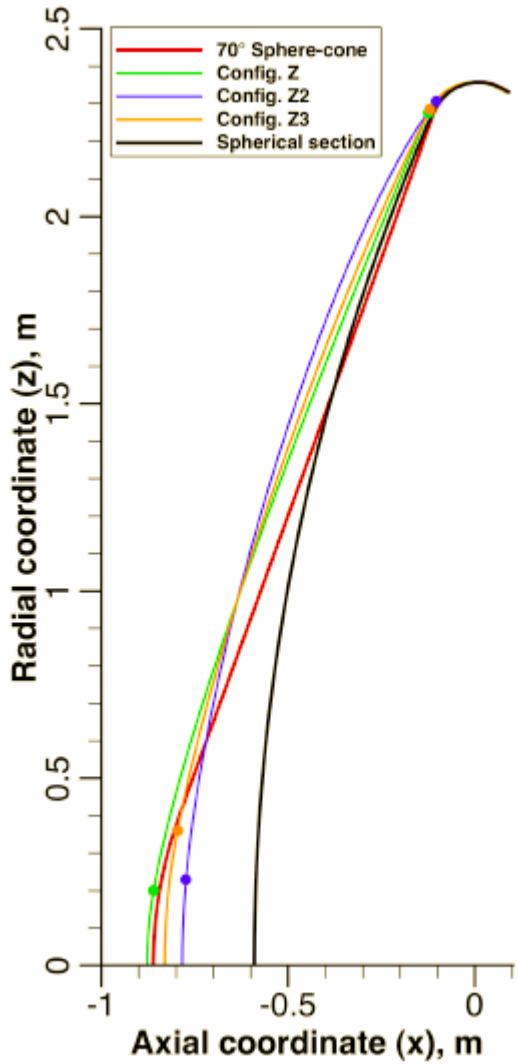


MHD control applications

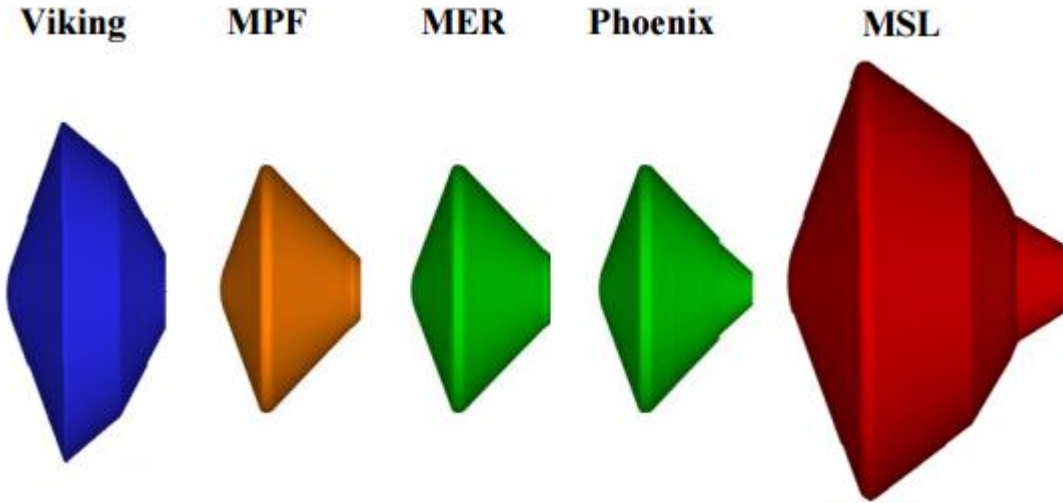
- *Hypersonic scramjet aerodynamics*
- *Atmospheric entry vehicles*
- *MHD energy bypass engine*



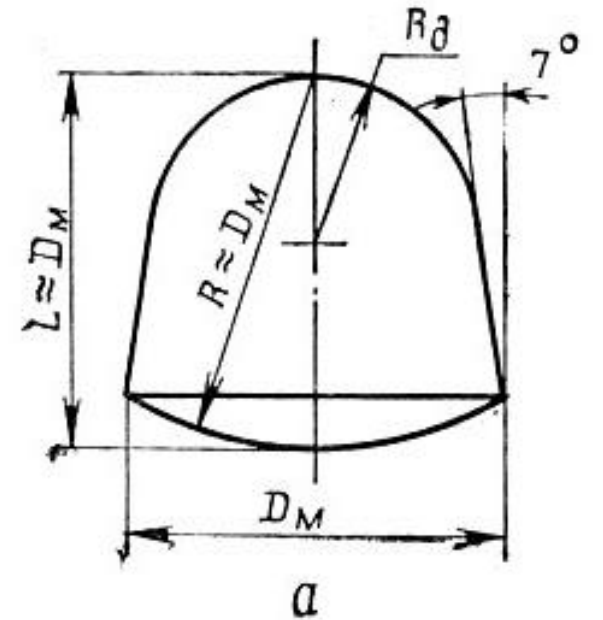
Case geometries



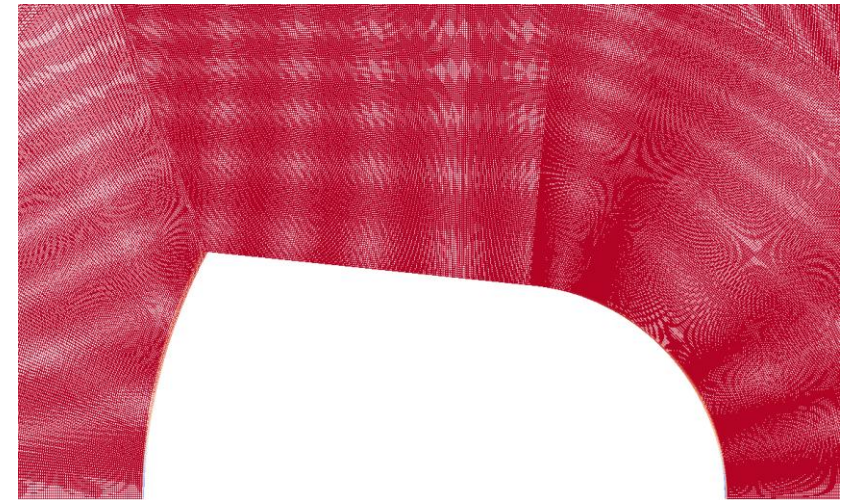
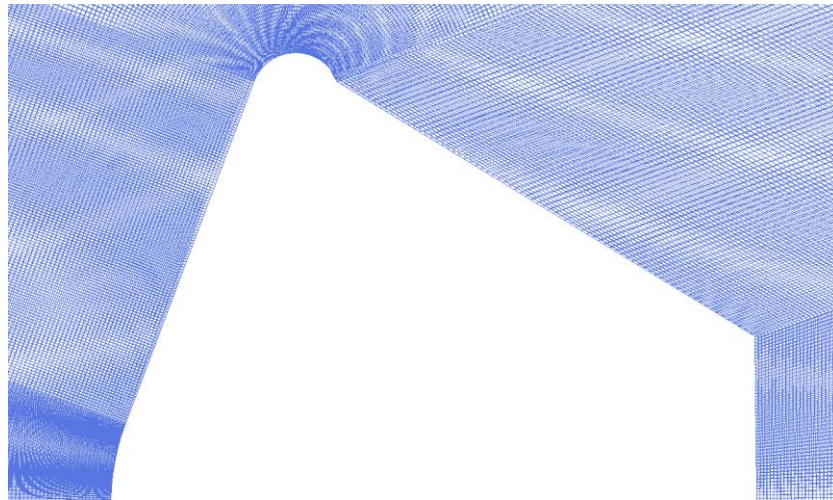
Generatrices



NASA Mars descent capsules shapes



Soyuz capsule schematics



Corresponding meshes

OpenFOAM supersonic and MHD capabilities

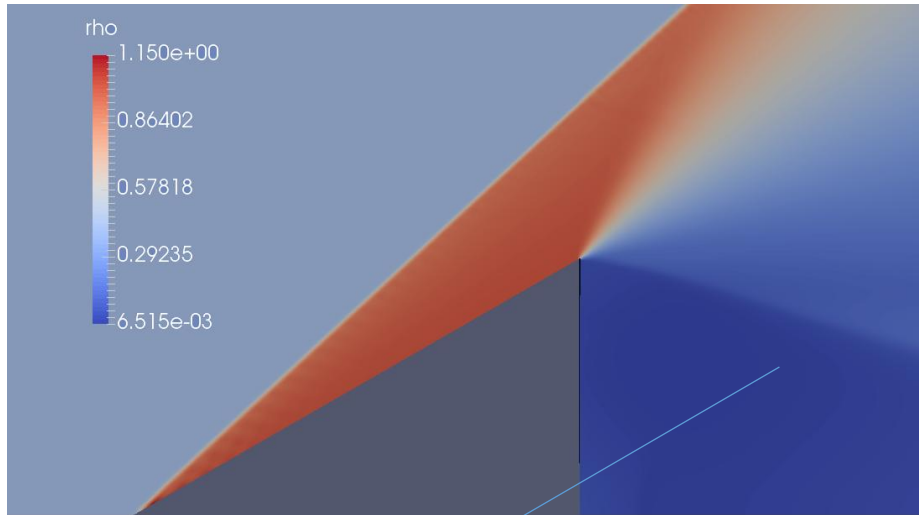
Supersonic solvers

Solver	Source	Application	Comments
sonicFoam	OpenFOAM	Transient, trans-sonic/supersonic	Pressure-based
rhoCentralFoam	OpenFOAM	Supersonic	Density-based, Kurganov-Tadmor
dbnsTurbFoam	foam-extend	Supersonic	Roe-type
pisoCentralFoam	Kraposhin, Strijhak	Subsonic/Supersonic	Hybrid KT-PISO

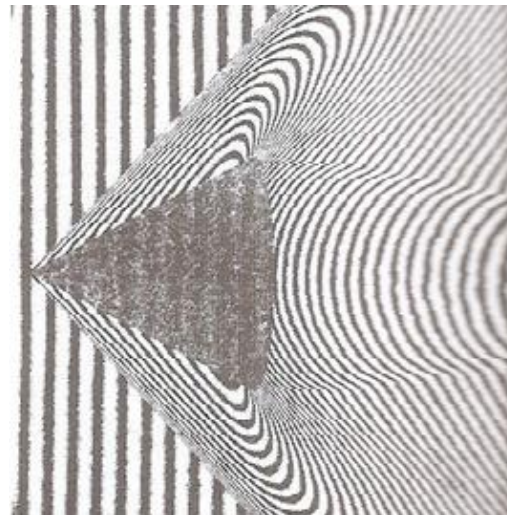
MHD solvers

Solver	Source	Application	Comments
mhdFoam	OpenFOAM	Incompressible MHD	Incompressible Induction form
rhoPisoFoam (MHD)	Xisto, et. al.	Compressible resistive MHD	Pressure-based

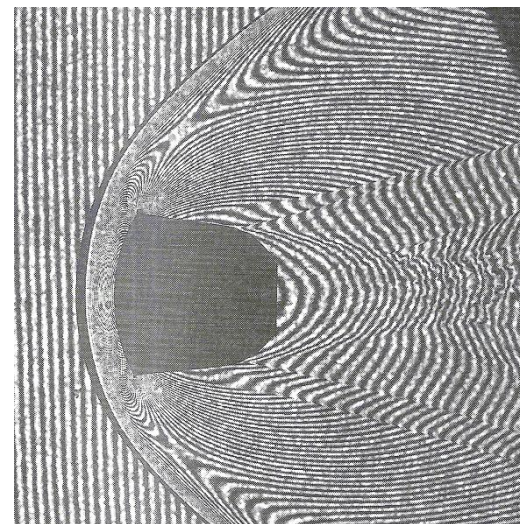
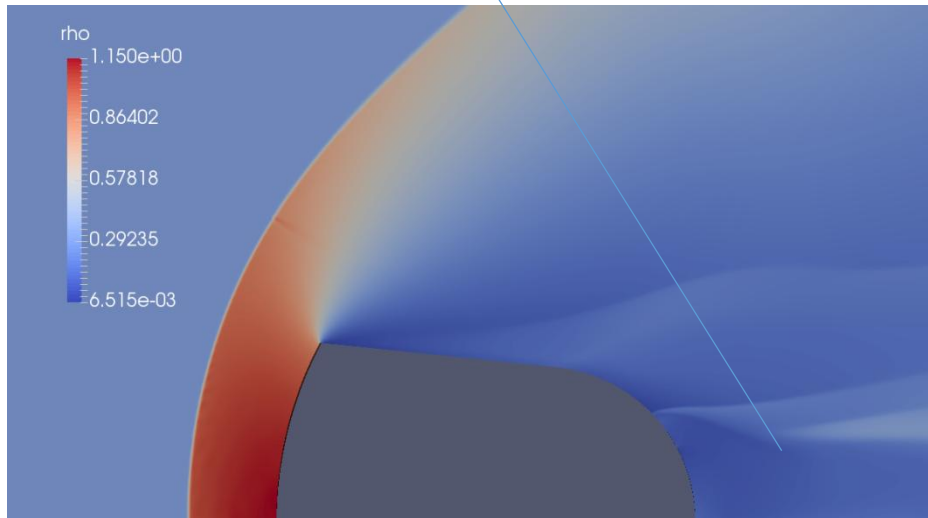
Supersonic flow experimental data



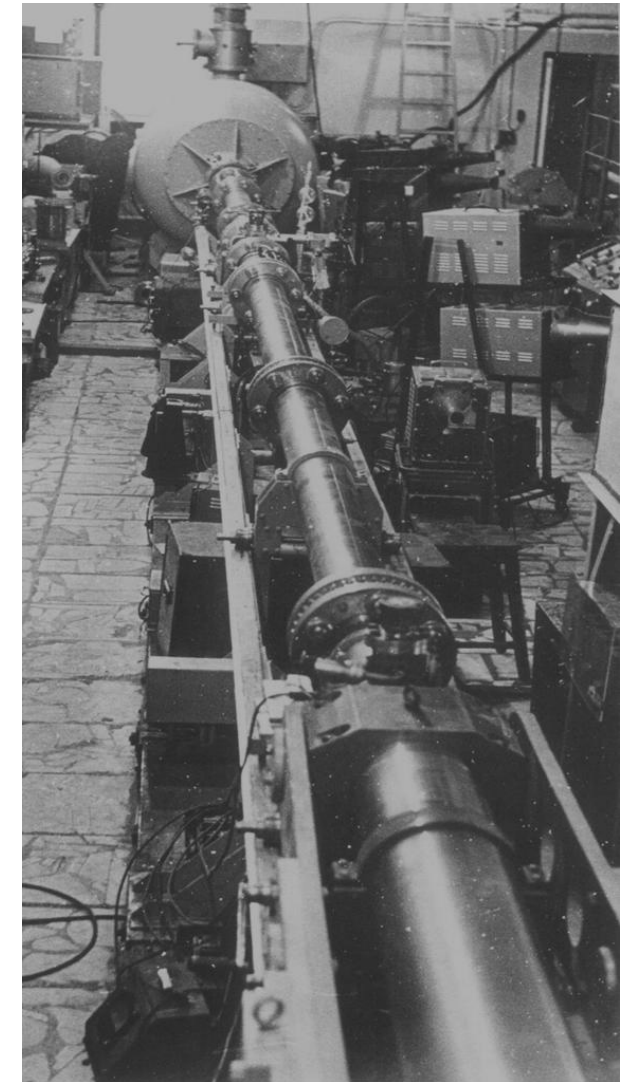
Subsonic flow region



Cone, middle diameter: 19 mm, Mach = 2



“Soyuz” model, middle diameter: 17.4 mm, Mach = 2.4



Ioffe Institute shock tube

Flow parameters and MHD equations

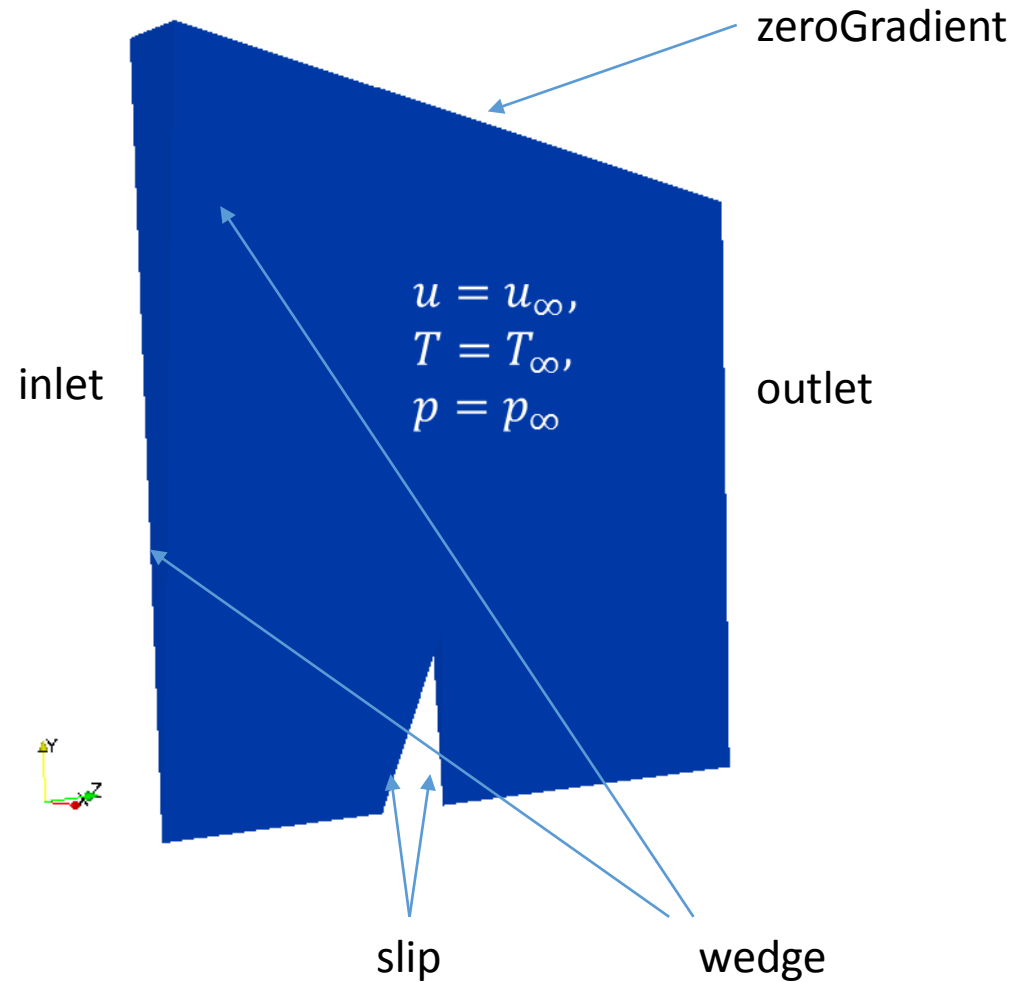
Parameter	Formula	Value
Reynolds number (R)	$\frac{\rho v L_c}{\eta}$	$10^5 - 10^6$
Stuart number (S)	$\frac{\sigma L_c B^2}{\rho v}$	$0 - 1$
Magnetic Reynolds number	$\frac{uL}{\eta_m}$	$\ll 1$
Knudsen number	$\frac{k_B T}{\sqrt{2} \pi d^2 p l}$	$\sim 10^{-3} - 10^{-5}$
Mach number	$\frac{u}{\sqrt{\frac{\gamma R T}{M}}}$	$2 - 4$

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0, \quad \frac{\partial}{\partial t} (\rho \mathbf{v}) + \nabla \cdot \left[\rho \mathbf{v} \mathbf{v} + \left(p + \frac{1}{2} B^2 \right) I_{3 \times 3} - \mathbf{B} \mathbf{B} \right] = 0,$$

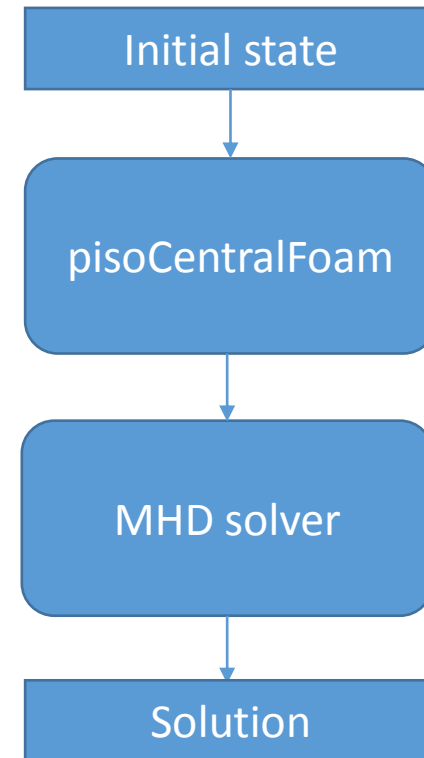
$$\frac{\partial}{\partial t} \left(\frac{1}{2} \rho v^2 + \rho e + \frac{1}{2} B^2 \right) + \nabla \cdot \left[\left(\frac{1}{2} \rho v^2 + \rho e + p + B^2 \right) \mathbf{v} - \mathbf{v} \cdot \mathbf{B} \mathbf{B} \right] = 0.$$

$$B = B_0(x, y, z)$$

Initial and boundary conditions

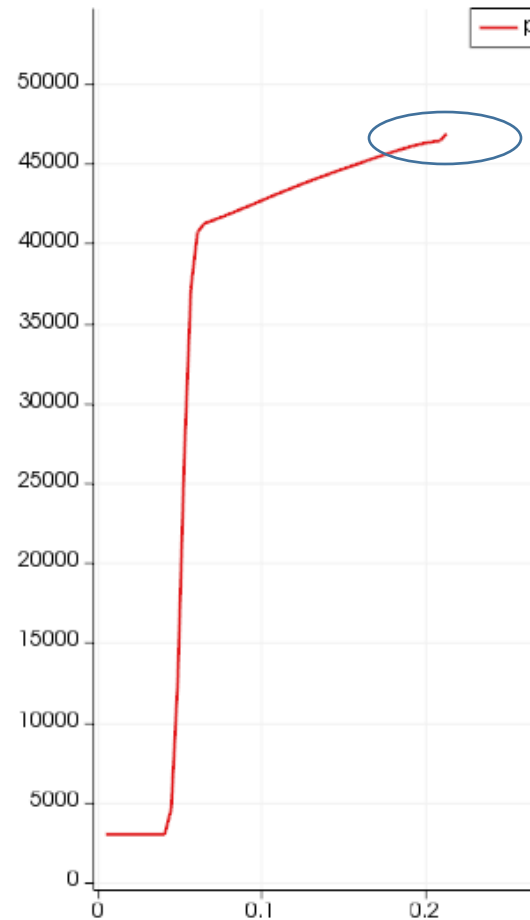


Solution flowchart

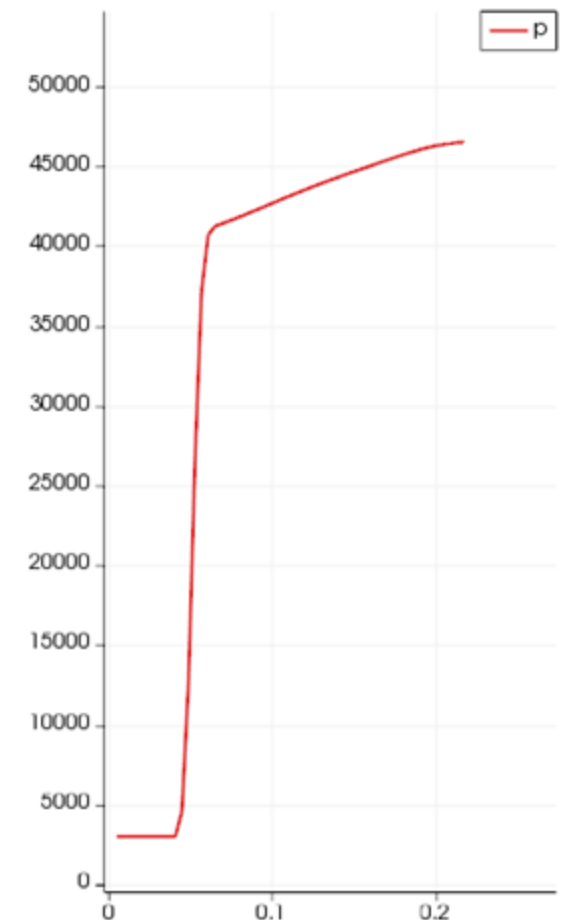


1. **B-T schemes** (*Balbás J., Tadmor E., Wu C. C. Non-oscillatory central schemes for one- and two-dimensional MHD equations*)
2. **HLL-Roe scheme**. (*Janhunen P., A positive conservative method for magnetohydrodynamics based on HLL and Roe methods*)

Balbas-Tadmor



HLL-Roe



Pressure profiles on the axis

MHD interactions experiment

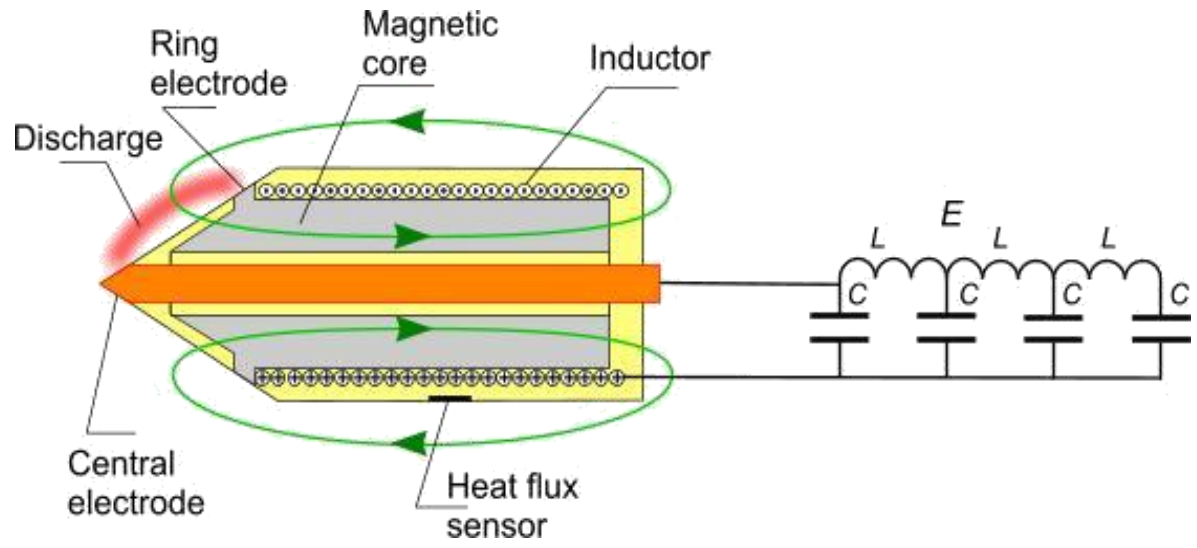
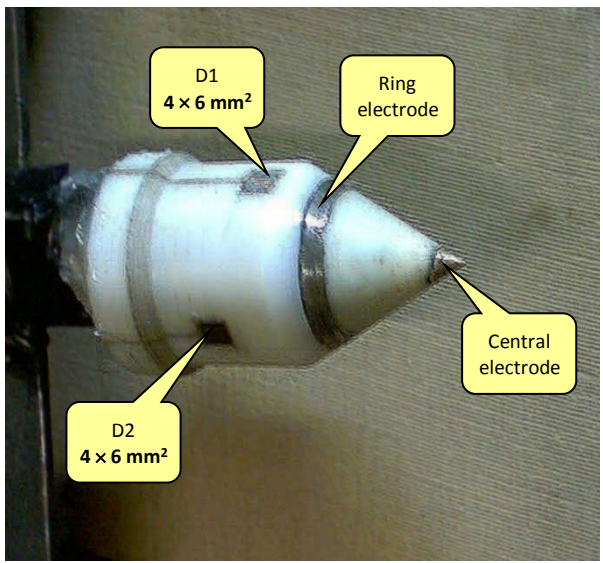
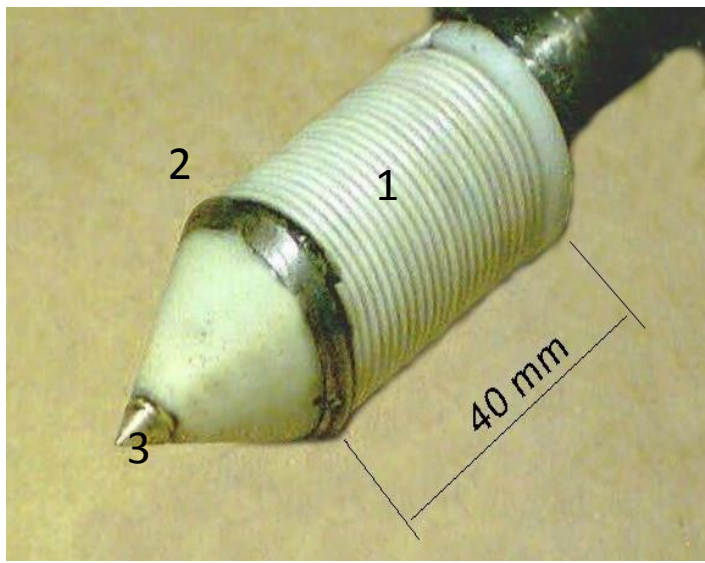
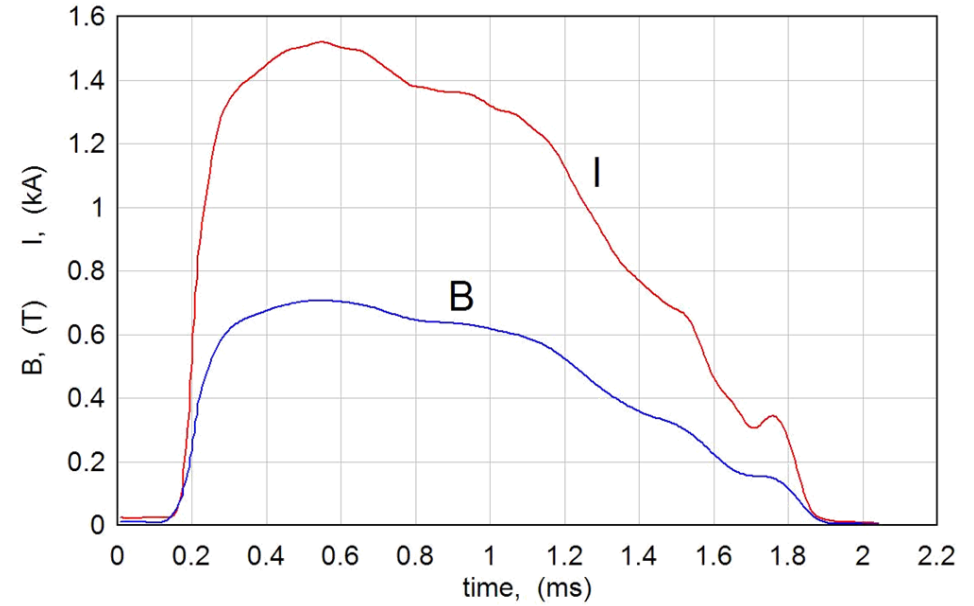


Fig. Model schematics



1. Solenoid
 2. Ring electrode
 3. Central electrode
- D1, D2 – Hear sensors

*from the materials of Fundamental Research session of RAS presidium "Fundamental problems in mechanics and related sciences" Saint-Petersburg, July 5-6, 2014

Passive (Thermal)

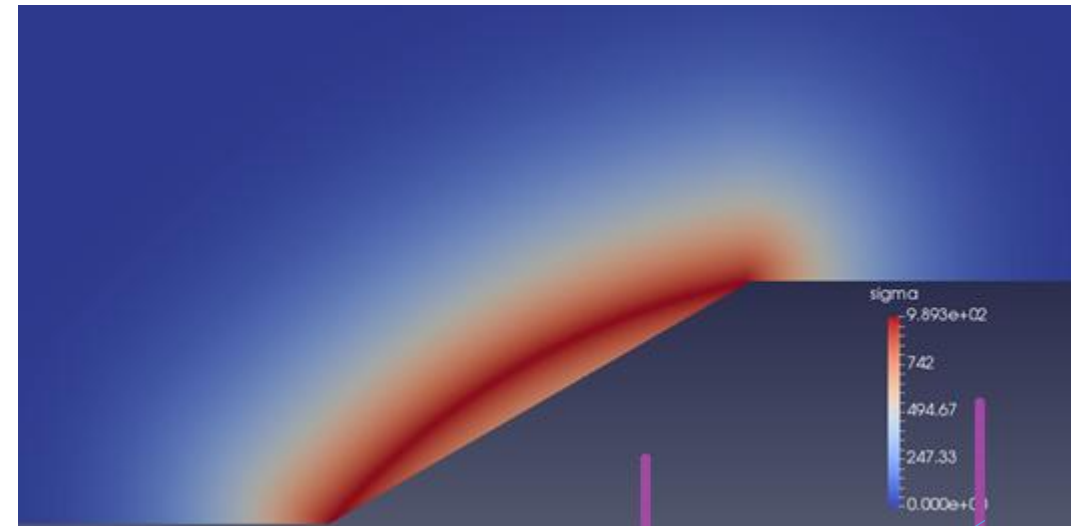
Spitzer – Harm conductivity formula

$$\sigma = 1.53 \times 10^{-2} \frac{T^{\frac{3}{2}}}{\ln \Lambda};$$

$$\ln \Lambda = \ln \left(\frac{12\sqrt{2}\pi(k_B\epsilon_0 T)^{\frac{3}{2}}}{q^3 n^{\frac{1}{2}}} \right).$$

$$T = \frac{1}{c_v} \left[e_t - \frac{1}{2} \left(U^2 + \frac{B^2}{\rho\mu_0} \right) \right].$$

Active (Discharge)

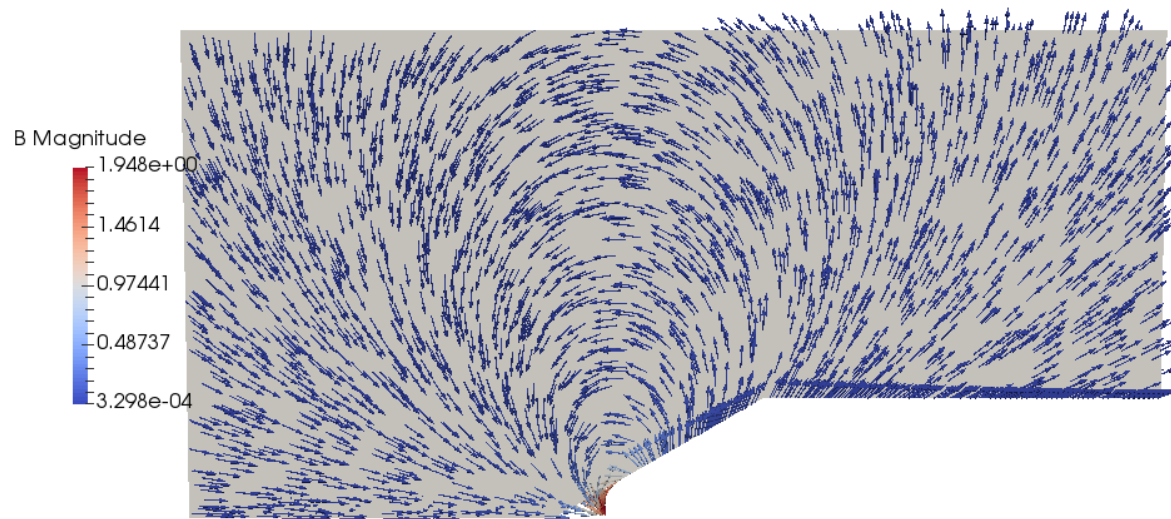


Position 2

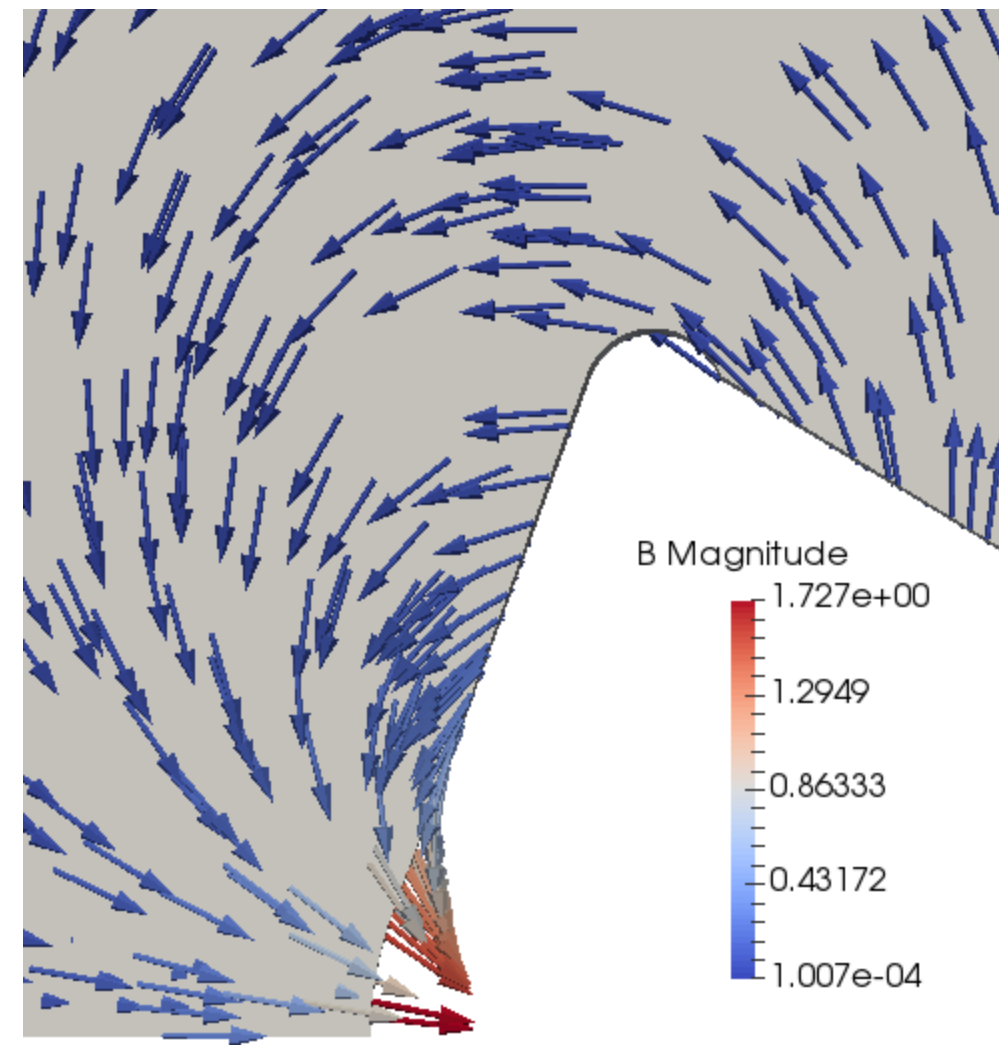
Position 1

Gas in front of the body is ionized by the electrical discharge between the vertex and the base of the cone. Coil, that generates the magnetic field was placed in 2 different positions.

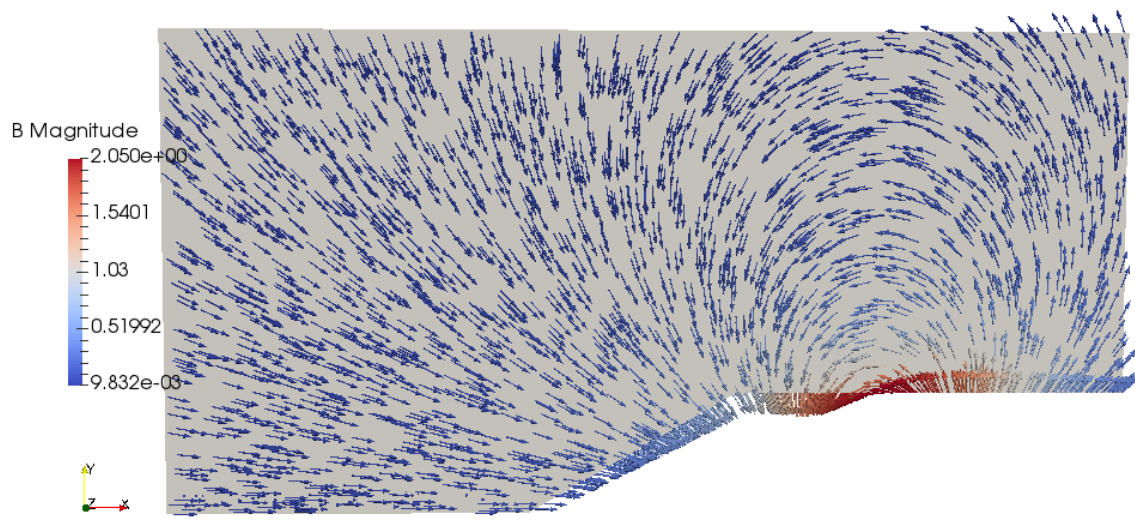
Magnetic field distribution



Cone-cylinder case 1



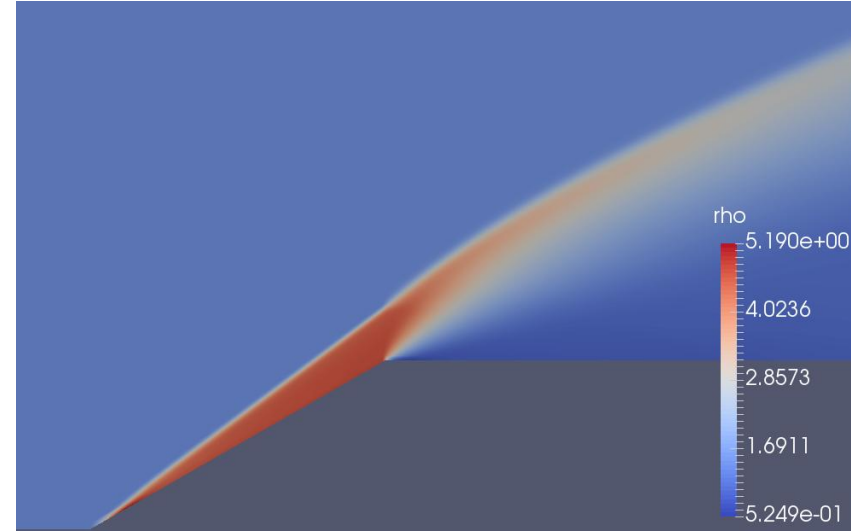
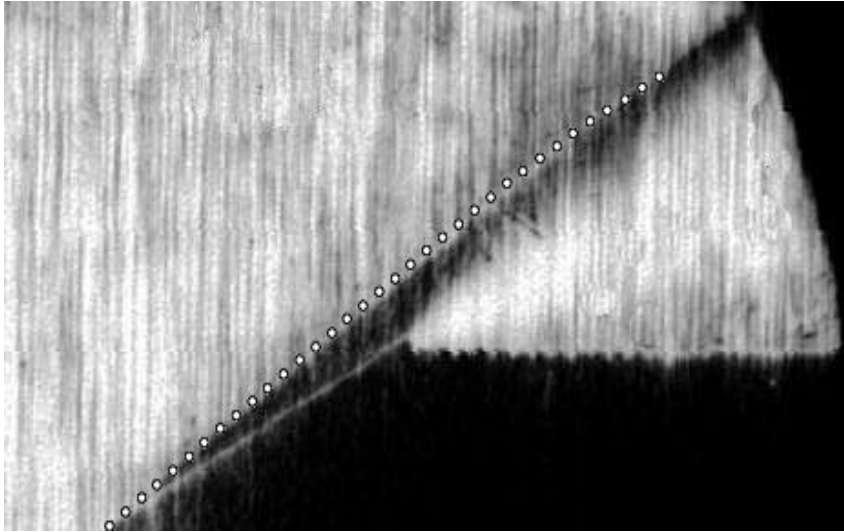
Frustum case



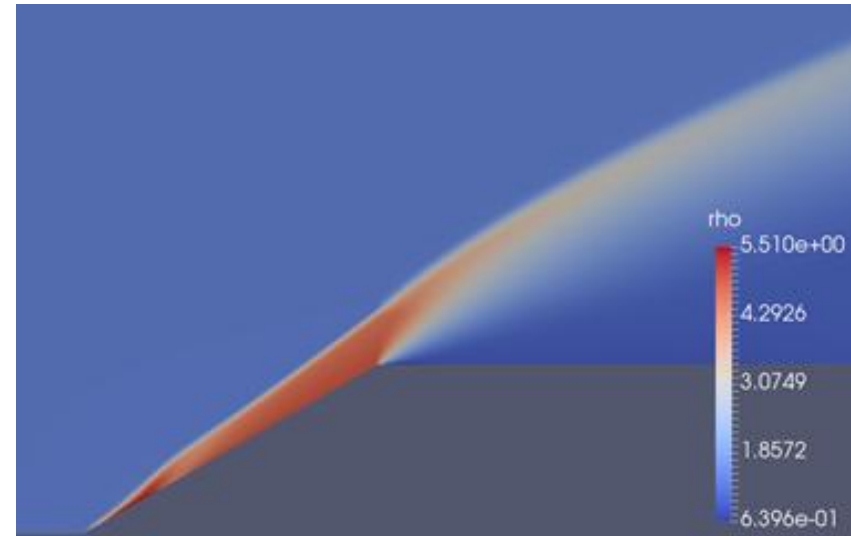
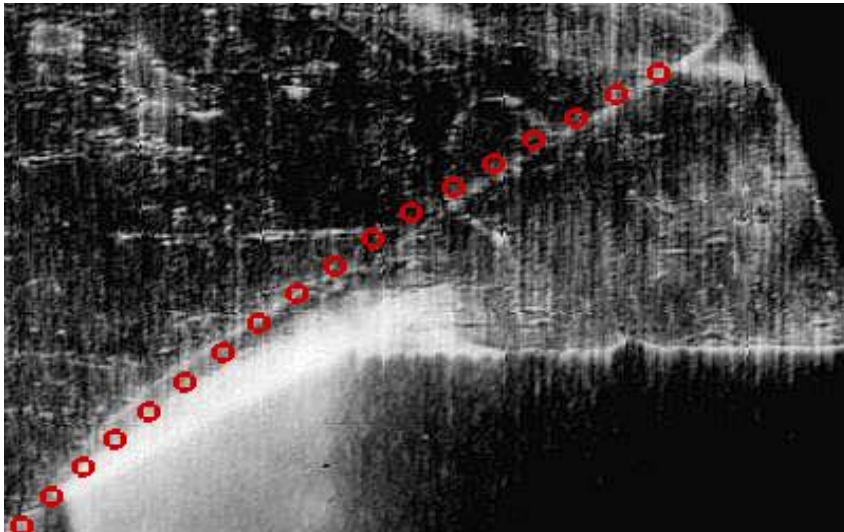
Cone-cylinder case 2

Wave front shape comparison

a.)

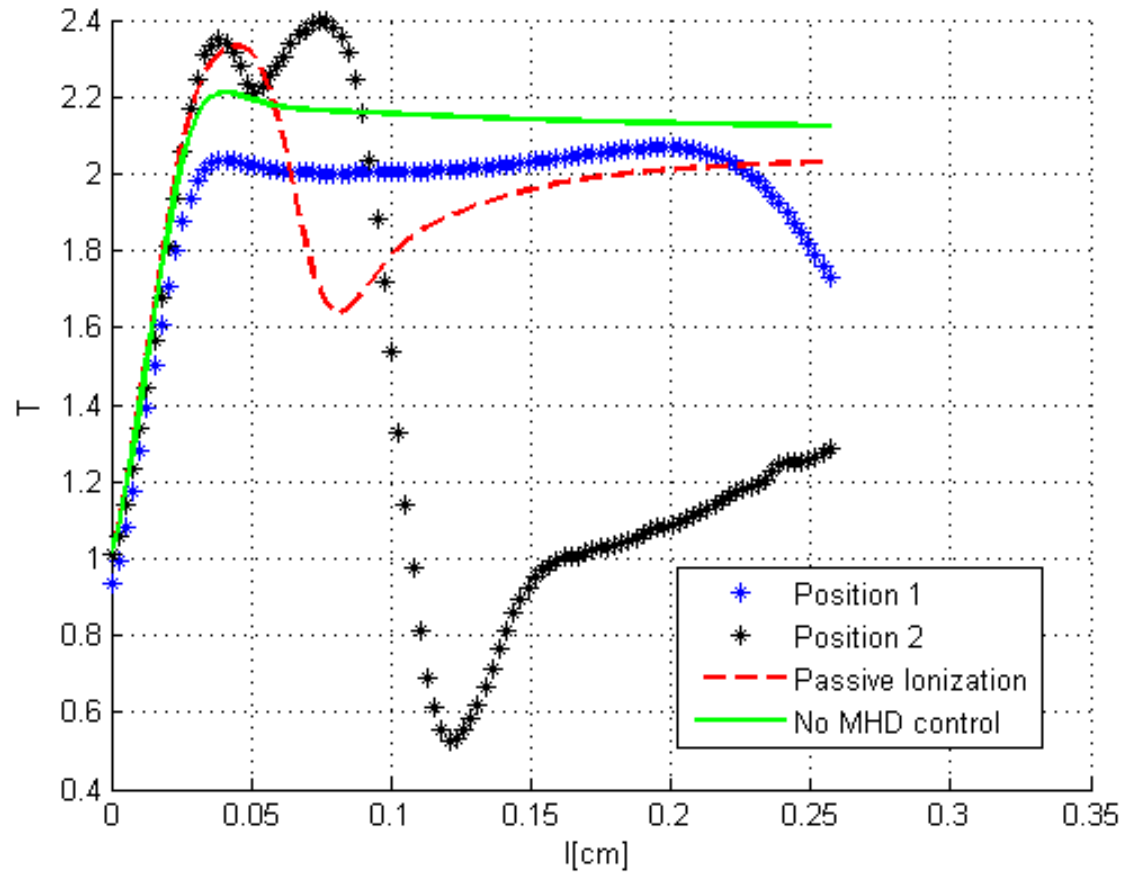


b.)

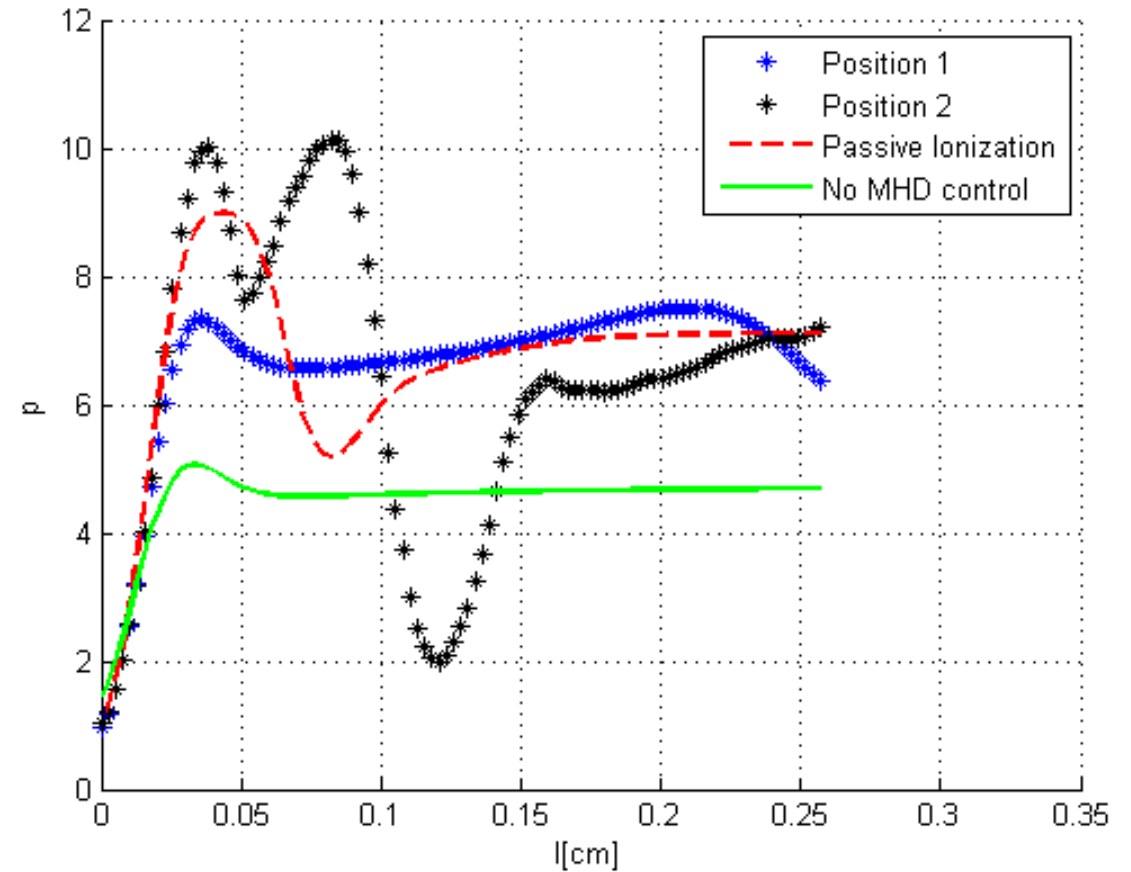


Shadowgrams of the flow (on the left) a.) without a magnetic field b.) with a magnetic field compared to the numerical results (on the right)

Numerical results: cone-cylinder



Temperature profiles
on the generatrix of a cone-cylinder

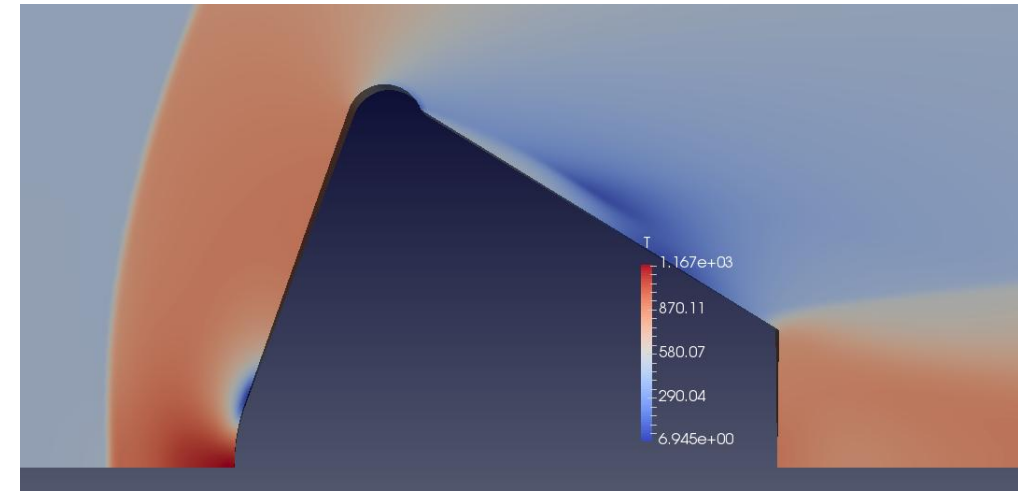
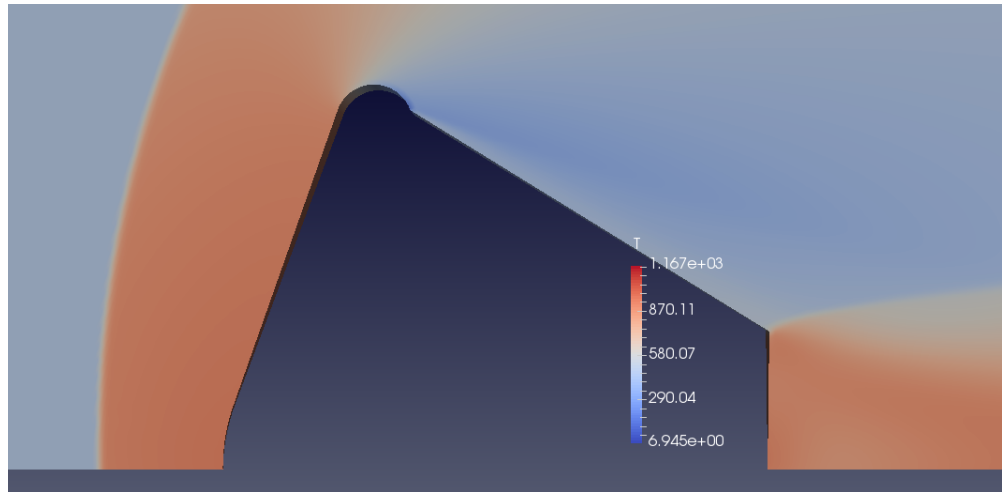


Pressure profiles
on the generatrix of a cone-cylinder

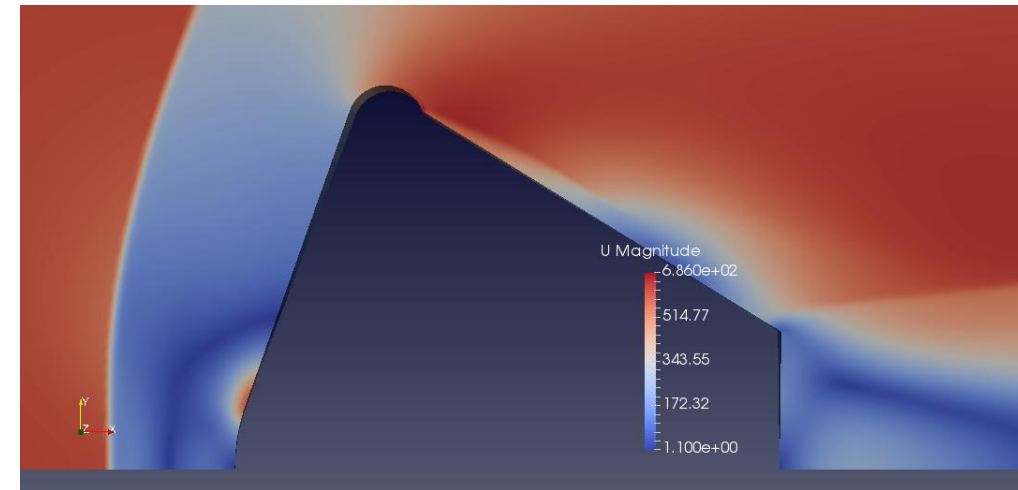
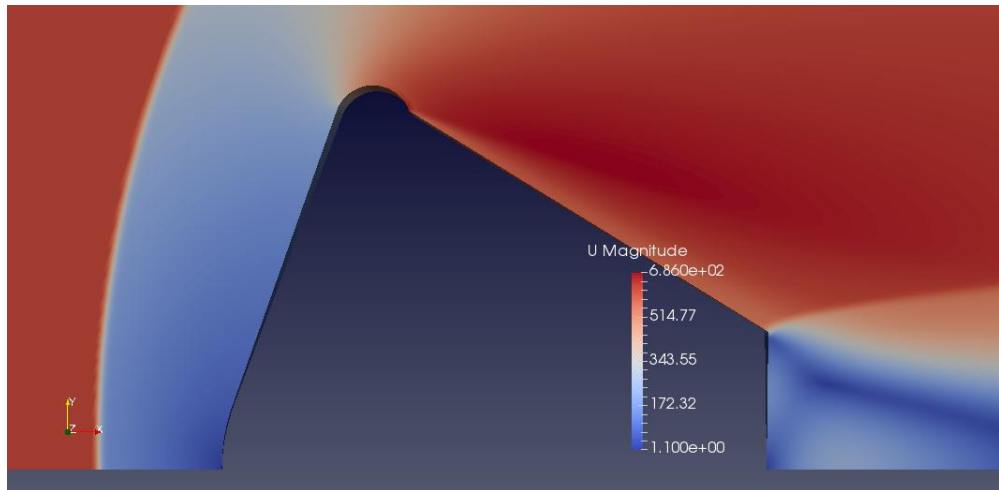
Numerical results: flow around sphere-cone

no MHD

MHD



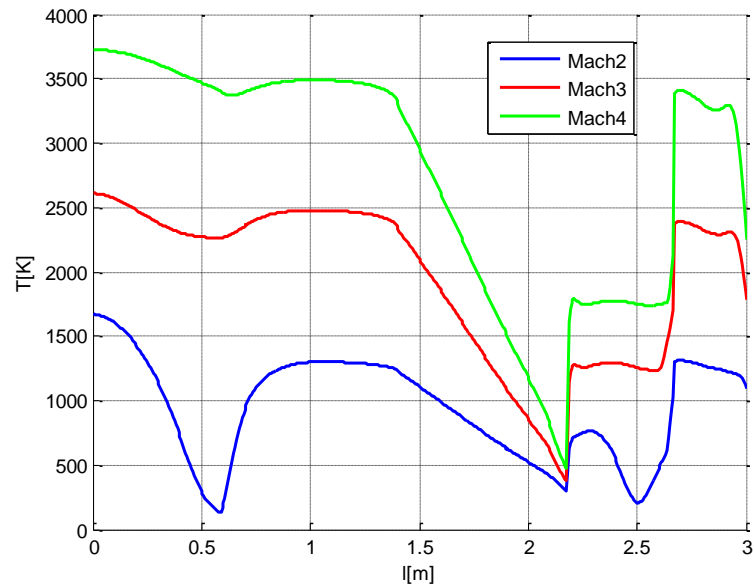
Temperature



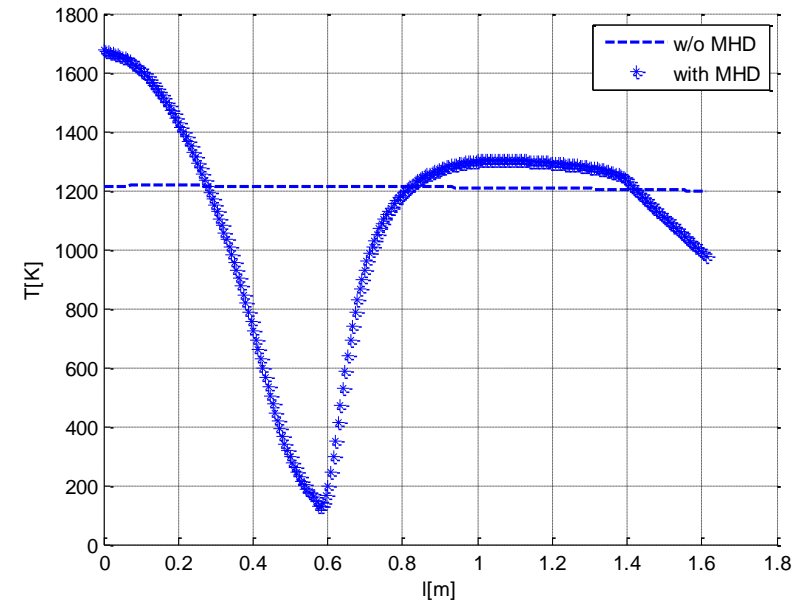
Velocity magnitude

Numerical results: flow around sphere-cone

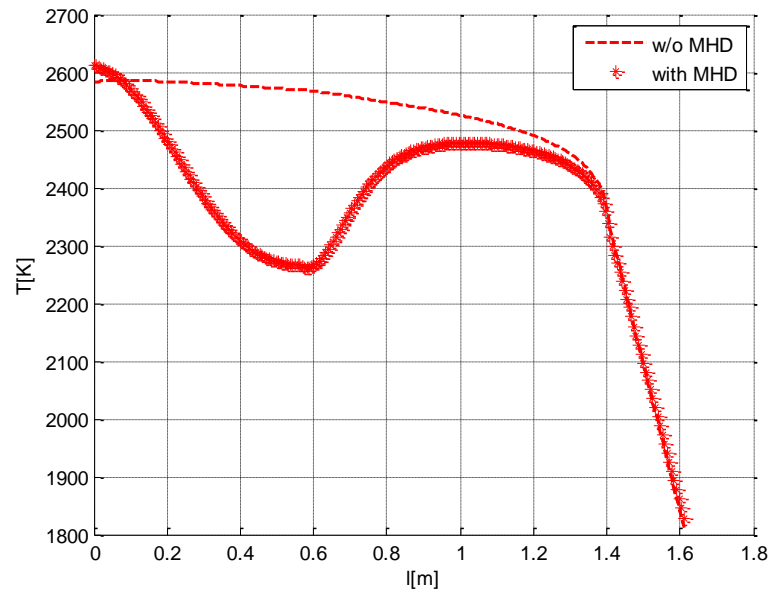
Temperature profiles over the whole body:



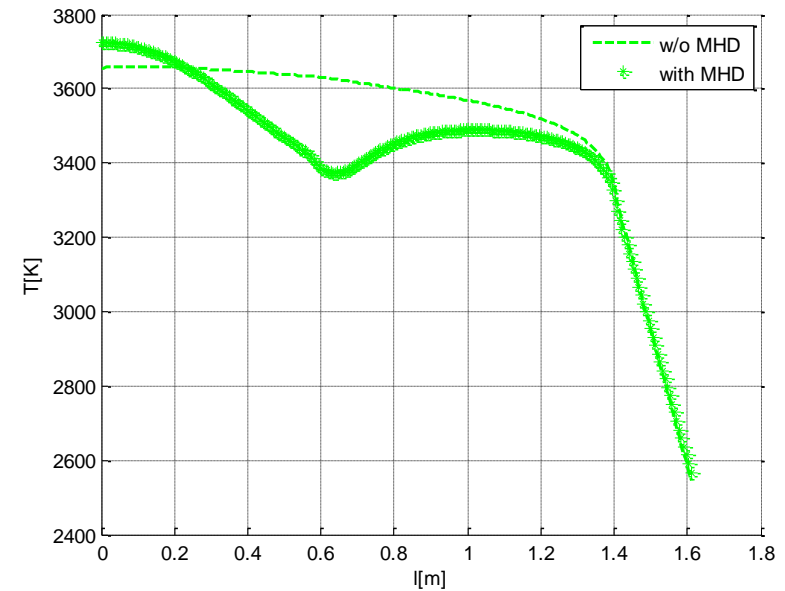
T on the front, Mach 2



T on the front, Mach 3



T on the front, Mach 4



Further research prospects

Physical phenomenon investigation

- Determining the feasibility of the concept
- Designing a flexible control system
- Figuring the energy cost

Mathematical model enhancement

- Transition to 3D, angle of attack
- Taking into account real gas effects
- Surface radiation
- Laminar-turbulent transition
- Introducing comprehensive thermochemical model, ionization model

Solver development

- Increasing stability and accuracy
- Dealing with low-density effects